
Ollier Smurthwaite Architects on behalf of Irfan Dema

Environmental Standards Statement

Proposal for 36 new dwellings @ the former VASA Club, Charlestown

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1 Executive Summary

This Environmental Standards Statement has been prepared by Watt Energy on for Ollier Smurthwaite on behalf of Irfan Dema to support a planning application for the development of the former VASA Club site.. The statement specifically addresses the following Manchester City Council approved climate change action plans in addition to planning policies, as stipulated in the Manchester Core Strategy (July 2012):

- Guide to Development in Manchester SPD (2007)
- Our Manchester Strategy 2016-2025
- Manchester: A Certain Future (2013)
- Manchester Climate Change Board – The Zero Carbon Framework 2020-2038
- Climate Change and Low Emissions Implementation Plan 2016-2020
- Meeting Our Objectives and Targets – Manchester Climate Change Framework – 2020-25
- Manchester Residential Quality Guidance 2017
- Core Strategy Policy DM 1 - Development Management
- Core Strategy Policy EN 4 - Reducing CO₂ Emissions by Enabling Low and Zero Carbon Development
- Core Strategy Policy EN 6 - Target Framework for CO₂ Reductions from Low or Zero Carbon Energy Supplies
- Core Strategy Policy EN 8 – Adaptation to Climate Change
- Core Strategy Policy EN 9 – Green Infrastructure
- Core Strategy Policy EN 14 – Flood Risk
- Core Strategy Policy EN 15 – Biodiversity and Geological Conservation
- Core Strategy Policy T 1 – Sustainable Transport

The statement details how the development will incorporate sustainable design and resource efficiency in line with the Energy Hierarchy, so to meet the policy requirements and council targets whilst reducing its overall environmental impact. The methodology and calculations are consistent with the MCC Appendix A EN6 Energy Target Explanation and all figures used within this report have been based on the most recent issue of drawings and modelled using SAP 2012 to accurately predict Energy Usage and CO₂ reductions.

In relation to the planning documents and policies outlined above, the development is required to achieve a **10%** reduction in carbon emissions over Part L 2013 of the Building Regulations.

In order to achieve compliance, the development has been designed with a holistic low energy design concept involving a fabric first approach. The U-values, design air permeability and ventilation targets all aspire to Passive House design standards along with the consideration and application of low zero carbon (LZC) renewable technologies.

Accordingly, this energy and sustainability statement has been prepared to meet the above requirements based solely on energy efficiency measures which have gone beyond Manchester City Council Carbon targets, negating the need for additional LZC technologies.

As a result, the predicted site wide reduction in CO₂ over Part L 2013 of the Building Regulations can be summarised as:

- **13.4%** with SAP 9 carbon factors (current Building Regulations)
- **36.1%** with SAP 10 carbon factors
- **61.5%** with SAP 10.1 carbon factors (proposed improvements to Part L)

This statement also examines how the design, specification and characteristics of the proposal will contribute to sustainability and meet the relevant objectives outlined within the National Planning Policy Framework (NPPF) revised July 2021, in addition to the Manchester City Council approved climate change action plans and core strategy planning policies outlined above. The sustainability measures assessed included:

- Flood Risk Zone
- Green and Blue Infrastructure
- Sustainable Drainage Systems (SUDs)
- Biodiversity / Ecology
- Internal Water Efficiency
- Waste Management
- Materials
- Pollution Control
- Health and Wellbeing
- Sustainable Transport

The development therefore complies with all Manchester City Council's current and future policy requirements relating to creating a sustainable development.

In relation to the planning target centred around carbon emissions reduction, the proposed development is achieving a **13.4%** reduction in these emissions, over the Part L1A 2013 of the Building Regulations. This surpasses all of Manchester City Council's planning targets and therefore allows compliance to be reached.

2 Planning Statement

The following statement relates to the proposed development at the Former VASA Club at 283 White Moss Lane, Charlestown.

2.1 The Site and Proposed Development

The site is located northeast of the centre of Manchester, within Charlestown. The site occupies approximately 0.403 hectares of land. A plan, with the site's extents denoted by the red outline seen in Figure 1 (shown later in this subsection).

The site is bounded to the northwest by White Moss Road, Haddington Drive to the southeast and adjacent to Haverfield Road to the southwest. The site is currently occupied by the former VASA club, a community club and bar.

The proposal is for a residential-led mixed use development consisting of 20 new build houses, 16 new build apartments and approximately one 31.04sqm private amenity space to the rear of each dwelling. The apartments will be a mix of one and two bed, and the townhouses will be a mix of three and four bed (use class C3). Also provided will be associated ancillary facilities including a refuse/recycling store and bike store.

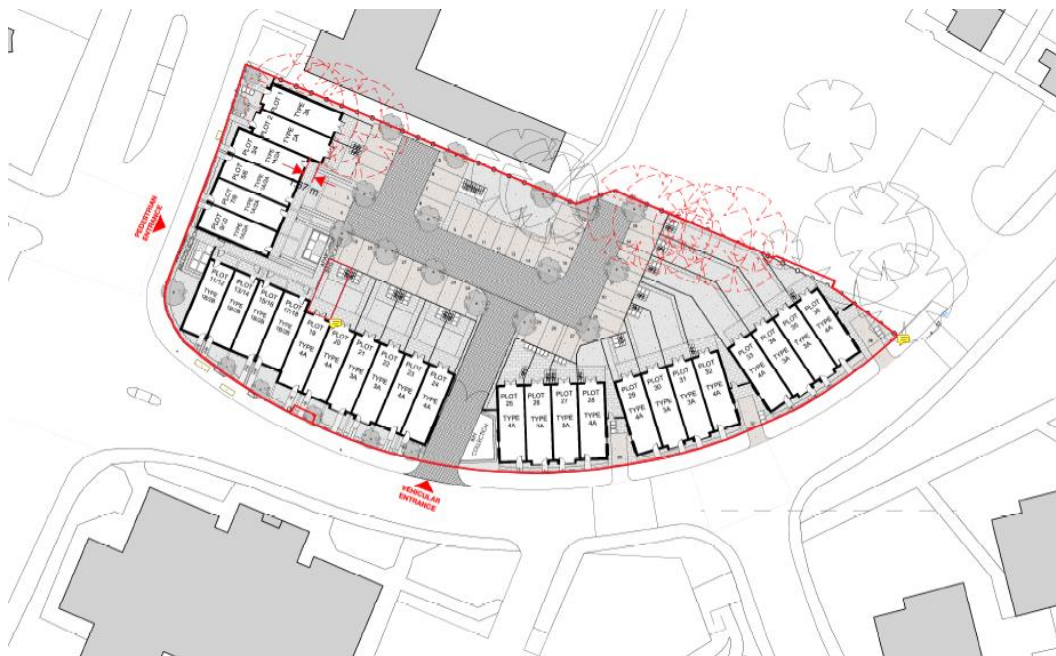


Figure 1: Ground Floor Plan

2.2 Relevant Policies and Guidance

2.2.1 Local Planning Policy

2.2.1.1 Manchester Core Strategy

Manchester's Core Strategy (CS) was adopted on 11th July 2012 and is the key Development Plan Document (DPD) guiding the measures assessed in this report.

CS Policy DM 1 - Development Management: Stipulates that all new development should have regard for several development principles relevant to sustainability, including: waste management, designing for health, flood risk, green infrastructure, biodiversity. Additionally, subject to scheme viability, developers will be required to demonstrate that new non-domestic development will achieve a BREEAM Rating of 'Very Good' or for domestic development to achieve the Code for Sustainable Homes standard.

CS Policy EN 4 – Reducing CO2 Emissions: This policy targets the reducing of CO2 emissions through the following of the energy hierarchy; firstly reducing the need for energy through efficient design measures, followed by clean energy and lastly, the application of renewable or LZC technologies. In addition to this point, MCC state within this policy all new development is required to use building materials that have low embodied carbon.

CS Policy EN 6 - Target Framework for CO2 Reductions from Low or Zero Carbon Energy Supplies: This Policy requires electricity intense residential development of 10 or more units to meet, as a minimum, a 15% reduction in domestic CO2 emissions over Part L of the 2010 Building Regulations, unless proven to be unviable. As Part L 2013 of the Building Regulations represents a 6% improvement on 2010 levels, this target is subsequently equivalent to a 9% improvement in CO2 emissions over Part L 2013. Section 2.3 provides evidence of how this target is achieved.

CS Policy EN 8 – Adaptation to Climate Change: Expects all new development to be adaptable to climate change in terms of its design, layout, siting, and function of both building associated external spaces.

CS Policy EN 9 – Green Infrastructure: Requires new developments to maintain existing green infrastructure whilst using every opportunity, in accordance with current Green Infrastructure Strategies, to enhance the quality and quantity of green infrastructure, improve the performance of its functions and create and improve linkages to and between area of green infrastructure.

CS Policy EN 14 – Flood Risk: This policy expects all new developments to minimise surface water run-off through the use of SUDs and Green Infrastructure.

CS Policy EN 15 – Biodiversity and Geological Enhancement: Developers will be expected to identify and implement reasonable opportunities to enhance, restore or create new biodiversity, either on or adjacent to the proposed site.

CS Policy T 1 – Sustainable Transport: Policy aims to deliver sustainable, high quality, integrated transport systems to encourage a shift away from car travel to public transport, cycling and walking.

2.2.1.2 Guide to Development in Manchester, Supplementary Planning Document 2007

The Development Guide in Manchester Supplementary Planning Documents (SPD) establish and set out the ongoing generation of the City by providing a set of set principles which will guide developers, architects, and residents in the design of the city. The MCC Core Strategy stipulates that all new residential developments should comply with the design guidance set out in the SPDs. These principles include the following environmental standards relevant to this report: energy strategy, water consumption, drainage management, weather resilience, waste management, construction management, biodiversity, and waterways.

2.2.1.3 Manchester Residential Quality Guide 2017

The Manchester Residential Quality Guide has been developed to help shape the creation of new homes and communities across the Greater Manchester city region, beginning with the Centre and its immediate surroundings. This document outlines the considerations, qualities, and opportunities that will help to deliver high quality residential development as part of successful and sustainable neighbourhoods across Manchester. The guidance includes the following nine components:

Make it Manchester – developers must understand the city’s unique character, heritage old and new, density and scale in various parts of the city and appreciate how new homes will fit in to what is already there.

Make it bring people together – new homes must encourage a sense of community and neighbourliness, offering a mix of tenures to promote a mix of people.

Make it animate streets and spaces – understand the relationship between new homes and its environment and create public space.

Make it easy to get around – make sure developments have good transport links, along with good walking and cycling provision.

Make work with the landscape – development should improve the connection with the local environment with improved biodiversity, as well as greening and water schemes.

Make it practical – dealing with waste, car parking, bike storage and visitors should be made as easy as possible.

Make it future proof – design must anticipate the impacts of climate change and extreme weather with efficient design and adaptability.

Make it a home – sufficient space, natural light, privacy and storage are essential for people to settle down and flourish.

Make it happen – ensuring proposals are delivered, to a high quality, with high design standards and high sustainability.

2.2.1.4 Manchester's Great Outdoors 2015-25

A Green and Blue Infrastructure Strategy for Manchester aims to invest to date in the city's Green and Blue infrastructure over the next 10 years (by 2025). Four objectives have been established to enable the vision to be achieved: 1. Improve the quality and function of existing green and blue Infrastructure, to maximize the benefits it delivers. 2. Use appropriate green and blue infrastructure as a key component of new developments to help create successful neighbourhoods and support the city's growth. 3. Improve connectivity and accessibility to green and blue infrastructure within the city and beyond. 4. Improve and promote a wider understanding and awareness of the benefits that green and blue infrastructure provides to residents, the economy, and the local environment.

2.2.1.5 Manchester Climate Change Framework 2020-25

Following the declaration of a climate emergency by MCC In July 2019, this framework was adopted and is an in-depth strategy to accompany the Draft Manchester Zero Carbon Framework 2020-38, which was published in February 2019. It is a framework that will continue to develop over the next five years, in line with changes in policy, climate science, rate of progress and other factors. The framework has set out four objectives to facilitate this:

Objective 1 – Staying within our carbon budgets.

- Direct CO2 emissions: staying within our 15-million-ton carbon budget for 2018-2100, including reducing the CO2 emitted from our homes, workplaces and ground transport by at least 50% during 2020-25.
- Indirect CO2 emissions: understanding and taking action on the things that we consume, and which generate greenhouse gases through their production, transportation and disposal.

Objective 2 – Climate adaptation and resilience

- Increase the amount of urban green infrastructure cover, aiming for a 10% increase by 2038 from 2018 levels, in line with the Greater Manchester aim.
- Respond to these risks by incorporating adaptation and resilience within our plans and strategies, and acting to make necessary changes to our buildings, infrastructure and our natural environment.

Objective 3 – Health and wellbeing

- Adapt the city's built and natural environment and prepare our residents to become more resilient to these changes. Increasing the amount and quality of green space to enable residents to benefit from the improved physical and mental health that will come as a result.
- Improving the energy efficiency of the city's homes and providing access to affordable, secure supplies of renewable energy are essential help get 38,000 Manchester households out of fuel poverty.

Objective 4 – Inclusive, zero carbon and climate resilient economy

- Ensure that Manchester establishes an inclusive, zero carbon and climate resilient economy where everyone can benefit from playing an active role in decarbonising and adapting the city to the changing climate.

2.2.2 Manchester City Council's Planning Document Targets

Manchester City Planning Policy currently uses the following documents to look to establish the carbon reduction targets to be achieved in new developments across the City.

These documents use different terminology to describe achieving the various reduced carbon emissions.

Please see below a summary of the terminology and targets set out within the current Manchester Planning Policy documents:

Planning Document:	Time of Production or Adoption:	Low Carbon Target:	Sustainable Design Definition:
Manchester Council's Core Strategy 2012-2027	Adopted 2012	Targets a 9% reduction in carbon emissions over Part L Building Regulations.	Low Carbon (9% over Part L 2013)
Climate Change and Low Emission Strategies 2016-2020	Adopted 2016	Targets a 48% reduction in carbon emissions from 1990 - 2020	Low Carbon (48% over 1990 emissions)
Manchester: A Certain Future	Produced in 2009, updated in 2013	Targets emitting 41% less CO ₂ in 2020 than in 2005 – Equates to 10% over Part L 2013 (if going by Part L requirements)	Low Carbon (10% over Part L 2013)

Table 1: Overview of Manchester Planning Documents Carbon Targets



2.2.3 National Planning Policy

The NPPF (revised July 2021) sets out the Government's planning policies for England and how these are expected to be applied. The overall emphasis of the NPPF is to reiterate the Government's key objectives, including securing sustainable development.

The NPPF defines the purpose of the planning system as being to contribute to the achievement of sustainable development. It explains at Paragraph 8 that there are three dimensions to sustainable development. These are economic, social and environmental and should be pursued simultaneously through the planning system.

Paragraph 10 states that at the heart of the Framework is a presumption in favour of sustainable development.

2.3 Sustainable Design Strategy

2.3.1 Energy and Carbon Emissions

Building Services Strategy

In response to the policy requirements and climate change plan targets set out in section 2.2, developments should aim to assist and achieve the following carbon reduction targets:

1. Achieve a minimum of 10% CO₂ reduction over the Part L 2013 Target Emission Rate (TER), as per Target 2 (Electricity intense buildings) in Table 12.1 of Policy EN6.
2. Assist in achieving carbon neutrality by 2038.

To achieve the most accurate calculations and estimates, the proposed units have been modelled using SAP 2012 the governments Standard Assessment Procedure for residential dwellings.

The proposed strategy for minimising energy use and carbon emissions is based on the energy hierarchy described in CIBSE Guide F 2012 (Energy efficiency in buildings). The energy hierarchy has been adopted for the development to ensure that the correct approach to design is taken to promote an energy-efficient low carbon solution (see figure 2). This has ensured that the benefits of effective methods of energy use reduction have been maximised first. The approach adopted is as follows:



Fig 2: Energy Hierarchy

Minimise energy demand – Implement passive design measures and optimise the building envelope in terms of orientation, air tightness, and insulation. For example, the proposal is targeting a low carbon classification through a holistic low energy design concept as it will be designed with a fabric first approach whereby standards designed to exceed Building Regulations compliancy are aspired to for all fabric U-values and air permeability targets.

Meet demands efficiently – Specification of energy efficient decentralised plant, heating, ventilation, lighting, and system controls to facilitate efficient operation.

Particular attention is being paid to the wellbeing of occupants. The ventilation strategy has been developed to minimise noise ingress from the proposed location as far as possible while minimising the risk of overheating.

Additional Renewable Energy Measures

Opportunities for incorporating low and zero carbon technologies (LZCT) have been considered for this development. The viability of several separate technologies was examined in a LZCT study (see section 3).

Efficient and Sustainable Design Measures

In line with the above Sustainable Design Strategy, the following Energy Efficient design measures are specified.

- High levels of insulation throughout with minimal thermal bridges
- Passive solar gains and internal heat sources
- Excellent level of airtightness
- Good indoor air quality by openable windows

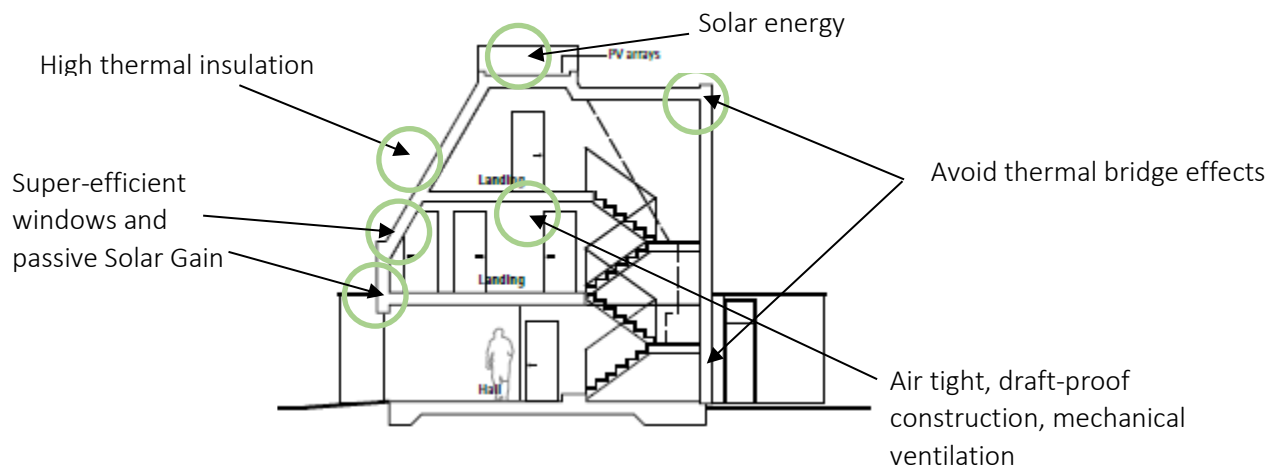


Fig 3. Efficient Design Measure examples

The Proposed specifications and key energy efficient design measures are as follows:

Residential Units:

- Ground floor U-values of 0.10 W/m²K
- External Wall U-values of 0.15 W/m²K
- Flat Roof U-values of 0.10 W/m²K
- Pitched Roof U-values of 0.10 W/m²K
- Low Triple Glazed Window U-values of 0.8 W/m²K
- Thermal Lintels to reduce heat loss through thermal bridging
- 100% low energy lighting throughout
- 100% efficient electric panel heaters to each dwelling
- 120/180/300L Oso Super Xpress electric immersion cylinders to each dwelling
- MVHR – Vent Axia Sentinel Kinetic FH to each dwelling
- Air Permeability Rate of 3m³/hm² in all houses
- Electric Vehicle charging points to all houses and 10% provision provided to each flat

2.3.2 Choice and Impact of Renewable Technology

All reasonable technologies were investigated for their suitability to the site and development; please refer to section 3 for details.

Although LZC technologies have been assessed, energy efficiency measures have been prioritised to achieve MCC carbon targets.

2.3.2.1 Energy Efficiency Measures

The design team have considered the issues of solar heat gain in conjunction with protecting the dwelling from overheating to consider orientation and passive design. Not only does good insulation assist in reducing heat losses in the winter, it has a significant impact on preventing heat travelling through the build fabric during the summer.

The main living areas (and the associated large patio gazed areas) are orientated to the north easterly aspect; this approach ensures good levels of natural daylight and sunlight to the principle living areas, while much reducing any potential for overheating.

As highlighted in section 2.3.1 the dwellings have been designed with high levels of insulation to ensure U-values that far exceed the building regulations minima to reduce fabric heat loss. In addition, excellent levels of air tightness are to be achieved with accompanying MVHR units recovering heat extracted from wet rooms and supplying fresh filtered air.

The results show that, for the new developments with the energy efficiency measures, the reduction in CO₂ emissions is **13.3%** - Clearly, the client has confirmed their commitment to go beyond the requirements via the “fabric first approach” and meet MCC carbon targets.

2.3.3 Energy and CO₂ Reduction Summary

A summary of all stages of the energy demand assessment from baseline figures to final carbon reduction are shown in Figures 1 & 2 below:

Summary of CO ₂ Emission Reductions	Total CO ₂ emissions (kgCO ₂ /year)		
Carbon Factors (Gas / Electric)	0.216 / 0.519	0.210 / 0.233	0.210 / 0.136
Baseline emissions	82188.9	50030.1	48434.6
Improved emissions (after application of energy efficiency measures) - residual emissions	71235.1	31980.3	18666.6
Improved emissions (after incorporation of efficient energy supply)	71190.2	31960.2	18654.9
Improved emissions (after incorporation of renewable energy technology) % CO ₂ displaced in total	71190.2	31960.2	18654.9
% CO ₂ displaced in total	13.4%	36.1%	61.5%
% CO ₂ displaced by energy efficiency measures	13.3%	36.1%	61.5%
% CO ₂ displaced by efficient supply of energy	0.06%	0.06%	0.06%
% CO ₂ displaced by renewable energy	0.0%	0.0%	0.0%

Table 2: Summary of CO₂ Reductions



	Energy demand (kWh pa)	Energy saving achieved (%)	Regulated CO ₂ emissions (kg pa)	Saving achieved on residual CO ₂ emissions (%)
Building Regulations Part L compliance (“Baseline” energy demand & emissions)	236437.2		82188.9	
Proposed scheme after energy efficiency measures (“Residual” energy demand & emissions)	137254.6	41.9%	71235.1	13.3%
Proposed scheme after clean energy supply	137168.1	0.1%	71190.2	0.1%
Proposed scheme after on-site renewables	137168.1	0.0%	71190.2	0.0%
Proposed scheme offset for financial contribution or other “allowable solution”			0	0
Total savings on residual emissions				0.0%

Table 3. Total Energy and Carbon Emissions Savings Based on SAP 9.0 Carbon Factors



For a full Breakdown of the figures and calculations please see Appendix A – Energy Demand Assessment Spreadsheet.

Baseline energy demand

‘Standard Assessment Procedure - SAP 2012’ was used to produce example SAP reports to generate the figures used within the calculations.

Baseline energy demand (kWh pa)	236437.2
Baseline carbon emissions (kg pa)	82188.9

Be Lean stage

The following table demonstrates how the development achieves the reduction in carbon dioxide emissions from energy efficiency measures.

Energy savings from energy efficiency measures (kWh pa)	99182.6
Emission savings from energy efficiency measures (kg pa)	10953.8
Total regulated emissions after CHP savings and energy efficiency measures (kg pa) (“residual emissions”)	71235.1

Be Clean stage

The heating and cooling hierarchy has been applied to the design process of the development. It has resulted in large focus on energy efficiency measures and as can be seen in Figure 1.

Energy savings from the use of CHP systems (kWh pa)	-
Emission savings from the use of CHP systems (kg pa)	-
Total regulated emissions after CHP savings (kg pa)	71190.2

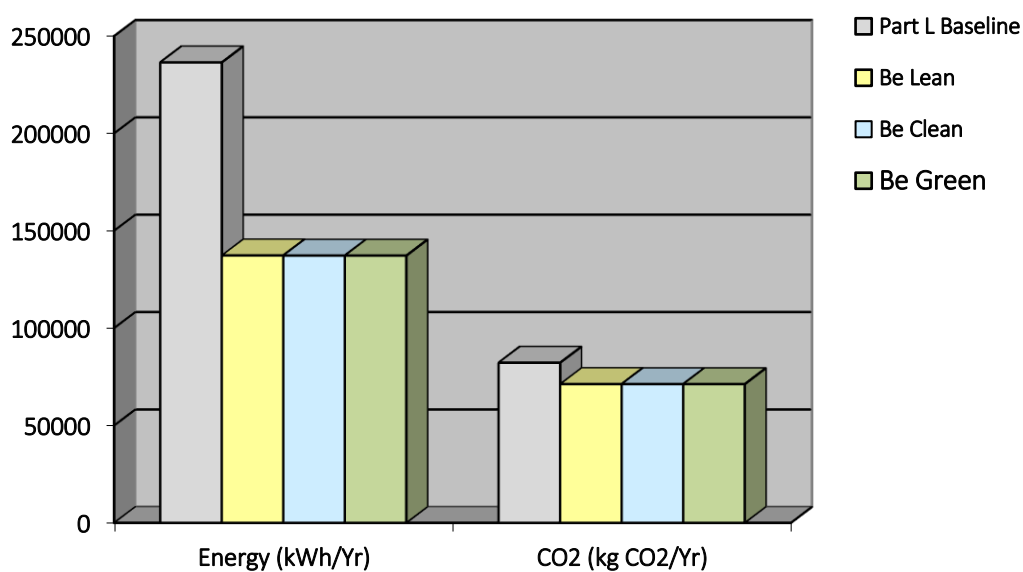


Be Green stage

The following table demonstrates how the development achieves the reduction in carbon dioxide emissions from LZC technologies.

Energy saving from the use of renewables (kWh)	-
Saving on residual emissions from the use of renewables (kg)	-
Saving on residual emissions from the use of renewables (%)	-

The chart below illustrates the improvements over the Part L Compliant Baseline:



2.3.4 Manchester City Council' Policy and Targets Summary

With regards to the Manchester City Council's planning documents policy and targets (outlined in section 2.2.1 to 2.2.3) the table below details how the Sustainable Design Strategy (outlined in section 2.3.1) achieves the current planning policy requirements and targets.

Planning Document:	Sustainable Design Strategy
Manchester Council's Core Strategy 2012-2027	The Sustainable Design Strategy achieves a 13.4% reduction in carbon emissions over Part L 2013 - exceeding the EN6 documents Low Carbon target of 9% over Part L 2013.
Climate Change and Low Emission Strategies 2016-2020	The Sustainable Design Strategy achieves a 13.4% reduction in carbon emissions over Part L 2013 – exceeding the documents Low Carbon target of 48% over 1990 Emissions.
Manchester: A Certain Future	The Sustainable Design Strategy achieves a 13.4% reduction in carbon emissions over Part L 2013 – exceeding the documents Low Carbon target of 10% over Part L 2013.

Table 4. Summary of MCC and Planning Targets

As a result of the sustainable design parameters outlined within section 2.3.1 and the energy and CO2 reduction figures summarised above, the development of 36 new residential dwellings at the Former VASA Club site achieves a total reduction of **13.4%** in carbon emissions over Part L 2013.

The low carbon classification for the Former VASA Club development can be derived from its prioritisation of fabric first carbon reduction through exceeding Building Regulation design standards.

2.4 Adaptation to Climate Change

In addition to the primary building design and fabric, many other issues that will influence creating a Sustainable Development, including flood prevention, material use, waste minimisation and transport. All these issues feature regularly within the separate climate change action plans, outlined within section 2.2, as areas that Manchester is aiming to significantly improve on in order to become a more carbon neutral and clean city.

All the sections of creating a sustainable development should be taken into consideration from the start of the development and promoted throughout the building construction on site in order to maximise their benefits. Additionally, features which enable more efficient usage should also be specified to encourage the building users to maintain efficient use once construction has been completed.

2.4.1 Flood Risk Zone

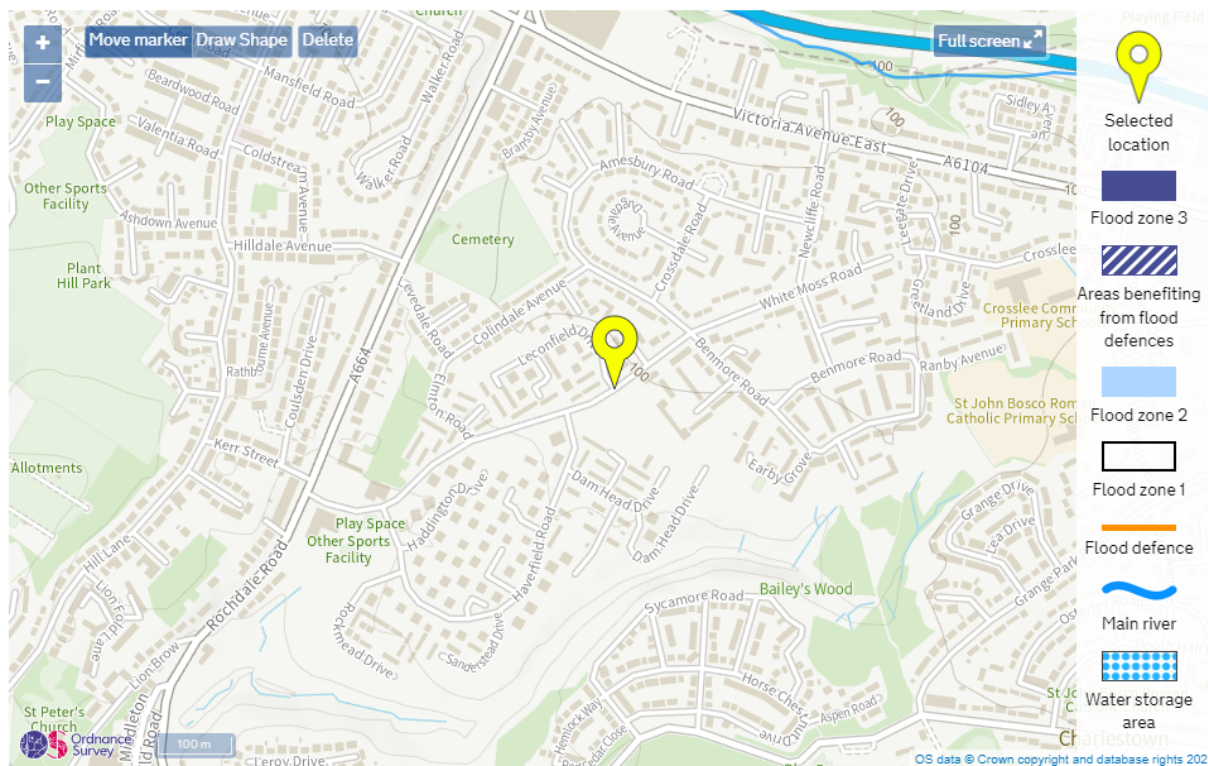


Fig 4: Flood Risk Map

The above map and snippet have been taken from a Government licenced flood risk map for Manchester. It can be seen that the site is just located within flood risk zone 1 and therefore has minimal to no risk of flooding.

2.4.2 Green Blue Infrastructure

2.4.2.1 Sustainable Drainage Systems (SUDs)

Even though it has been shown that the proposed scheme is located on a site with a low to zero flood risk, it should still be ensured that the levels of surface water run-off do not increase from the existing development to the proposed, especially due to the new scheme having a different footprint and potentially resulting in new areas of impermeable surfacing. Therefore, a drainage strategy assessment should be undertaken, by a suitably qualified professional, to assess the feasibility of introducing on-site SUDs measures, that will reduce surface water run-off and any flood risks associated.

By incorporating SuDs, flood risk can be managed and mitigated. Section 1.1 of the SuDs Manual (Ciria C753) states the following:

“Sustainable drainage systems (SuDs) can deliver multiple benefits.

Surface water is a valuable resource, and this should be reflected in the way it is managed and used in the built environment. It can add to and enhance biodiversity, beauty, tranquillity and the natural

aesthetic of buildings, places and landscapes and it can help make them more resilient to the changing climate.”

The general concept of SUDs is to manage the flood and pollution risks in developed areas. This is done by efficiently managing surface water run-off by either slowing down the surface water run-off, or by reducing the quantity of surface water run-off. There are different methods to achieve this such as:

- Harvesting – capturing rainwater and facilitate its use within the development
- Infiltrating – rainwater infiltrates into the ground
- Storing – capturing rainwater and control the flow through the means of storing and releasing it slowly i.e. attenuation
- Conveying & treating – capturing rainwater and removing any contaminants, then convey the flow towards a downstream system

The SuDS Manual describes the four pillars of SuDS design as Water Quality, Water Quantity, Amenity and Biodiversity as illustrated in Figure 3 below:

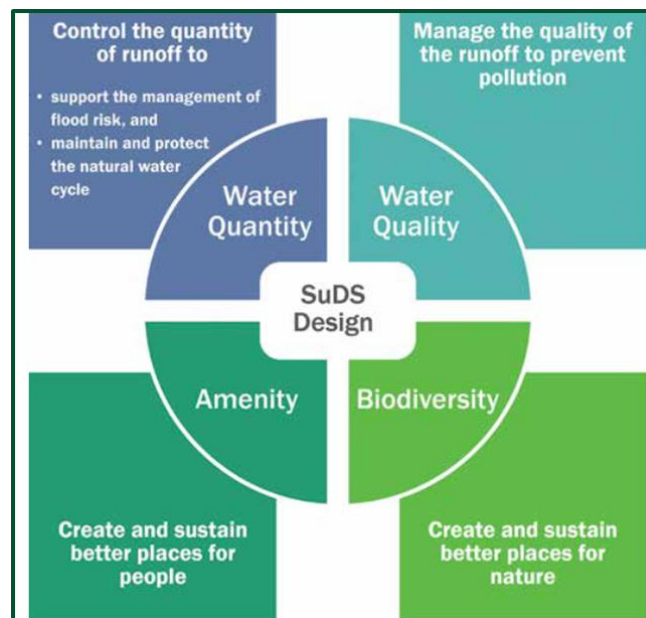


Fig 5. Representation of figure 2.1 of the SUDs Manual

SuDS are increasingly gaining popularity as a holistic solution to a wide range of pressing issues including flood risk, water pollution, groundwater depletion, biodiversity loss and urban decline.

Drainage Hierarchy

To alleviate pressure on existing sewer networks and to address issues of climate change the following hierarchy has been developed and implemented from a planning perspective.

The Planning Practice Guidance, states that:

“generally, the aim should be to discharge surface run-off as high up the following hierarchy of drainage options as reasonable practicably:

1. *Into the ground (infiltration)*
2. *To a surface water body*
3. *To a surface water sewer*
4. *To a combined sewer”*

The “Building Regulations Approved Document H” refer to this discharge hierarchy.

Description	Benefit
Flood risk management	SuDS aim to have an attenuating affect by slowing down and storing surface water run-off
Drainage resilience	Future proofing designed to be resilient against climate change
Natural flow regime protection	Mimic natural drainage arrangements to emulate natural flow
Water quality	Filter out pollutants and discharge cleaner water
Water reuse	Can be strategically placed to clean and capture water for reuse
Biodiversity and ecology	SuDS use vegetation and natural landscape to support biodiversity and ecology
Amenity	Improve visual integrity and desirability of the site by implementing green and blue features
Carbon reduction	SuDS can reduce carbon use throughout the life cycle including construction, maintenance, and demolition
Microclimate	Aim in reducing heat island effects
Education	Educate and engage the general public about surface water management

Table 5. Outline of types of green/blue infrastructure and associated benefit



2.4.2.2 Biodiversity

Similarly, to the previous section on SUDs, the nature of the proposal: including the demolishing of an existing building and potential change in area of impermeable surface, there could be adverse impacts on the surrounding ecology as well potential for the enhancement. Therefore, an ecology report should be produced, by a suitably qualified professional, in order to ensure that any existing ecology on or near the site is adequately protected and to determine the possibility of new habitat creation, planting schemes, green wall areas.

2.4.3 Internal Water Efficiency

Part G of the Building Regulations requires all new dwellings to have an internal water consumption of no greater than 110 litres / person / day, unless specified to be less. Therefore, fittings proposed should have low flow rates, capacities, effective flush volumes etc. Example targets for these to achieve the required internal consumption are as follows:

Appliance	Unit of measure	Amount (litres)
WC (Dual flush)	Full flush volume	4
WC (Dual flush)	Part flush volume	2.6
Taps (excluding kitchen)	Flow rate l/min	5
Kitchen taps	Flow rate l/min	6
Bath	Capacity to Overflow	170
Shower	Flow rate l/min	8
Washing Machine	Litres / kg dry load	8.17
Dishwasher	Litres / place setting	1.25

Table 6. Internal Water Efficiency Flow Rates

The above rates will achieve a total internal water consumption of 106.31 with a bath present and 98.25 with only a shower present.

The specifying of 'A' rated appliances should be prioritised where possible.

2.4.4 Waste Management

2.4.4.1 Occupational Waste

Manchester City Council's Waste Storage and Collection Guidance for New Developments 2017 encourages all new developments to incorporate a waste management strategy into the build at the earliest stage possible.

2.4.4.2 Construction Waste

A target of at least 90% of waste generated on site, throughout the construction stage of the development, to be diverted from landfill' will be included as part of a Construction Environmental Management Plan (CEMP) to be agreed with MCC.

The proposal will also endeavour to maximise the use of recycled materials on site, whereby further promoting the minimising of waste production.

2.4.5 Materials

The construction of new buildings and building elements has a large environmental impact in terms of both, energy, and embodied carbon of new materials. Therefore, Manchester City Council promote the prioritising of environmentally friendly materials, where possible, and encourages the use of recycled building materials. This information should also be incorporated into the SWMP mentioned in the previous subsection (Waste Management) as a means of promoting the re-using and recycling of materials.

Where new materials are to be used, careful consideration of their environmental impact should be taken. This can be achieved by ensuring that only materials that score well under The Green Guide to Specification. This useful online tool can be used as a reference that provides guidance on the relative environmental impacts for a wide range of different building specifications. The BRE's Environmental Profile Methodology determines the Life Cycle Assessment (LCA) of materials, which is what the Guide's specifications are based on.

In order to take full advantage of low impact materials, elements key to the scheme should be specified to achieve ratings of between A+ and C under The Green Guide's ratings. Insulation materials that are specified will also have a global warming potential (GWP) of 5 or less, with an ODP of 0. Additionally, 100% of all timber used as part of the scheme will be responsibly sourced from suppliers that are either Forest Stewardship Council (FSC) accredited, Programme for the Endorsement of Forestry Certification accredited, or a similar recognised accreditation body.

To further promote embodied energy and carbon savings, the scheme will first prioritise the reusing of any demolished materials within the site, however if this is not possible secondary priority must be given to the redirecting from landfill, in line with the waste hierarchy.

Finally, in addition to the above policy points, the development is also recommended to register with the Considerate Constructors Scheme, or a similar approved scheme.

2.4.6 Pollution Control

To reduce emissions of gases with high global warming potential (GWP) and nitrogen oxide (NOx) into the atmosphere, new buildings will be specified with insulating materials that have a GWP of less than 5. This will follow throughout the development to reduce the impact that the construction phase has upon climate change.

Additionally, the following measures will be implemented:

- Pollution Prevention Guidance will be adhered to in respects of air (dust) and water (ground and surface) pollution during the demolition and construction phase.
- External light fittings will be controlled through a time switch, or daylight sensor, to prevent operation during daylight hours to limit the impact of artificial lighting for the development's residents and surrounding environment.
- Dust suppression measures will also be put in place as part of the Main Contractor's Environmental Management Plan, this will reduce the potential risk to local watercourses (River Irk) and neighbouring properties.

Sound insulation will be specified to achieve Building Regulation Part E compliance standard (this will be verified by pre-completion testing) in addition to meeting the requirements of the council. This will reduce the impact of sound pollution for the occupants within adjoining dwellings.

2.4.7 Health and Wellbeing

The following measures will also be incorporated:

- Efficient MVHR Units are to be specified to each individual dwelling which will provide a continuous source of fresh, filtered air to maintain a healthy indoor environment.
- Enhancing the green infrastructure of the site by introducing planting wherever possible, therefore improving the physical and mental wellbeing of residents, visitors, and workers.
- Secure by Design accreditation will be sought which will incorporate the adoption of crime prevention measures to further prevent crime and promote a safe environment.

The above findings and technology will all help to promote healthy housing for residents which has been identified by the World Health Organisation (WHO) as an increasingly important factor in increasing quality of life, preventing disease and illness, and mitigating climate change.

2.4.8 Sustainable Transport

A key message from all climate change adaptation plans (as mentioned in section 2.2), specifically Our Manchester Strategy 2016-2025, The Zero Carbon Framework (formulated by the Manchester Climate Change Board) and Manchester City Council's Core Strategy 2012-2027, is the need to increase the proportion of cycling, walking and public transport journeys. This is due to it providing both environmental and social benefits through the reducing of emissions, improving air quality, and promoting a more active lifestyle.

The proposed development acknowledges the benefits associated with these forms of sustainable transport and is therefore providing a cycle store to the rear of each dwelling, and although car parking is included, electric vehicle charging points will be provided, thereby encouraging all residents to commute in a sustainable manner.

Further to providing cycle provision, the site is bounded to White Moss Road, which has several bus stops and is a five-minute walk to Rochdale Road which has regular buses to Manchester City centre. This proximity to several transport nodes with such a range of travel possibilities further reduces the reliance on cars and the negative environmental impacts associated.

Transport Links

- **Train:** The closest train station to the site is Moston Train Station, which is located approximately Piccadilly Train Station, which is located approximately 1.64 miles southeast of the site. This station provides access to Manchester stations where regional and national destinations can be accessed.
- **Bus:** The nearest bus stop is adjacent to the site, located on White Moss Road, providing frequent services north towards Middleton. The site is also located 508 ft from the bus stop on Rochdale Road which provide frequent services to Manchester City Centre; where further buses can be caught to more regional destinations.
- **Metrolink:** The closest Metrolink station to the site is Boker Vale, which is located approximately 1.59 miles southwest of the site. This provides an additional means of public transport to locations within central Manchester, Manchester Airport and also further afield to Altrincham, Bury, Eccles, East Didsbury, Rochdale, Ashton-Under-Lyne and Manchester Airport.

Local Amenities

- Boggart Hole Clough Recreation Area is situated 861 metres from the site; providing a recreational space for residents.
- The site is also adjacent to Rochdale Road where a multitude of shops and amenities can be accessed.
- Due to its proximity to Central Manchester, the site has good access to music, theatre and art venues, places of religion and Manchester's City Library.

3 Feasibility Assessment of Renewable Energy and Low Carbon Technologies

Solar Hot Water (Thermal)

Solar water heating systems are one of the more familiar renewable technologies used at the moment. They use the energy from the sun to heat water, most commonly for hot water needs. Solar heating systems use a heat collector that is usually mounted on a roof in which the sun heats a fluid. This fluid is used to heat water that is stored in either a separate hot water cylinder or in a twin-coil hot water cylinder (the second coil is used to provide additional heating from a boiler or other heat source).

Solar hot water panels could be used however, PV will provide slightly better savings and avoid the need for water storage cylinders when compared.

Renewable Technology Not Chosen.

Photovoltaic Panels (PV)

Photovoltaic modules convert sunlight directly to DC electricity. The solar cells consist of a thin piece of semiconductor material, in most cases of silicon. Through a process called doping, very small amounts of impurities are added to the semiconductor, which creates two different layers called n-type and p-type layers.

Certain wavelengths of light are able to ionize the silicon atoms, which separates some of the positive charges (holes) from the negative charges (electrons). The holes move into the positive or p-layer and the electrons into the negative or n-layer. These opposite charges are attracted to each other, but most of them can only re-combine by the electrons passing through an external circuit, due to an internal potential energy barrier. This flow of electrons produces a DC current.

A PV array could be mounted on the suitable roof space however, as previously mentioned the development is already achieving the required reduction through efficient design measures

Renewable Technology Not Chosen.

Ground Source Heat pumps

A heat pump is a device that takes up heat at a certain temperature and releases it at a higher temperature. The essential components of a heat pump are heat exchangers (through which energy is extracted and emitted) and a means of pumping heat between the exchangers. The effectiveness of the heat pump is measured by the ratio of the heating capacity to the effective power input, usually known as the coefficient of performance (COP). Ground-source heat pumps (GSHP) extract heat from the ground. They are classified as either water-to-air or water-to-water units depending on whether the heat distribution system in the building uses air or water. Ground source heat pumps either use long shallow trenches or deep vertical boreholes to take low grade heat from the ground and then compress it to create higher temperatures.

Ground source heat pumps would not be suitable due to the lack of land space around the properties and the associated costs.

Renewable Technology Not Viable

Air Source Heat pumps

Air source heat pumps absorb heat from the outside air. This is usually used to heat radiators, underfloor heating systems, or warm air convectors and hot water in your home. An air source heat pump extracts heat from the outside air in the same way that a fridge extracts heat from its inside.

The system performs down to air temperatures of -20°C which means that they are more than suitable for installations within the UK. Hot water and Heating can be provided 365 days a year. The hot water is produced without the aid of electrical immersions and at 55°C is more than hot enough for baths and showers.

There are two main types of air source heat pump system:

- An air-to-water system distributes heat via your wet central heating system. Heat pumps work much more efficiently at a lower temperature than a standard boiler system would. So they are more suitable for under-floor heating systems or larger radiators, which give out heat at lower temperatures over longer periods of time.
- An air-to-air system produces warm air which is circulated by fans to heat your home. They are unlikely to provide you with hot water as well.

Air Source heat pumps are a good option to provide heating and cooling however, as previously mentioned the development is already achieving the required reduction through efficient design measures.

Renewable Technology Not Chosen

Biomass Heating

Biomass is any plant-derived organic material that renews itself over a short period.

Biomass energy systems are based on either the direct or indirect combustion of fuels derived from those plant sources. The most common form of biomass is the direct combustion of wood in treated or untreated forms. The use of biomass is becoming increasingly common in some European countries.

The environmental benefits relate to the significantly lower amounts of energy used in biomass production and processing compared to the energy released when they are burnt. This can range from a four-fold return for biodiesel to an approximate 20-fold energy return for woody biomass. Biomass-fuels can be used to produce energy on a continuous basis (unlike renewables such as wind or solar energy) and it can be an economic alternative to fossil fuels as it is a potential source of both heat and electricity.

However, Biomass systems have particular design management and maintenance requirements associated with sourcing, transportation and storage and are therefore more commonly used in commercial developments rather than domestic installations. It can be less convenient to operate than mains-supplied fuels such as natural gas and are more management intensive and require expertise in facilities management. Sources of biomass can also fluctuate, so boilers should be specified to operate on a variety of fuels without risk of overheating or tripping out.

A communal biomass system would not be feasible for this development due to the expense associated with the necessary output to heat all dwellings on the site.

Renewable Technology Not Chosen

Wind

Wind turbines convert the kinetic energy in wind into mechanical energy that is then converted to electricity. Turbines are available in a range of sizes and designs and can either be free-standing, mounted on a building or integrated into a building structure.

The wind speed in the area is under the advised minimum and the built-up area means that a wind turbine wouldn't be feasible.

Renewable Technology Not Viable

4 Conclusion

This statement has assessed the proposed development at the former VASA Club site against the relevant climate change and sustainability policies and targets, as outlined within: the Manchester City Council Core Strategy (July 2012), Our Manchester Strategy, Manchester: A Certain Future and The Zero Carbon Framework, through the following of the energy hierarchy, the modelling of apartments in the FSAP 2012 software and addressing all aspects of a sustainable development. In addition, the proposal has been assessed against national sustainable design definitions to determine how it can be classified.

As part of this process, the development was designed with a fabric first approach; with U-values, design air permeability and ventilation targets all aspiring to exceed Building Regulations Part L 2013 standards. Following on from this, efficient MVHR systems were proposed for each apartment and house, to further reduce the total energy demands whilst simultaneously providing each dwelling with healthy internal environments. This approach demonstrates a holistic low energy design concept, involving very low limiting values and thus led to high-energy performance targets and being defined as a low carbon development.

Furthermore, an LZC feasibility assessment was carried out, with all suitable technologies investigated for their suitability to the site and development. Although feasible, the “fabric-first” approach satisfies all of the MCC carbon targets bringing the total carbon reduction to 13.4% when using SAP 9.0 carbon factors. However, this reduction rises further to **36.1%** and **61.5%** when using SAP 10 and 10.1 carbon factors. In addition, the development can also be defined as carbon neutral because it will have net zero carbon emissions. This is to be achieved by obtaining all the energy used on site from a 100% renewable energy electricity supply provider.

The development will also be adapting to climate change by incorporating sustainable drainage measures into the design, protecting existing ecology, enhancing biodiversity where possible and providing cycle storage provision and electric vehicle charging stations to residents.

In addition to the following of the energy hierarchy through the efficient design and renewable technology measures mentioned and meeting all relevant Manchester City Council carbon targets the proposal will include many sustainability measures throughout construction and once completed, which will contribute heavily to the development’s sustainability performance and accord with the requirements of the NPPF. The key measures to be included and therefore can be taken from this report include:

- The proposal sits within Flood Risk Zone 1 and therefore has minimal to no risk of flooding.
- A SUDs strategy will be produced to outline all measures to be incorporated that will ensure any additional surface water is collected, treated and removed.
- The development will incorporate green infrastructure in the form of extensive planting involving hedges, trees and ornamental planting that will instil a sense of wellbeing whilst also assisting with offsetting carbon dioxide and balancing local temperatures through evapotranspiration.

- Internal water efficiency will be prioritised by ensuring that efficient water fixtures are proposed so that each dwelling achieves less than 110L per person per day and 'A' rated appliances will be specified where possible.
- Waste minimisation will be targeted from throughout construction and occupational phase. It is targeted that at least 90% of construction waste will be diverted from landfill.
- In addition to targeting Secure by Design accreditation through adoption crime prevention measures, the site layout promotes busy spaces and routes and facilitates natural surveillance. These will therefore reduce the fear of crime and subsequently improving mental health of residents, visitors and workers.
- Prioritising reusing existing materials and locally sourced materials for construction to reduce waste and transportation to landfill in addition and promote a low embodied carbon development.
- When new materials are specified that are not locally attainable then only those that score well on the BRE: The Green Guide to Specification are to be used; to further encourage the use of sustainable materials and reductions in embodied carbon.
- The buildings will have a daylight and sunlight analysis carried out and will aim to achieve high pass rates. Additionally, highly efficient MVHR systems are being proposed to each flat individually to provide a continuous source of fresh air and maintain healthy indoor environments. These will promote healthy housing and subsequently boost physical and mental wellbeing of residents.
- The proximity of the Manchester City Centre to the proposed site is highly sustainable in terms of transport and local amenities as it is near a number of public transport nodes including Boker Vale Metrolink and Moston Train station, multiple bus stops as well as a multitude of shops and other local amenities.
- The development will also include significant cycle storage provision and electric vehicle charging stations.

As a result of all the above, the proposed sustainable design and energy strategy allows the development to comply with Manchester City Council's planning policy requirement and is in line with all targets put forward in their planning documents.

House Type/Name	Plot 1 Type 3A End Tce	Plot 2 Type 3A Mid Tce	Plot 3-7 Type 1A Mid Tce x3	Plot 3-7 Type 2A Mid Tce x3	Plot 9 Type 1A End Tce	Plot 10 Type 2A End Tce	Plot 11 Type 1B End Tce	Plot 12 Type 2B End Tce	Plot 13-17 Type 1B Mid Tce x3	Plot 14-18 Type 2B Mid Tce x3
Frequency	1	1	3	3	1	1	1	1	3	3
BASELINE Dwelling Emission Rate (DER)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)
Main Heating Fuel Requirement (DER)	5501.32	4405.39	1051.99	3059.4	1532.71	3682.62	1552.93	4221.29	1329.66	2992.36
Secondary Main Heating Fuel Requirement (DER)	0	0	0	0	0	0	0	0	0	0
Secondary Heating Fuel Requirement (DER)	0	0	0	0	0	0	0	0	0	0
Water Fuel Requirement (DER)	2663.47	2676.52	1870.22	2454.54	1854.05	2444.4	1853.57	2437.02	1860.2	2456.58
Electricity Pumps Fans Requirement (DER)	75	75	75	75	75	75	75	75	75	75
Electricity Lighting Requirement (DER)	477.47	477.47	178.67	359.38	178.67	358.33	178.67	358.37	178.67	358.37
TOTAL PER DEVELOPMENT										
AFTER ENERGY SAVING MEASURES Dwelling Emission Rate (DER)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)
Main Heating Fuel Requirement (DER)	2500.77	1704.75	298.63	958.63	565.42	1382.57	555.26	1746.35	496.34	805.63
Secondary Main Heating Fuel Requirement (DER)	0	0	0	0	0	0	0	0	0	0
Secondary Heating Fuel Requirement (DER)	0	0	0	0	0	0	0	0	0	0
Water Fuel Requirement (DER)	1941.25	1941.25	1242.77	1754.58	1242.77	1754.58	1242.77	1754.58	1242.77	1754.58
Electricity Pumps Fans Requirement (DER)	428.02	428.02	86.52	253.21	86.52	253.21	86.52	269.09	86.52	269.09
Electricity Lighting Requirement (DER)	490.13	490.13	178.67	364.92	178.67	361.61	178.67	358.37	178.67	360.39
TOTAL PER DEVELOPMENT										
FINAL Dwelling Emission Rate (DER)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)
Main Heating Fuel Requirement (DER)	2500.77	1704.75	298.63	958.63	565.42	1382.57	555.26	1746.35	496.34	805.63
Secondary Main Heating Fuel Requirement (DER)	0	0	0	0	0	0	0	0	0	0
Secondary Heating Fuel Requirement (DER)	0	0	0	0	0	0	0	0	0	0
Water Fuel Requirement (DER)	1941.25	1941.25	1242.77	1754.58	1242.77	1754.58	1242.77	1754.58	1242.77	1754.58
Electricity Pumps Fans Requirement (DER)	428.02	428.02	86.52	253.21	86.52	253.21	86.52	269.09	86.52	269.09
Electricity Lighting Requirement (DER)	490.13	490.13	178.67	364.92	178.67	361.61	178.67	358.37	178.67	360.39
TOTAL PER DEVELOPMENT										
PV Energy Produced (DER)										
TOTAL PER DEVELOPMENT										



Plot 192023 Type 4A Mid Tce x3	Type 3A Mid Tce x8	Plot 24252829323336 Type 4A End Tce x7	TOTAL (kWh/yr)		TOTAL (kgCO2/yr)	SAP 10.0	TOTAL (kgCO2/yr)	SAP 10.1	TOTAL (kgCO2/yr)
3	8	7	63						
Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Carbon Emission Factor	Associated Total CO2 (kgCO2/yr)	Carbon Emission Factor	Associated Total CO2 (kgCO2/yr)	Carbon Emission Factor	Associated Total CO2 (kgCO2/yr)
4507.99	4274.59	5373.41	131531.1	0.216	44036.6	0.210	27621.5	0.210	27621.5
0	0	0	0.0	0.519	0.0	0.233	0.0	0.136	0.0
0	0	0	0.0	0.216	0.0	0.210	0.0	0.136	0.0
2725.37	2678.39	2714.44	88458.0	0.216	29615.7	0.210	18576.2	0.210	18576.2
75	75	75	2700.0	0.519	1401.3	0.233	629.1	0.136	367.2
471.69	477.47	465.58	13748.1	0.519	7135.3	0.233	3203.3	0.136	1869.7
			236437.2		82188.9		50030.1		48434.6
Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Carbon Emission Factor	Associated Total CO2 (kgCO2/yr)	Carbon Emission Factor	Associated Total CO2 (kgCO2/yr)	Carbon Emission Factor	Associated Total CO2 (kgCO2/yr)
1546.06	1609.15	2151.86	48707.2	0.519	25279.0	0.233	11348.8	0.136	6624.2
0	0	0	0.0	0.519	0.0	0.233	0.0	0.136	0.0
0	0	0	0.0	0.519	0.0	0.233	0.0	0.136	0.0
1971.87	1941.25	1971.87	63110.0	0.519	32754.1	0.233	14704.6	0.136	8583.0
402.87	428.02	451.22	11428.7	0.519	5931.5	0.233	2662.9	0.136	1554.3
483.86	490.13	475.79	14008.7	0.519	7270.5	0.233	3264.0	0.136	1905.2
			137254.6		71235.1		31980.3		18666.6
Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Total Energy Demand (kWh/yr)	Carbon Emission Factor	Associated Total CO2 (kgCO2/yr)	Carbon Emission Factor	Associated Total CO2 (kgCO2/yr)	Carbon Emission Factor	Associated Total CO2 (kgCO2/yr)
1546.06	1609.15	2151.86	48707.2	0.519	25279.0	0.233	11348.8	0.136	6624.2
0	0	0	0.0	0.519	0.0	0.233	0.0	0.136	0.0
0	0	0	0.0	0.519	0.0	0.233	0.0	0.136	0.0
1971.87	1941.25	1971.87	63110.0	0.519	32754.1	0.233	14704.6	0.136	8583.0
402.87	428.02	451.22	11342.2	0.519	5886.6	0.233	2642.7	0.136	1542.5
483.86	490.13	475.79	14008.7	0.519	7270.5	0.233	3264.0	0.136	1905.2
			137168.1		71190.2		31960.2		18654.9
			0.0	0.519	0.0	0.233	0.0	0.136	0.0
			137168.1		71190.2		31960.2		18654.9



Regulations Compliance Report

Approved Document L1A, 2013 Edition, England assessed by Stroma FSAP 2012 program, Version: 1.0.5.51
Printed on 10 February 2022 at 14:52:43

Project Information:

Assessed By: Daniel Watt (STRO026464)

Building Type: End-terrace House

Dwelling Details:

NEW DWELLING DESIGN STAGE

Total Floor Area: 127.28m²

Site Reference : VASA Club

Plot Reference: Plot 1 Type 3A End Tce

Address : VASA Club, 283 White Moss Rd, Manchester, M9 6NZ

Client Details:

Name:

Address :

This report covers items included within the SAP calculations.

It is not a complete report of regulations compliance.

1a TER and DER

Fuel for main heating system: Electricity

Fuel factor: 1.55 (electricity)

Target Carbon Dioxide Emission Rate (TER) 23.73 kg/m²

Dwelling Carbon Dioxide Emission Rate (DER) 21.86 kg/m² **OK**

1b TFEE and DFEE

Target Fabric Energy Efficiency (TFEE) 53.6 kWh/m²

Dwelling Fabric Energy Efficiency (DFEE) 37.7 kWh/m² **OK**

2 Fabric U-values

Element	Average	Highest	
External wall	0.15 (max. 0.30)	0.15 (max. 0.70)	OK
Party wall	0.00 (max. 0.20)	-	OK
Floor	0.10 (max. 0.25)	0.10 (max. 0.70)	OK
Roof	0.10 (max. 0.20)	0.13 (max. 0.35)	OK
Openings	0.81 (max. 2.00)	1.00 (max. 3.30)	OK

2a Thermal bridging

Thermal bridging calculated from linear thermal transmittances for each junction

3 Air permeability

Air permeability at 50 pascals 3.00 (design value)
Maximum 10.0 **OK**

4 Heating efficiency

Main Heating system: Room heaters - electric
Panel, convector or radiant heaters

Secondary heating system: None

5 Cylinder insulation

Hot water Storage: Measured cylinder loss: 1.48 kWh/day
Permitted by DBSCG: 2.56 kWh/day **OK**
Primary pipework insulated: No primary pipework

Regulations Compliance Report

6 Controls

Space heating controls	Programmer and appliance thermostats	OK
Hot water controls:	Cylinderstat	OK

7 Low energy lights

Percentage of fixed lights with low-energy fittings	100.0%	
Minimum	75.0%	OK

8 Mechanical ventilation

Continuous supply and extract system		
Specific fan power:	0.71	
Maximum	1.5	OK
MVHR efficiency:	86%	
Minimum	70%	OK

9 Summertime temperature

Overheating risk (North West England):	Not significant	OK
Based on:		
Overshading:	Average or unknown	
Windows facing: North West	12.41m ²	
Windows facing: South East	9.38m ²	
Ventilation rate:	8.00	
Blinds/curtains:	Dark-coloured curtain or roller blind	
	Closed 100% of daylight hours	

10 Key features

Air permeability	3.0 m ³ /m ² h
Windows U-value	0.8 W/m ² K
Doors U-value	1 W/m ² K
Roofs U-value	0.1 W/m ² K
Party Walls U-value	0 W/m ² K
Floors U-value	0.1 W/m ² K

SAP Input

Property Details: Plot 1 Type 3A End Tce

Address: VASA Club, 283 White Moss Rd, Manchester, M9 6NZ
Located in: England
Region: North West England
UPRN:
Date of assessment: 10 February 2022
Date of certificate: 10 February 2022
Assessment type: New dwelling design stage
Transaction type: New dwelling
Tenure type: Unknown
Related party disclosure: Employed by the professional dealing with the property transaction
Thermal Mass Parameter: Indicative Value Medium
Water use <= 125 litres/person/day: True
PCDF Version: 490

Property description:

Dwelling type: House
Detachment: End-terrace
Year Completed: 2022
Floor Location: Floor area: Storey height:
 Floor 0 43.42 m² 2.6 m
 Floor 1 43.42 m² 2.8 m
 Floor 2 40.44 m² 2.93 m
Living area: 18 m² (fraction 0.141)
Front of dwelling faces: North West

Opening types:

Name:	Source:	Type:	Glazing:	Argon:	Frame:
Front Door	Manufacturer	Solid			Wood
Front	Manufacturer	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U
Rear	Manufacturer	Windows	low-E, En = 0.05, soft coat	Yes	PVC-U

Name:	Gap:	Frame Factor:	g-value:	U-value:	Area:	No. of Openings:
Front Door	mm	0.7	0	1	1.73	1
Front	16mm or more	0.7	0.72	0.8	12.41	1
Rear	16mm or more	0.7	0.72	0.8	9.38	1

Name:	Type-Name:	Location:	Orient:	Width:	Height:
Front Door		Walls	North West	0	0
Front		Walls	North West	0	0
Rear		Walls	South East	0	0

Overshading: Average or unknown

Opaque Elements:

Type:	Gross area:	Openings:	Net area:	U-value:	Ru value:	Curtain wall:	Kappa:
External Elements							
Walls	150.82	23.52	127.3	0.15	0	False	N/A
Sloped Ceiling	57.53	0	57.53	0.1	0		N/A
Flat Roof	2.88	0	2.88	0.13	0		N/A
Ground	43.42			0.1			N/A
Internal Elements							
Party Elements							
Party Walls	84						N/A

Thermal bridges:

SAP Input

Thermal bridges:

User-defined (individual PSI-values) Y-Value = 0.0584

	Length	Psi-value		
	10.94	0.03	E2	Other lintels (including other steel lintels)
[Approved]	8.16	0.04	E3	Sill
[Approved]	35	0.05	E4	Jamb
[Approved]	20.06	0.16	E5	Ground floor (normal)
[Approved]	38.06	0.07	E6	Intermediate floor within a dwelling
[Approved]	13	0.04	E11	Eaves (insulation at rafter level)
[Approved]	4.98	0.04	E13	Gable (insulation at rafter level)
	4.85	0.08	E14	Flat roof
	11	0.16	P1	Ground floor
	22	0	P2	Intermediate floor within a dwelling
	11.18	0.24	P4	Roof (insulation at ceiling level)
	13	0.08	R4	Ridge (vaulted ceiling)

Ventilation:

Pressure test:	Yes (As designed)
Ventilation:	Balanced with heat recovery
	Number of wet rooms: Kitchen + 3
	Ductwork: Insulation, rigid
	Approved Installation Scheme: False
Number of chimneys:	0
Number of open flues:	0
Number of fans:	0
Number of passive stacks:	0
Number of sides sheltered:	3
Pressure test:	3

Main heating system:

Main heating system:	Room heaters
	Electric (direct acting) room heaters
	Fuel: Electricity
	Info Source: SAP Tables
	SAP Table: 691
	Panel, convactor or radiant heaters
	Central heating pump : 2013 or later
	Design flow temperature: Design flow temperature<=45°C
	Unknown
	Boiler interlock: Yes

Main heating Control:

Main heating Control:	Programmer and appliance thermostats
	Control code: 2603

Secondary heating system:

Secondary heating system:	None
---------------------------	------

Water heating:

Water heating:	Electric immersion (on-peak or off-peak)
	Water code: 903
	Fuel :Electricity
	Hot water cylinder
	Cylinder volume: 250 litres
	Cylinder insulation: Measured loss, 1.48kWh/day
	Primary pipework insulation: False
	Cylinderstat: True
	Cylinder in heated space: True
	Immersion: Single
	Solar panel: False

SAP Input

Others:

Electricity tariff:	Standard Tariff
In Smoke Control Area:	Unknown
Conservatory:	No conservatory
Low energy lights:	100%
Terrain type:	Low rise urban / suburban
EPC language:	English
Wind turbine:	No
Photovoltaics:	None
Assess Zero Carbon Home:	No

SAP WorkSheet: New dwelling design stage

User Details:

Assessor Name: Daniel Watt **Stroma Number:** STRO026464
Software Name: Stroma FSAP 2012 **Software Version:** Version: 1.0.5.51

Property Address: Plot 1 Type 3A End Tce

Address : VASA Club, 283 White Moss Rd, Manchester, M9 6NZ

1. Overall dwelling dimensions:

	Area(m ²)		Av. Height(m)		Volume(m ³)
Ground floor	43.42 (1a)	x	2.6 (2a)	=	112.89 (3a)
First floor	43.42 (1b)	x	2.8 (2b)	=	121.58 (3b)
Second floor	40.44 (1c)	x	2.93 (2c)	=	118.49 (3c)
Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n)	127.28 (4)				
Dwelling volume				(3a)+(3b)+(3c)+(3d)+(3e)+.....(3n) =	352.96 (5)

2. Ventilation rate:

	main heating	secondary heating	other	total	m ³ per hour
Number of chimneys	0	+	0	=	0 (6a)
Number of open flues	0	+	0	=	0 (6b)
Number of intermittent fans				0 x 10 =	0 (7a)
Number of passive vents				0 x 10 =	0 (7b)
Number of flueless gas fires				0 x 40 =	0 (7c)

Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) =	0	÷ (5) =	0 (8)
<i>If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)</i>			
Number of storeys in the dwelling (ns)			0 (9)
Additional infiltration		[(9)-1]x0.1 =	0 (10)
Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction <i>if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35</i>			0 (11)
If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0			0 (12)
If no draught lobby, enter 0.05, else enter 0			0 (13)
Percentage of windows and doors draught stripped			0 (14)
Window infiltration	0.25 - [0.2 x (14) ÷ 100] =		0 (15)
Infiltration rate	(8) + (10) + (11) + (12) + (13) + (15) =		0 (16)
Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area			3 (17)
If based on air permeability value, then (18) = [(17) ÷ 20] + (8), otherwise (18) = (16)			0.15 (18)
<i>Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used</i>			
Number of sides sheltered			3 (19)
Shelter factor	(20) = 1 - [0.075 x (19)] =		0.78 (20)
Infiltration rate incorporating shelter factor	(21) = (18) x (20) =		0.12 (21)

Infiltration rate modified for monthly wind speed

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

Monthly average wind speed from Table 7

(22)m=	5.1	5	4.9	4.4	4.3	3.8	3.8	3.7	4	4.3	4.5	4.7
--------	-----	---	-----	-----	-----	-----	-----	-----	---	-----	-----	-----

SAP WorkSheet: New dwelling design stage

Wind Factor (22a)m = (22)m ÷ 4

(22a)m=	1.27	1.25	1.23	1.1	1.08	0.95	0.95	0.92	1	1.08	1.12	1.18
---------	------	------	------	-----	------	------	------	------	---	------	------	------

Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

	0.15	0.15	0.14	0.13	0.12	0.11	0.11	0.11	0.12	0.12	0.13	0.14
--	------	------	------	------	------	------	------	------	------	------	------	------

Calculate effective air change rate for the applicable case

If mechanical ventilation:

0.5 (23a)

If exhaust air heat pump using Appendix N, (23b) = (23a) × Fmv (equation (N5)) , otherwise (23b) = (23a)

0.5 (23b)

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

73.1 (23c)

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) × [1 – (23c) ÷ 100]

(24a)m= 0.28 0.28 0.28 0.26 0.26 0.24 0.24 0.24 0.25 0.26 0.27 0.27 (24a)

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

(24b)m= 0 0 0 0 0 0 0 0 0 0 0 0 (24b)

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 × (23b), then (24c) = (23b); otherwise (24c) = (22b) m + 0.5 × (23b)

(24c)m= 0 0 0 0 0 0 0 0 0 0 0 0 (24c)

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² x 0.5]

(24d)m= 0 0 0 0 0 0 0 0 0 0 0 0 (24d)

Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

(25)m= 0.28 0.28 0.28 0.26 0.26 0.24 0.24 0.24 0.25 0.26 0.27 0.27 (25)

3. Heat losses and heat loss parameter:

ELEMENT	Gross area (m²)	Openings m²	Net Area A ,m²	U-value W/m²K	A X U (W/K)	k-value kJ/m²·K	A X k kJ/K
Doors			1.73	x 1	= 1.73		(26)
Windows Type 1			12.41	x 1/[1/(0.8)+0.04]	= 9.62		(27)
Windows Type 2			9.38	x 1/[1/(0.8)+0.04]	= 7.27		(27)
Floor			43.42	x 0.1	= 4.342		(28)
Walls	150.82	23.52	127.3	x 0.15	= 19.1		(29)
Roof Type1	57.53	0	57.53	x 0.1	= 5.75		(30)
Roof Type2	2.88	0	2.88	x 0.13	= 0.37		(30)
Total area of elements, m²			254.65				(31)
Party wall			84	x 0	= 0		(32)

* for windows and roof windows, use effective window U-value calculated using formula 1/[(1/U-value)+0.04] as given in paragraph 3.2

** include the areas on both sides of internal walls and partitions

Fabric heat loss, W/K = S (A x U) (26)...(30) + (32) = 48.19 (33)

Heat capacity Cm = S(A x k) ((28)...(30) + (32) + (32a)...(32e) = 14637.89 (34)

Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m²K Indicative Value: Medium 250 (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f can be used instead of a detailed calculation.

Thermal bridges : S (L x Y) calculated using Appendix K 14.87 (36)

if details of thermal bridging are not known (36) = 0.05 x (31)

Total fabric heat loss (33) + (36) = 63.05 (37)

SAP WorkSheet: New dwelling design stage

Ventilation heat loss calculated monthly

$$(38)m = 0.33 \times (25)m \times (5)$$

(38)m=

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
32.93	32.59	32.25	30.56	30.22	28.53	28.53	28.19	29.21	30.22	30.9	31.58

(38)

Heat transfer coefficient, W/K

$$(39)m = (37) + (38)m$$

(39)m=

95.98	95.65	95.31	93.62	93.28	91.58	91.58	91.25	92.26	93.28	93.95	94.63
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

$$\text{Average} = \text{Sum}(39)_{1...12} / 12 =$$

93.53

(39)

Heat loss parameter (HLP), W/m²K

$$(40)m = (39)m \div (4)$$

(40)m=

0.75	0.75	0.75	0.74	0.73	0.72	0.72	0.72	0.72	0.73	0.74	0.74
------	------	------	------	------	------	------	------	------	------	------	------

$$\text{Average} = \text{Sum}(40)_{1...12} / 12 =$$

0.73

(40)

Number of days in month (Table 1a)

(41)m=

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
31	28	31	30	31	30	31	31	30	31	30	31

(41)

4. Water heating energy requirement:

kWh/year:

Assumed occupancy, N

2.89

(42)

if TFA > 13.9, $N = 1 + 1.76 \times [1 - \exp(-0.000349 \times (TFA - 13.9)^2)] + 0.0013 \times (TFA - 13.9)$

if TFA ≤ 13.9, N = 1

Annual average hot water usage in litres per day $V_{d,average} = (25 \times N) + 36$

102.78

(43)

Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

Hot water usage in litres per day for each month $V_{d,m} = \text{factor from Table 1c} \times (43)$

(44)m=

113.06	108.95	104.84	100.72	96.61	92.5	92.5	96.61	100.72	104.84	108.95	113.06
--------	--------	--------	--------	-------	------	------	-------	--------	--------	--------	--------

$$\text{Total} = \text{Sum}(44)_{1...12} =$$

1233.36

(44)

Energy content of hot water used - calculated monthly = $4.190 \times V_{d,m} \times n_m \times DT_m / 3600$ kWh/month (see Tables 1b, 1c, 1d)

(45)m=

167.66	146.64	151.32	131.92	126.58	109.23	101.22	116.15	117.54	136.98	149.52	162.37
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

$$\text{Total} = \text{Sum}(45)_{1...12} =$$

1617.13

(45)

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

(46)m=

25.15	22	22.7	19.79	18.99	16.38	15.18	17.42	17.63	20.55	22.43	24.36
-------	----	------	-------	-------	-------	-------	-------	-------	-------	-------	-------

(46)

Water storage loss:

Storage volume (litres) including any solar or WWHRS storage within same vessel

250

(47)

If community heating and no tank in dwelling, enter 110 litres in (47)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in (47)

Water storage loss:

a) If manufacturer's declared loss factor is known (kWh/day):

1.48

(48)

Temperature factor from Table 2b

0.6

(49)

Energy lost from water storage, kWh/year

$$(48) \times (49) =$$

0.89

(50)

b) If manufacturer's declared cylinder loss factor is not known:

Hot water storage loss factor from Table 2 (kWh/litre/day)

0

(51)

If community heating see section 4.3

Volume factor from Table 2a

0

(52)

Temperature factor from Table 2b

0

(53)

Energy lost from water storage, kWh/year

$$(47) \times (51) \times (52) \times (53) =$$

0

(54)

Enter (50) or (54) in (55)

0.89

(55)

Water storage loss calculated for each month

$$((56)m = (55) \times (41)m$$

(56)m=

27.53	24.86	27.53	26.64	27.53	26.64	27.53	27.53	26.64	27.53	26.64	27.53
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

(56)

SAP WorkSheet: New dwelling design stage

If cylinder contains dedicated solar storage, (57)m = (56)m × [(50) – (H11)] ÷ (50), else (57)m = (56)m where (H11) is from Appendix H

(57)m=

27.53	24.86	27.53	26.64	27.53	26.64	27.53	27.53	26.64	27.53	26.64	27.53
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

 (57)

Primary circuit loss (annual) from Table 3

0

 (58)

Primary circuit loss calculated for each month (59)m = (58) ÷ 365 × (41)m

(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat)

(59)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

 (59)

Combi loss calculated for each month (61)m = (60) ÷ 365 × (41)m

(61)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

 (61)

Total heat required for water heating calculated for each month (62)m = 0.85 × (45)m + (46)m + (57)m + (59)m + (61)m

(62)m=

195.19	171.5	178.85	158.56	154.11	135.87	128.75	143.68	144.18	164.51	176.16	189.9
--------	-------	--------	--------	--------	--------	--------	--------	--------	--------	--------	-------

 (62)

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)

(add additional lines if FGHRs and/or WWHRs applies, see Appendix G)

(63)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

 (63)

Output from water heater

(64)m=

195.19	171.5	178.85	158.56	154.11	135.87	128.75	143.68	144.18	164.51	176.16	189.9
--------	-------	--------	--------	--------	--------	--------	--------	--------	--------	--------	-------

Output from water heater (annual) ^{1...12}	1941.25
---	---------

 (64)

Heat gains from water heating, kWh/month $0.25 \times [0.85 \times (45)m + (61)m] + 0.8 \times [(46)m + (57)m + (59)m]$

(65)m=

77.77	68.65	72.34	65.18	64.11	57.63	55.68	60.64	60.39	67.57	71.03	76.01
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

 (65)

include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts

(66)m=

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
173.25	173.25	173.25	173.25	173.25	173.25	173.25	173.25	173.25	173.25	173.25	173.25

 (66)

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5

(67)m=

69.38	61.63	50.12	37.94	28.36	23.94	25.87	33.63	45.14	57.31	66.89	71.31
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

 (67)

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5

(68)m=

439.42	443.98	432.49	408.03	377.15	348.13	328.74	324.18	335.67	360.13	391.01	420.03
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

 (68)

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5

(69)m=

55.21	55.21	55.21	55.21	55.21	55.21	55.21	55.21	55.21	55.21	55.21	55.21
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

 (69)

Pumps and fans gains (Table 5a)

(70)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

 (70)

Losses e.g. evaporation (negative values) (Table 5)

(71)m=

-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

 (71)

Water heating gains (Table 5)

(72)m=

104.53	102.16	97.22	90.52	86.17	80.04	74.84	81.51	83.88	90.82	98.65	102.17
--------	--------	-------	-------	-------	-------	-------	-------	-------	-------	-------	--------

 (72)

Total internal gains = (66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m

(73)m=

726.3	720.73	692.8	649.46	604.65	565.08	542.41	552.28	577.65	621.23	669.52	706.47
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 (73)

6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

Orientation:	Access Factor Table 6d	Area m ²	Flux Table 6a	g_ Table 6b	FF Table 6c	Gains (W)
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SAP WorkSheet: New dwelling design stage

Southeast 0.9x	0.77	x	9.38	x	36.79	x	0.72	x	0.7	=	120.54	(77)
Southeast 0.9x	0.77	x	9.38	x	62.67	x	0.72	x	0.7	=	205.33	(77)
Southeast 0.9x	0.77	x	9.38	x	85.75	x	0.72	x	0.7	=	280.94	(77)
Southeast 0.9x	0.77	x	9.38	x	106.25	x	0.72	x	0.7	=	348.1	(77)
Southeast 0.9x	0.77	x	9.38	x	119.01	x	0.72	x	0.7	=	389.9	(77)
Southeast 0.9x	0.77	x	9.38	x	118.15	x	0.72	x	0.7	=	387.08	(77)
Southeast 0.9x	0.77	x	9.38	x	113.91	x	0.72	x	0.7	=	373.19	(77)
Southeast 0.9x	0.77	x	9.38	x	104.39	x	0.72	x	0.7	=	342	(77)
Southeast 0.9x	0.77	x	9.38	x	92.85	x	0.72	x	0.7	=	304.2	(77)
Southeast 0.9x	0.77	x	9.38	x	69.27	x	0.72	x	0.7	=	226.93	(77)
Southeast 0.9x	0.77	x	9.38	x	44.07	x	0.72	x	0.7	=	144.38	(77)
Southeast 0.9x	0.77	x	9.38	x	31.49	x	0.72	x	0.7	=	103.16	(77)
Northwest 0.9x	0.77	x	12.41	x	11.28	x	0.72	x	0.7	=	48.91	(81)
Northwest 0.9x	0.77	x	12.41	x	22.97	x	0.72	x	0.7	=	99.55	(81)
Northwest 0.9x	0.77	x	12.41	x	41.38	x	0.72	x	0.7	=	179.35	(81)
Northwest 0.9x	0.77	x	12.41	x	67.96	x	0.72	x	0.7	=	294.55	(81)
Northwest 0.9x	0.77	x	12.41	x	91.35	x	0.72	x	0.7	=	395.94	(81)
Northwest 0.9x	0.77	x	12.41	x	97.38	x	0.72	x	0.7	=	422.11	(81)
Northwest 0.9x	0.77	x	12.41	x	91.1	x	0.72	x	0.7	=	394.87	(81)
Northwest 0.9x	0.77	x	12.41	x	72.63	x	0.72	x	0.7	=	314.8	(81)
Northwest 0.9x	0.77	x	12.41	x	50.42	x	0.72	x	0.7	=	218.55	(81)
Northwest 0.9x	0.77	x	12.41	x	28.07	x	0.72	x	0.7	=	121.66	(81)
Northwest 0.9x	0.77	x	12.41	x	14.2	x	0.72	x	0.7	=	61.54	(81)
Northwest 0.9x	0.77	x	12.41	x	9.21	x	0.72	x	0.7	=	39.94	(81)

Solar gains in watts, calculated for each month

(83)m = Sum(74)m ... (82)m

(83)m=

169.45	304.88	460.3	642.65	785.84	809.19	768.06	656.8	522.75	348.59	205.92	143.1
--------	--------	-------	--------	--------	--------	--------	-------	--------	--------	--------	-------

 (83)

Total gains – internal and solar (84)m = (73)m + (83)m , watts

(84)m=

895.75	1025.6	1153.09	1292.11	1390.48	1374.27	1310.47	1209.08	1100.4	969.82	875.44	849.57
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 (84)

7. Mean internal temperature (heating season)

Temperature during heating periods in the living area from Table 9, Th1 (°C)

21

 (85)

Utilisation factor for gains for living area, h1,m (see Table 9a)

(86)m=

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
0.99	0.98	0.94	0.81	0.62	0.43	0.31	0.35	0.57	0.88	0.98	0.99

 (86)

Mean internal temperature in living area T1 (follow steps 3 to 7 in Table 9c)

(87)m=

20.43	20.58	20.76	20.94	20.99	21	21	21	21	20.91	20.64	20.41
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 (87)

Temperature during heating periods in rest of dwelling from Table 9, Th2 (°C)

(88)m=

20.29	20.3	20.3	20.31	20.31	20.32	20.32	20.33	20.32	20.31	20.31	20.3
-------	------	------	-------	-------	-------	-------	-------	-------	-------	-------	------

 (88)

Utilisation factor for gains for rest of dwelling, h2,m (see Table 9a)

(89)m=

0.99	0.98	0.93	0.78	0.57	0.38	0.26	0.3	0.52	0.85	0.98	0.99
------	------	------	------	------	------	------	-----	------	------	------	------

 (89)

Mean internal temperature in the rest of dwelling T2 (follow steps 3 to 7 in Table 9c)

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(90)m=	19.54	19.75	20.01	20.24	20.3	20.32	20.32	20.33	20.32	20.21	19.86	19.51	(90)
fLA = Living area ÷ (4) =												0.14	(91)

Mean internal temperature (for the whole dwelling) = fLA × T1 + (1 – fLA) × T2

(92)m=	19.67	19.86	20.12	20.34	20.4	20.42	20.42	20.42	20.41	20.31	19.97	19.64	(92)
--------	-------	-------	-------	-------	------	-------	-------	-------	-------	-------	-------	-------	------

Apply adjustment to the mean internal temperature from Table 4e, where appropriate

(93)m=	19.67	19.86	20.12	20.34	20.4	20.42	20.42	20.42	20.41	20.31	19.97	19.64	(93)
--------	-------	-------	-------	-------	------	-------	-------	-------	-------	-------	-------	-------	------

8. Space heating requirement

Set Ti to the mean internal temperature obtained at step 11 of Table 9b, so that Ti,m=(76)m and re-calculate the utilisation factor for gains using Table 9a

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

Utilisation factor for gains, hm:

(94)m=	0.99	0.97	0.92	0.78	0.58	0.39	0.27	0.3	0.53	0.85	0.97	0.99	(94)
--------	------	------	------	------	------	------	------	-----	------	------	------	------	------

Useful gains, hmGm , W = (94)m x (84)m

(95)m=	885.57	996.98	1064.39	1011.89	805.02	532.64	349.77	366.88	579.89	822.13	850.61	842.41	(95)
--------	--------	--------	---------	---------	--------	--------	--------	--------	--------	--------	--------	--------	------

Monthly average external temperature from Table 8

(96)m=	4.3	4.9	6.5	8.9	11.7	14.6	16.6	16.4	14.1	10.6	7.1	4.2	(96)
--------	-----	-----	-----	-----	------	------	------	------	------	------	-----	-----	------

Heat loss rate for mean internal temperature, Lm , W =[(39)m x [(93)m– (96)m]

(97)m=	1474.86	1431.19	1297.88	1070.93	811.68	532.92	349.78	366.92	582.39	905.89	1208.86	1460.73	(97)
--------	---------	---------	---------	---------	--------	--------	--------	--------	--------	--------	---------	---------	------

Space heating requirement for each month, kWh/month = 0.024 x [(97)m – (95)m] x (41)m

(98)m=	438.43	291.79	173.71	42.51	4.95	0	0	0	0	62.32	257.94	460.03	
Total per year (kWh/year) = Sum(98) _{1...5,9...12} =												1731.67	(98)

Space heating requirement in kWh/m²/year

13.61	(99)
-------	------

9a. Energy requirements – Individual heating systems including micro-CHP)

Space heating:

Fraction of space heat from secondary/supplementary system 0 (201)

Fraction of space heat from main system(s) (202) = 1 – (201) = 1 (202)

Fraction of total heating from main system 1 (204) = (202) × [1 – (203)] = 1 (204)

Efficiency of main space heating system 1 100 (206)

Efficiency of secondary/supplementary heating system, % 0 (208)

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	kWh/year
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	----------

Space heating requirement (calculated above)

438.43	291.79	173.71	42.51	4.95	0	0	0	0	62.32	257.94	460.03
--------	--------	--------	-------	------	---	---	---	---	-------	--------	--------

(211)m = {[(98)m x (204)] } x 100 ÷ (206) (211)

438.43	291.79	173.71	42.51	4.95	0	0	0	0	62.32	257.94	460.03
--------	--------	--------	-------	------	---	---	---	---	-------	--------	--------

Total (kWh/year) =Sum(211)_{1...5,10...12} = 1731.67 (211)

Space heating fuel (secondary), kWh/month

= {[(98)m x (201)] } x 100 ÷ (208)

(215)m=	0	0	0	0	0	0	0	0	0	0	0		
Total (kWh/year) =Sum(215) _{1...5,10...12} =												0	(215)

Water heating

Output from water heater (calculated above)

195.19	171.5	178.85	158.56	154.11	135.87	128.75	143.68	144.18	164.51	176.16	189.9
--------	-------	--------	--------	--------	--------	--------	--------	--------	--------	--------	-------

Efficiency of water heater 100 (216)

SAP WorkSheet: New dwelling design stage

(217)m=

100	100	100	100	100	100	100	100	100	100	100	100
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

 (217)

Fuel for water heating, kWh/month

(219)m = (64)m x 100 ÷ (217)m

(219)m=

195.19	171.5	178.85	158.56	154.11	135.87	128.75	143.68	144.18	164.51	176.16	189.9
--------	-------	--------	--------	--------	--------	--------	--------	--------	--------	--------	-------

Total = Sum(219a)_{1...12} =

1941.25

 (219)

Annual totals

Space heating fuel used, main system 1 kWh/year

1731.67

 (219)

Water heating fuel used

1941.25

 (219)

Electricity for pumps, fans and electric keep-hot

mechanical ventilation - balanced, extract or positive input from outside

428.02

 (230a)

Total electricity for the above, kWh/year sum of (230a)...(230g) =

428.02

 (231)

Electricity for lighting

490.13

 (232)

Total delivered energy for all uses (211)...(221) + (231) + (232)...(237b) =

4591.08

 (338)

10a. Fuel costs - individual heating systems:

	Fuel kWh/year		Fuel Price (Table 12)		Fuel Cost £/year		
Space heating - main system 1	(211) x		<table border="1"><tr><td>13.19</td></tr></table>	13.19	x 0.01 =	<table border="1"><tr><td>228.41</td></tr></table> (240)	228.41
13.19							
228.41							
Space heating - main system 2	(213) x		<table border="1"><tr><td>0</td></tr></table>	0	x 0.01 =	<table border="1"><tr><td>0</td></tr></table> (241)	0
0							
0							
Space heating - secondary	(215) x		<table border="1"><tr><td>13.19</td></tr></table>	13.19	x 0.01 =	<table border="1"><tr><td>0</td></tr></table> (242)	0
13.19							
0							
Water heating (electric off-peak tariff)							
High-rate fraction (Table 13, or Appendix F for electric CPSU)					<table border="1"><tr><td>1</td></tr></table> (243)	1	
1							
Low-rate fraction	1.0 – (243) =				<table border="1"><tr><td>0</td></tr></table> (244)	0	
0							
High-rate cost	(219) x (243) x		<table border="1"><tr><td>13.19</td></tr></table>	13.19	x 0.01 =	<table border="1"><tr><td>256.05</td></tr></table> (245)	256.05
13.19							
256.05							
Low-rate cost	(219) x (244) x		<table border="1"><tr><td>13.19</td></tr></table>	13.19	x 0.01 =	<table border="1"><tr><td>0</td></tr></table> (246)	0
13.19							
0							
Pumps, fans and electric keep-hot	(231)		<table border="1"><tr><td>13.19</td></tr></table>	13.19	x 0.01 =	<table border="1"><tr><td>56.46</td></tr></table> (249)	56.46
13.19							
56.46							
(if off-peak tariff, list each of (230a) to (230g) separately as applicable and apply fuel price according to Table 12a)							
Energy for lighting	(232)		<table border="1"><tr><td>13.19</td></tr></table>	13.19	x 0.01 =	<table border="1"><tr><td>64.65</td></tr></table> (250)	64.65
13.19							
64.65							
Additional standing charges (Table 12)					<table border="1"><tr><td>0</td></tr></table> (251)	0	
0							

Appendix Q items: repeat lines (253) and (254) as needed

Total energy cost (245)...(247) + (250)...(254) =

605.56

 (255)

11a. SAP rating - individual heating systems

Energy cost deflator (Table 12)

0.42

 (256)

Energy cost factor (ECF) [(255) x (256)] ÷ [(4) + 45.0] =

1.48

 (257)

SAP rating (Section 12)

79.41

 (258)

12a. CO2 emissions – Individual heating systems including micro-CHP

	Energy kWh/year		Emission factor kg CO2/kWh		Emissions kg CO2/year		
Space heating (main system 1)	(211) x		<table border="1"><tr><td>0.519</td></tr></table>	0.519	=	<table border="1"><tr><td>898.74</td></tr></table> (261)	898.74
0.519							
898.74							

SAP WorkSheet: New dwelling design stage

Space heating (secondary)	(215) x	0.519	=	0	(263)
Water heating	(219) x	0.519	=	1007.51	(264)
Space and water heating	(261) + (262) + (263) + (264) =			1906.25	(265)
Electricity for pumps, fans and electric keep-hot	(231) x	0.519	=	222.14	(267)
Electricity for lighting	(232) x	0.519	=	254.38	(268)
Total CO ₂ , kg/year	sum of (265)...(271) =			2382.77	(272)
CO₂ emissions per m²	(272) ÷ (4) =			18.72	(273)
El rating (section 14)				81	(274)

13a. Primary Energy

	Energy kWh/year	Primary factor		P. Energy kWh/year	
Space heating (main system 1)	(211) x	3.07	=	5316.24	(261)
Space heating (secondary)	(215) x	3.07	=	0	(263)
Energy for water heating	(219) x	3.07	=	5959.63	(264)
Space and water heating	(261) + (262) + (263) + (264) =			11275.87	(265)
Electricity for pumps, fans and electric keep-hot	(231) x	3.07	=	1314.03	(267)
Electricity for lighting	(232) x	0	=	1504.71	(268)
'Total Primary Energy	sum of (265)...(271) =			14094.62	(272)
Primary energy kWh/m²/year	(272) ÷ (4) =			110.74	(273)

DER WorkSheet: New dwelling design stage

User Details:

Assessor Name: Daniel Watt **Stroma Number:** STRO026464
Software Name: Stroma FSAP 2012 **Software Version:** Version: 1.0.5.51

Property Address: Plot 1 Type 3A End Tce

Address : VASA Club, 283 White Moss Rd, Manchester, M9 6NZ

1. Overall dwelling dimensions:

	Area(m ²)		Av. Height(m)		Volume(m ³)
Ground floor	43.42 (1a)	x	2.6 (2a)	=	112.89 (3a)
First floor	43.42 (1b)	x	2.8 (2b)	=	121.58 (3b)
Second floor	40.44 (1c)	x	2.93 (2c)	=	118.49 (3c)
Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n)	127.28 (4)				
Dwelling volume				(3a)+(3b)+(3c)+(3d)+(3e)+.....(3n) =	352.96 (5)

2. Ventilation rate:

	main heating	secondary heating	other	total	m ³ per hour
Number of chimneys	0	+	0	=	0 (6a)
Number of open flues	0	+	0	=	0 (6b)
Number of intermittent fans				0 x 10 =	0 (7a)
Number of passive vents				0 x 10 =	0 (7b)
Number of flueless gas fires				0 x 40 =	0 (7c)

Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) =	0	÷ (5) =	0 (8)
<i>If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)</i>			
Number of storeys in the dwelling (ns)			0 (9)
Additional infiltration		[(9)-1]x0.1 =	0 (10)
Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction <i>if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35</i>			0 (11)
If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0			0 (12)
If no draught lobby, enter 0.05, else enter 0			0 (13)
Percentage of windows and doors draught stripped			0 (14)
Window infiltration	0.25 - [0.2 x (14) ÷ 100] =		0 (15)
Infiltration rate	(8) + (10) + (11) + (12) + (13) + (15) =		0 (16)
Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area			3 (17)
If based on air permeability value, then (18) = [(17) ÷ 20] + (8), otherwise (18) = (16)			0.15 (18)
<i>Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used</i>			
Number of sides sheltered			3 (19)
Shelter factor	(20) = 1 - [0.075 x (19)] =		0.78 (20)
Infiltration rate incorporating shelter factor	(21) = (18) x (20) =		0.12 (21)

Infiltration rate modified for monthly wind speed

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

Monthly average wind speed from Table 7

(22)m=	5.1	5	4.9	4.4	4.3	3.8	3.8	3.7	4	4.3	4.5	4.7
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DER WorkSheet: New dwelling design stage

Wind Factor (22a)m = (22)m ÷ 4

(22a)m=	1.27	1.25	1.23	1.1	1.08	0.95	0.95	0.92	1	1.08	1.12	1.18
---------	------	------	------	-----	------	------	------	------	---	------	------	------

Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

	0.15	0.15	0.14	0.13	0.12	0.11	0.11	0.11	0.12	0.12	0.13	0.14
--	------	------	------	------	------	------	------	------	------	------	------	------

Calculate effective air change rate for the applicable case

If mechanical ventilation:

0.5 (23a)

If exhaust air heat pump using Appendix N, (23b) = (23a) × Fmv (equation (N5)) , otherwise (23b) = (23a)

0.5 (23b)

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

73.1 (23c)

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) × [1 – (23c) ÷ 100]

(24a)m= 0.28 0.28 0.28 0.26 0.26 0.24 0.24 0.24 0.25 0.26 0.27 0.27 (24a)

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

(24b)m= 0 0 0 0 0 0 0 0 0 0 0 0 (24b)

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 × (23b), then (24c) = (23b); otherwise (24c) = (22b) m + 0.5 × (23b)

(24c)m= 0 0 0 0 0 0 0 0 0 0 0 0 (24c)

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² x 0.5]

(24d)m= 0 0 0 0 0 0 0 0 0 0 0 0 (24d)

Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

(25)m= 0.28 0.28 0.28 0.26 0.26 0.24 0.24 0.24 0.25 0.26 0.27 0.27 (25)

3. Heat losses and heat loss parameter:

ELEMENT	Gross area (m²)	Openings m²	Net Area A ,m²	U-value W/m²K	A X U (W/K)	k-value kJ/m²·K	A X k kJ/K
Doors			1.73	x 1	= 1.73		(26)
Windows Type 1			12.41	x 1/[1/(0.8)+0.04]	= 9.62		(27)
Windows Type 2			9.38	x 1/[1/(0.8)+0.04]	= 7.27		(27)
Floor			43.42	x 0.1	= 4.342		(28)
Walls	150.82	23.52	127.3	x 0.15	= 19.1		(29)
Roof Type1	57.53	0	57.53	x 0.1	= 5.75		(30)
Roof Type2	2.88	0	2.88	x 0.13	= 0.37		(30)
Total area of elements, m²			254.65				(31)
Party wall			84	x 0	= 0		(32)

* for windows and roof windows, use effective window U-value calculated using formula 1/[(1/U-value)+0.04] as given in paragraph 3.2

** include the areas on both sides of internal walls and partitions

Fabric heat loss, W/K = S (A x U) (26)...(30) + (32) = 48.19 (33)

Heat capacity Cm = S(A x k) ((28)...(30) + (32) + (32a)...(32e) = 14637.89 (34)

Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m²K Indicative Value: Medium 250 (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f can be used instead of a detailed calculation.

Thermal bridges : S (L x Y) calculated using Appendix K 14.87 (36)

if details of thermal bridging are not known (36) = 0.05 x (31)

Total fabric heat loss (33) + (36) = 63.05 (37)

DER WorkSheet: New dwelling design stage

Ventilation heat loss calculated monthly

$$(38)m = 0.33 \times (25)m \times (5)$$

(38)m=

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
32.93	32.59	32.25	30.56	30.22	28.53	28.53	28.19	29.21	30.22	30.9	31.58

(38)

Heat transfer coefficient, W/K

$$(39)m = (37) + (38)m$$

(39)m=

95.98	95.65	95.31	93.62	93.28	91.58	91.58	91.25	92.26	93.28	93.95	94.63
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

$$\text{Average} = \text{Sum}(39)_{1...12} / 12 =$$

93.53

(39)

Heat loss parameter (HLP), W/m²K

$$(40)m = (39)m \div (4)$$

(40)m=

0.75	0.75	0.75	0.74	0.73	0.72	0.72	0.72	0.72	0.73	0.74	0.74
------	------	------	------	------	------	------	------	------	------	------	------

$$\text{Average} = \text{Sum}(40)_{1...12} / 12 =$$

0.73

(40)

Number of days in month (Table 1a)

(41)m=

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
31	28	31	30	31	30	31	31	30	31	30	31

(41)

4. Water heating energy requirement:

kWh/year:

Assumed occupancy, N

2.89

(42)

if TFA > 13.9, $N = 1 + 1.76 \times [1 - \exp(-0.000349 \times (TFA - 13.9)^2)] + 0.0013 \times (TFA - 13.9)$

if TFA ≤ 13.9, N = 1

Annual average hot water usage in litres per day $V_{d, \text{average}} = (25 \times N) + 36$

102.78

(43)

Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

Hot water usage in litres per day for each month $V_{d,m} = \text{factor from Table 1c} \times (43)$

(44)m=

113.06	108.95	104.84	100.72	96.61	92.5	92.5	96.61	100.72	104.84	108.95	113.06
--------	--------	--------	--------	-------	------	------	-------	--------	--------	--------	--------

$$\text{Total} = \text{Sum}(44)_{1...12} =$$

1233.36

(44)

Energy content of hot water used - calculated monthly = $4.190 \times V_{d,m} \times n_m \times DT_m / 3600$ kWh/month (see Tables 1b, 1c, 1d)

(45)m=

167.66	146.64	151.32	131.92	126.58	109.23	101.22	116.15	117.54	136.98	149.52	162.37
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

$$\text{Total} = \text{Sum}(45)_{1...12} =$$

1617.13

(45)

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

(46)m=

25.15	22	22.7	19.79	18.99	16.38	15.18	17.42	17.63	20.55	22.43	24.36
-------	----	------	-------	-------	-------	-------	-------	-------	-------	-------	-------

(46)

Water storage loss:

Storage volume (litres) including any solar or WWHRS storage within same vessel

250

(47)

If community heating and no tank in dwelling, enter 110 litres in (47)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in (47)

Water storage loss:

a) If manufacturer's declared loss factor is known (kWh/day):

1.48

(48)

Temperature factor from Table 2b

0.6

(49)

Energy lost from water storage, kWh/year

$$(48) \times (49) =$$

0.89

(50)

b) If manufacturer's declared cylinder loss factor is not known:

Hot water storage loss factor from Table 2 (kWh/litre/day)

0

(51)

If community heating see section 4.3

Volume factor from Table 2a

0

(52)

Temperature factor from Table 2b

0

(53)

Energy lost from water storage, kWh/year

$$(47) \times (51) \times (52) \times (53) =$$

0

(54)

Enter (50) or (54) in (55)

0.89

(55)

Water storage loss calculated for each month

$$((56)m = (55) \times (41)m$$

(56)m=

27.53	24.86	27.53	26.64	27.53	26.64	27.53	27.53	26.64	27.53	26.64	27.53
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

(56)

DER WorkSheet: New dwelling design stage

If cylinder contains dedicated solar storage, (57)m = (56)m × [(50) – (H11)] ÷ (50), else (57)m = (56)m where (H11) is from Appendix H

(57)m=	27.53	24.86	27.53	26.64	27.53	26.64	27.53	27.53	26.64	27.53	26.64	27.53	(57)
--------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	------

Primary circuit loss (annual) from Table 3	0	(58)
--	---	------

Primary circuit loss calculated for each month (59)m = (58) ÷ 365 × (41)m

(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat)

(59)m=	0	0	0	0	0	0	0	0	0	0	0	0	(59)
--------	---	---	---	---	---	---	---	---	---	---	---	---	------

Combi loss calculated for each month (61)m = (60) ÷ 365 × (41)m

(61)m=	0	0	0	0	0	0	0	0	0	0	0	0	(61)
--------	---	---	---	---	---	---	---	---	---	---	---	---	------

Total heat required for water heating calculated for each month (62)m = 0.85 × (45)m + (46)m + (57)m + (59)m + (61)m

(62)m=	195.19	171.5	178.85	158.56	154.11	135.87	128.75	143.68	144.18	164.51	176.16	189.9	(62)
--------	--------	-------	--------	--------	--------	--------	--------	--------	--------	--------	--------	-------	------

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)

(add additional lines if FGHRs and/or WWHRs applies, see Appendix G)

(63)m=	0	0	0	0	0	0	0	0	0	0	0	0	(63)
--------	---	---	---	---	---	---	---	---	---	---	---	---	------

Output from water heater

(64)m=	195.19	171.5	178.85	158.56	154.11	135.87	128.75	143.68	144.18	164.51	176.16	189.9	
Output from water heater (annual) ^{1...12}												1941.25	(64)

Heat gains from water heating, kWh/month 0.25 ´ [0.85 × (45)m + (61)m] + 0.8 × [(46)m + (57)m + (59)m]

(65)m=	77.77	68.65	72.34	65.18	64.11	57.63	55.68	60.64	60.39	67.57	71.03	76.01	(65)
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include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(66)m=	144.38	144.38	144.38	144.38	144.38	144.38	144.38	144.38	144.38	144.38	144.38	144.38	(66)

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5

(67)m=	27.75	24.65	20.05	15.18	11.34	9.58	10.35	13.45	18.06	22.93	26.76	28.52	(67)
--------	-------	-------	-------	-------	-------	------	-------	-------	-------	-------	-------	-------	------

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5

(68)m=	294.41	297.47	289.77	273.38	252.69	233.24	220.25	217.2	224.9	241.29	261.98	281.42	(68)
--------	--------	--------	--------	--------	--------	--------	--------	-------	-------	--------	--------	--------	------

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5

(69)m=	37.44	37.44	37.44	37.44	37.44	37.44	37.44	37.44	37.44	37.44	37.44	37.44	(69)
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Pumps and fans gains (Table 5a)

(70)m=	0	0	0	0	0	0	0	0	0	0	0	0	(70)
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Losses e.g. evaporation (negative values) (Table 5)

(71)m=	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	(71)
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	------

Water heating gains (Table 5)

(72)m=	104.53	102.16	97.22	90.52	86.17	80.04	74.84	81.51	83.88	90.82	98.65	102.17	(72)
--------	--------	--------	-------	-------	-------	-------	-------	-------	-------	-------	-------	--------	------

Total internal gains = (66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m

(73)m=	493.01	490.59	473.35	445.39	416.52	389.18	371.75	378.47	393.15	421.34	453.7	478.42	(73)
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	-------	--------	------

6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

Orientation:	Access Factor Table 6d	Area m ²	Flux Table 6a	g_ Table 6b	FF Table 6c	Gains (W)
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DER WorkSheet: New dwelling design stage

Southeast 0.9x	0.77	x	9.38	x	36.79	x	0.72	x	0.7	=	120.54	(77)
Southeast 0.9x	0.77	x	9.38	x	62.67	x	0.72	x	0.7	=	205.33	(77)
Southeast 0.9x	0.77	x	9.38	x	85.75	x	0.72	x	0.7	=	280.94	(77)
Southeast 0.9x	0.77	x	9.38	x	106.25	x	0.72	x	0.7	=	348.1	(77)
Southeast 0.9x	0.77	x	9.38	x	119.01	x	0.72	x	0.7	=	389.9	(77)
Southeast 0.9x	0.77	x	9.38	x	118.15	x	0.72	x	0.7	=	387.08	(77)
Southeast 0.9x	0.77	x	9.38	x	113.91	x	0.72	x	0.7	=	373.19	(77)
Southeast 0.9x	0.77	x	9.38	x	104.39	x	0.72	x	0.7	=	342	(77)
Southeast 0.9x	0.77	x	9.38	x	92.85	x	0.72	x	0.7	=	304.2	(77)
Southeast 0.9x	0.77	x	9.38	x	69.27	x	0.72	x	0.7	=	226.93	(77)
Southeast 0.9x	0.77	x	9.38	x	44.07	x	0.72	x	0.7	=	144.38	(77)
Southeast 0.9x	0.77	x	9.38	x	31.49	x	0.72	x	0.7	=	103.16	(77)
Northwest 0.9x	0.77	x	12.41	x	11.28	x	0.72	x	0.7	=	48.91	(81)
Northwest 0.9x	0.77	x	12.41	x	22.97	x	0.72	x	0.7	=	99.55	(81)
Northwest 0.9x	0.77	x	12.41	x	41.38	x	0.72	x	0.7	=	179.35	(81)
Northwest 0.9x	0.77	x	12.41	x	67.96	x	0.72	x	0.7	=	294.55	(81)
Northwest 0.9x	0.77	x	12.41	x	91.35	x	0.72	x	0.7	=	395.94	(81)
Northwest 0.9x	0.77	x	12.41	x	97.38	x	0.72	x	0.7	=	422.11	(81)
Northwest 0.9x	0.77	x	12.41	x	91.1	x	0.72	x	0.7	=	394.87	(81)
Northwest 0.9x	0.77	x	12.41	x	72.63	x	0.72	x	0.7	=	314.8	(81)
Northwest 0.9x	0.77	x	12.41	x	50.42	x	0.72	x	0.7	=	218.55	(81)
Northwest 0.9x	0.77	x	12.41	x	28.07	x	0.72	x	0.7	=	121.66	(81)
Northwest 0.9x	0.77	x	12.41	x	14.2	x	0.72	x	0.7	=	61.54	(81)
Northwest 0.9x	0.77	x	12.41	x	9.21	x	0.72	x	0.7	=	39.94	(81)

Solar gains in watts, calculated for each month

(83)m = Sum(74)m ... (82)m

(83)m=

169.45	304.88	460.3	642.65	785.84	809.19	768.06	656.8	522.75	348.59	205.92	143.1
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 (83)

Total gains – internal and solar (84)m = (73)m + (83)m , watts

(84)m=

662.46	795.46	933.65	1088.04	1202.35	1198.37	1139.81	1035.27	915.89	769.93	659.62	621.52
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 (84)

7. Mean internal temperature (heating season)

Temperature during heating periods in the living area from Table 9, Th1 (°C)

21

 (85)

Utilisation factor for gains for living area, h1,m (see Table 9a)

(86)m=

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	1	0.98	0.9	0.7	0.49	0.35	0.41	0.68	0.96	1	1

 (86)

Mean internal temperature in living area T1 (follow steps 3 to 7 in Table 9c)

(87)m=

20.25	20.4	20.63	20.87	20.98	21	21	21	20.99	20.81	20.48	20.23
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 (87)

Temperature during heating periods in rest of dwelling from Table 9, Th2 (°C)

(88)m=

20.29	20.3	20.3	20.31	20.31	20.32	20.32	20.33	20.32	20.31	20.31	20.3
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 (88)

Utilisation factor for gains for rest of dwelling, h2,m (see Table 9a)

(89)m=

1	0.99	0.97	0.87	0.66	0.44	0.3	0.35	0.62	0.94	1	1
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 (89)

Mean internal temperature in the rest of dwelling T2 (follow steps 3 to 7 in Table 9c)

DER WorkSheet: New dwelling design stage

(90)m=	19.28	19.5	19.82	20.17	20.3	20.32	20.32	20.33	20.31	20.1	19.62	19.25	(90)
fLA = Living area ÷ (4) =												0.14	(91)

Mean internal temperature (for the whole dwelling) = fLA × T1 + (1 – fLA) × T2

(92)m=	19.41	19.63	19.94	20.27	20.39	20.42	20.42	20.42	20.41	20.2	19.75	19.39	(92)
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Apply adjustment to the mean internal temperature from Table 4e, where appropriate

(93)m=	19.41	19.63	19.94	20.27	20.39	20.42	20.42	20.42	20.41	20.2	19.75	19.39	(93)
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8. Space heating requirement

Set Ti to the mean internal temperature obtained at step 11 of Table 9b, so that Ti,m=(76)m and re-calculate the utilisation factor for gains using Table 9a

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
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Utilisation factor for gains, hm:

(94)m=	1	0.99	0.97	0.87	0.66	0.44	0.31	0.35	0.63	0.94	0.99	1	(94)
--------	---	------	------	------	------	------	------	------	------	------	------	---	------

Useful gains, hmGm , W = (94)m x (84)m

(95)m=	661.12	789.63	905.39	946.06	795.41	532.16	349.74	366.81	574.26	719.93	655.52	620.7	(95)
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	-------	------

Monthly average external temperature from Table 8

(96)m=	4.3	4.9	6.5	8.9	11.7	14.6	16.6	16.4	14.1	10.6	7.1	4.2	(96)
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Heat loss rate for mean internal temperature, Lm , W =[(39)m x [(93)m– (96)m]

(97)m=	1450.69	1408.79	1280.76	1064.29	810.76	532.88	349.78	366.91	581.86	895.32	1188.12	1437.19	(97)
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Space heating requirement for each month, kWh/month = 0.024 x [(97)m – (95)m] x (41)m

(98)m=	587.44	416.08	279.27	85.12	11.42	0	0	0	0	130.49	383.47	607.47	
Total per year (kWh/year) = Sum(98) _{1...5,9...12} =												2500.77	(98)

Space heating requirement in kWh/m²/year

19.65	(99)
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9a. Energy requirements – Individual heating systems including micro-CHP)

Space heating:

Fraction of space heat from secondary/supplementary system 0 (201)

Fraction of space heat from main system(s) (202) = 1 – (201) = 1 (202)

Fraction of total heating from main system 1 (204) = (202) × [1 – (203)] = 1 (204)

Efficiency of main space heating system 1 100 (206)

Efficiency of secondary/supplementary heating system, % 0 (208)

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	kWh/year
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	----------

Space heating requirement (calculated above)

587.44	416.08	279.27	85.12	11.42	0	0	0	0	130.49	383.47	607.47
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(211)m = {[(98)m x (204)] } x 100 ÷ (206) (211)

587.44	416.08	279.27	85.12	11.42	0	0	0	0	130.49	383.47	607.47
--------	--------	--------	-------	-------	---	---	---	---	--------	--------	--------

Total (kWh/year) =Sum(211)_{1...5,10...12} =

2500.77	(211)
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Space heating fuel (secondary), kWh/month

= {[(98)m x (201)] } x 100 ÷ (208)

(215)m=	0	0	0	0	0	0	0	0	0	0	0		
Total (kWh/year) =Sum(215) _{1...5,10...12} =												0	(215)

Water heating

Output from water heater (calculated above)

195.19	171.5	178.85	158.56	154.11	135.87	128.75	143.68	144.18	164.51	176.16	189.9
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Efficiency of water heater 100 (216)

DER WorkSheet: New dwelling design stage

(217)m=	100	100	100	100	100	100	100	100	100	100	100	(217)
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Fuel for water heating, kWh/month

(219)m = (64)m x 100 ÷ (217)m

(219)m=	195.19	171.5	178.85	158.56	154.11	135.87	128.75	143.68	144.18	164.51	176.16	189.9	
Total = Sum(219a) _{1...12} =												1941.25	(219)

Annual totals

	kWh/year	kWh/year
Space heating fuel used, main system 1		2500.77
Water heating fuel used		1941.25
Electricity for pumps, fans and electric keep-hot		
mechanical ventilation - balanced, extract or positive input from outside	428.02	(230a)
Total electricity for the above, kWh/year	sum of (230a)...(230g) =	428.02 (231)
Electricity for lighting		490.13 (232)
Total delivered energy for all uses (211)...(221) + (231) + (232)...(237b) =		5360.17 (338)

12a. CO2 emissions – Individual heating systems including micro-CHP

	Energy kWh/year	Emission factor kg CO2/kWh	Emissions kg CO2/year
Space heating (main system 1)	(211) x	0.519	= 1297.9 (261)
Space heating (secondary)	(215) x	0.519	= 0 (263)
Water heating	(219) x	0.519	= 1007.51 (264)
Space and water heating	(261) + (262) + (263) + (264) =		2305.41 (265)
Electricity for pumps, fans and electric keep-hot	(231) x	0.519	= 222.14 (267)
Electricity for lighting	(232) x	0.519	= 254.38 (268)
Total CO2, kg/year		sum of (265)...(271) =	2781.93 (272)
Dwelling CO2 Emission Rate		(272) ÷ (4) =	21.86 (273)
El rating (section 14)			78 (274)

TER WorkSheet: New dwelling design stage

User Details:

Assessor Name: Daniel Watt **Stroma Number:** STRO026464
Software Name: Stroma FSAP 2012 **Software Version:** Version: 1.0.5.51

Property Address: Plot 1 Type 3A End Tce

Address : VASA Club, 283 White Moss Rd, Manchester, M9 6NZ

1. Overall dwelling dimensions:

	Area(m ²)		Av. Height(m)		Volume(m ³)
Ground floor	43.42 (1a)	x	2.6 (2a)	=	112.89 (3a)
First floor	43.42 (1b)	x	2.8 (2b)	=	121.58 (3b)
Second floor	40.44 (1c)	x	2.93 (2c)	=	118.49 (3c)
Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n)	127.28 (4)				
Dwelling volume				(3a)+(3b)+(3c)+(3d)+(3e)+.....(3n) =	352.96 (5)

2. Ventilation rate:

	main heating	secondary heating	other	total	m ³ per hour
Number of chimneys	0	+	0	=	0 (6a)
Number of open flues	0	+	0	=	0 (6b)
Number of intermittent fans				4 x 10 =	40 (7a)
Number of passive vents				0 x 10 =	0 (7b)
Number of flueless gas fires				0 x 40 =	0 (7c)

Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) =	40	÷ (5) =	0.11 (8)
<i>If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)</i>			
Number of storeys in the dwelling (ns)			0 (9)
Additional infiltration		[(9)-1]x0.1 =	0 (10)
Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction <i>if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35</i>			0 (11)
If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0			0 (12)
If no draught lobby, enter 0.05, else enter 0			0 (13)
Percentage of windows and doors draught stripped			0 (14)
Window infiltration	0.25 - [0.2 x (14) ÷ 100] =		0 (15)
Infiltration rate	(8) + (10) + (11) + (12) + (13) + (15) =		0 (16)
Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area			5 (17)
If based on air permeability value, then (18) = [(17) ÷ 20] + (8), otherwise (18) = (16)			0.36 (18)
<i>Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used</i>			
Number of sides sheltered			3 (19)
Shelter factor	(20) = 1 - [0.075 x (19)] =		0.78 (20)
Infiltration rate incorporating shelter factor	(21) = (18) x (20) =		0.28 (21)

Infiltration rate modified for monthly wind speed

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
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Monthly average wind speed from Table 7

(22)m=	5.1	5	4.9	4.4	4.3	3.8	3.8	3.7	4	4.3	4.5	4.7
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TER WorkSheet: New dwelling design stage

Wind Factor (22a)m = (22)m ÷ 4

(22a)m=	1.27	1.25	1.23	1.1	1.08	0.95	0.95	0.92	1	1.08	1.12	1.18
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Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

	0.36	0.35	0.34	0.31	0.3	0.27	0.27	0.26	0.28	0.3	0.32	0.33
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Calculate effective air change rate for the applicable case

If mechanical ventilation:

0 (23a)

If exhaust air heat pump using Appendix N, (23b) = (23a) × Fmv (equation (N5)) , otherwise (23b) = (23a)

0 (23b)

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

0 (23c)

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) × [1 – (23c) ÷ 100]

(24a)m=	0	0	0	0	0	0	0	0	0	0	0	0
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(24a)

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

(24b)m=	0	0	0	0	0	0	0	0	0	0	0	0
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(24b)

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 × (23b), then (24c) = (23b); otherwise (24c) = (22b) m + 0.5 × (23b)

(24c)m=	0	0	0	0	0	0	0	0	0	0	0	0
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(24c)

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² x 0.5]

(24d)m=	0.56	0.56	0.56	0.55	0.55	0.54	0.54	0.53	0.54	0.55	0.55	0.55
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(24d)

Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

(25)m=	0.56	0.56	0.56	0.55	0.55	0.54	0.54	0.53	0.54	0.55	0.55	0.55
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(25)

3. Heat losses and heat loss parameter:

ELEMENT	Gross area (m²)	Openings m²	Net Area A ,m²	U-value W/m²K	A X U (W/K)	k-value kJ/m²·K	A X k kJ/K
Doors			1.73	x 1	= 1.73		(26)
Windows Type 1			12.41	x 1/[1/(1.4)+0.04]	= 16.45		(27)
Windows Type 2			9.38	x 1/[1/(1.4)+0.04]	= 12.44		(27)
Floor			43.42	x 0.13	= 5.644599		(28)
Walls	150.82	23.52	127.3	x 0.18	= 22.91		(29)
Roof Type1	57.53	0	57.53	x 0.13	= 7.48		(30)
Roof Type2	2.88	0	2.88	x 0.13	= 0.37		(30)
Total area of elements, m²			254.65				(31)
Party wall			84	x 0	= 0		(32)

* for windows and roof windows, use effective window U-value calculated using formula 1/[(1/U-value)+0.04] as given in paragraph 3.2

** include the areas on both sides of internal walls and partitions

Fabric heat loss, W/K = S (A x U) (26)...(30) + (32) = 67.03 (33)

Heat capacity Cm = S(A x k) ((28)...(30) + (32) + (32a)...(32e) = 14637.89 (34)

Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m²K Indicative Value: Medium 250 (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f can be used instead of a detailed calculation.

Thermal bridges : S (L x Y) calculated using Appendix K 10.48 (36)

if details of thermal bridging are not known (36) = 0.05 x (31)

Total fabric heat loss (33) + (36) = 77.51 (37)

TER WorkSheet: New dwelling design stage

Ventilation heat loss calculated monthly

$$(38)m = 0.33 \times (25)m \times (5)$$

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(38)m=	65.74	65.45	65.17	63.83	63.57	62.41	62.41	62.19	62.86	63.57	64.08	64.61	(38)

Heat transfer coefficient, W/K

$$(39)m = (37) + (38)m$$

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(39)m=	143.26	142.97	142.68	141.34	141.09	139.92	139.92	139.7	140.37	141.09	141.59	142.13	
Average = Sum(39) _{1...12} /12=												141.34	(39)

Heat loss parameter (HLP), W/m²K

$$(40)m = (39)m \div (4)$$

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(40)m=	1.13	1.12	1.12	1.11	1.11	1.1	1.1	1.1	1.1	1.11	1.11	1.12	
Average = Sum(40) _{1...12} /12=												1.11	(40)

Number of days in month (Table 1a)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(41)m=	31	28	31	30	31	30	31	31	30	31	30	31	(41)

4. Water heating energy requirement:

kWh/year:

Assumed occupancy, N

$$\text{if TFA} > 13.9, N = 1 + 1.76 \times [1 - \exp(-0.000349 \times (TFA - 13.9)^2)] + 0.0013 \times (TFA - 13.9)$$

$$\text{if TFA} \leq 13.9, N = 1$$

2.89 (42)

Annual average hot water usage in litres per day $V_{d,average} = (25 \times N) + 36$

102.78 (43)

Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(44)m=	113.06	108.95	104.84	100.72	96.61	92.5	92.5	96.61	100.72	104.84	108.95	113.06	
Total = Sum(44) _{1...12} =												1233.36	(44)

Energy content of hot water used - calculated monthly = $4.190 \times V_{d,m} \times n_m \times DT_m / 3600$ kWh/month (see Tables 1b, 1c, 1d)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(45)m=	167.66	146.64	151.32	131.92	126.58	109.23	101.22	116.15	117.54	136.98	149.52	162.37	
Total = Sum(45) _{1...12} =												1617.13	(45)

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(46)m=	25.15	22	22.7	19.79	18.99	16.38	15.18	17.42	17.63	20.55	22.43	24.36	(46)

Water storage loss:

Storage volume (litres) including any solar or WWHRS storage within same vessel 150 (47)

If community heating and no tank in dwelling, enter 110 litres in (47)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in (47)

Water storage loss:

a) If manufacturer's declared loss factor is known (kWh/day): 1.89 (48)

Temperature factor from Table 2b 0.54 (49)

Energy lost from water storage, kWh/year (48) x (49) = 1.02 (50)

b) If manufacturer's declared cylinder loss factor is not known:

Hot water storage loss factor from Table 2 (kWh/litre/day) 0 (51)

If community heating see section 4.3

Volume factor from Table 2a 0 (52)

Temperature factor from Table 2b 0 (53)

Energy lost from water storage, kWh/year (47) x (51) x (52) x (53) = 0 (54)

Enter (50) or (54) in (55) 1.02 (55)

Water storage loss calculated for each month ((56)m = (55) x (41)m

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
(56)m=	31.64	28.58	31.64	30.62	31.64	30.62	31.64	31.64	30.62	31.64	30.62	31.64	(56)

TER WorkSheet: New dwelling design stage

If cylinder contains dedicated solar storage, (57)m = (56)m × [(50) – (H11)] ÷ (50), else (57)m = (56)m where (H11) is from Appendix H

(57)m=

31.64	28.58	31.64	30.62	31.64	30.62	31.64	31.64	30.62	31.64	30.62	31.64
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

 (57)

Primary circuit loss (annual) from Table 3

0

 (58)

Primary circuit loss calculated for each month (59)m = (58) ÷ 365 × (41)m

(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat)

(59)m=

23.26	21.01	23.26	22.51	23.26	22.51	23.26	23.26	22.51	23.26	22.51	23.26
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

 (59)

Combi loss calculated for each month (61)m = (60) ÷ 365 × (41)m

(61)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

 (61)

Total heat required for water heating calculated for each month (62)m = 0.85 × (45)m + (46)m + (57)m + (59)m + (61)m

(62)m=

222.57	196.23	206.22	185.06	181.49	162.37	156.13	171.06	170.67	191.88	202.66	217.28
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

 (62)

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)

(add additional lines if FGHRs and/or WWHRs applies, see Appendix G)

(63)m=

0	0	0	0	0	0	0	0	0	0	0	0
---	---	---	---	---	---	---	---	---	---	---	---

 (63)

Output from water heater

(64)m=

222.57	196.23	206.22	185.06	181.49	162.37	156.13	171.06	170.67	191.88	202.66	217.28
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

Output from water heater (annual) ^{1...12}	2263.61
---	---------

 (64)

Heat gains from water heating, kWh/month 0.25 ´ [0.85 × (45)m + (61)m] + 0.8 × [(46)m + (57)m + (59)m]

(65)m=

99.67	88.43	94.24	86.37	86.01	78.83	77.58	82.55	81.59	89.47	92.22	97.91
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

 (65)

include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts

(66)m=

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
144.38	144.38	144.38	144.38	144.38	144.38	144.38	144.38	144.38	144.38	144.38	144.38

 (66)

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5

(67)m=

27.04	24.01	19.53	14.78	11.05	9.33	10.08	13.1	17.59	22.33	26.07	27.79
-------	-------	-------	-------	-------	------	-------	------	-------	-------	-------	-------

 (67)

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5

(68)m=

294.41	297.47	289.77	273.38	252.69	233.24	220.25	217.2	224.9	241.29	261.98	281.42
--------	--------	--------	--------	--------	--------	--------	-------	-------	--------	--------	--------

 (68)

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5

(69)m=

37.44	37.44	37.44	37.44	37.44	37.44	37.44	37.44	37.44	37.44	37.44	37.44
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

 (69)

Pumps and fans gains (Table 5a)

(70)m=

3	3	3	3	3	3	3	3	3	3	3	3
---	---	---	---	---	---	---	---	---	---	---	---

 (70)

Losses e.g. evaporation (negative values) (Table 5)

(71)m=

-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5	-115.5
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

 (71)

Water heating gains (Table 5)

(72)m=

133.97	131.59	126.66	119.96	115.61	109.48	104.27	110.95	113.32	120.26	128.09	131.6
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	-------

 (72)

Total internal gains = (66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m

(73)m=

524.73	522.39	505.27	477.44	448.66	421.37	403.92	410.57	425.12	453.19	485.45	510.13
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

 (73)

6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

Orientation:	Access Factor Table 6d	Area m²	Flux Table 6a	g_ Table 6b	FF Table 6c	Gains (W)
--------------	---------------------------	------------	------------------	----------------	----------------	--------------

TER WorkSheet: New dwelling design stage

Southeast 0.9x	0.77	x	9.38	x	36.79	x	0.63	x	0.7	=	105.48	(77)
Southeast 0.9x	0.77	x	9.38	x	62.67	x	0.63	x	0.7	=	179.66	(77)
Southeast 0.9x	0.77	x	9.38	x	85.75	x	0.63	x	0.7	=	245.82	(77)
Southeast 0.9x	0.77	x	9.38	x	106.25	x	0.63	x	0.7	=	304.59	(77)
Southeast 0.9x	0.77	x	9.38	x	119.01	x	0.63	x	0.7	=	341.16	(77)
Southeast 0.9x	0.77	x	9.38	x	118.15	x	0.63	x	0.7	=	338.69	(77)
Southeast 0.9x	0.77	x	9.38	x	113.91	x	0.63	x	0.7	=	326.54	(77)
Southeast 0.9x	0.77	x	9.38	x	104.39	x	0.63	x	0.7	=	299.25	(77)
Southeast 0.9x	0.77	x	9.38	x	92.85	x	0.63	x	0.7	=	266.17	(77)
Southeast 0.9x	0.77	x	9.38	x	69.27	x	0.63	x	0.7	=	198.57	(77)
Southeast 0.9x	0.77	x	9.38	x	44.07	x	0.63	x	0.7	=	126.33	(77)
Southeast 0.9x	0.77	x	9.38	x	31.49	x	0.63	x	0.7	=	90.26	(77)
Northwest 0.9x	0.77	x	12.41	x	11.28	x	0.63	x	0.7	=	42.79	(81)
Northwest 0.9x	0.77	x	12.41	x	22.97	x	0.63	x	0.7	=	87.1	(81)
Northwest 0.9x	0.77	x	12.41	x	41.38	x	0.63	x	0.7	=	156.94	(81)
Northwest 0.9x	0.77	x	12.41	x	67.96	x	0.63	x	0.7	=	257.73	(81)
Northwest 0.9x	0.77	x	12.41	x	91.35	x	0.63	x	0.7	=	346.44	(81)
Northwest 0.9x	0.77	x	12.41	x	97.38	x	0.63	x	0.7	=	369.35	(81)
Northwest 0.9x	0.77	x	12.41	x	91.1	x	0.63	x	0.7	=	345.52	(81)
Northwest 0.9x	0.77	x	12.41	x	72.63	x	0.63	x	0.7	=	275.45	(81)
Northwest 0.9x	0.77	x	12.41	x	50.42	x	0.63	x	0.7	=	191.23	(81)
Northwest 0.9x	0.77	x	12.41	x	28.07	x	0.63	x	0.7	=	106.45	(81)
Northwest 0.9x	0.77	x	12.41	x	14.2	x	0.63	x	0.7	=	53.84	(81)
Northwest 0.9x	0.77	x	12.41	x	9.21	x	0.63	x	0.7	=	34.95	(81)

Solar gains in watts, calculated for each month

(83)m = Sum(74)m ... (82)m

(83)m=

148.27	266.77	402.76	562.32	687.61	708.04	672.05	574.7	457.4	305.02	180.18	125.21
--------	--------	--------	--------	--------	--------	--------	-------	-------	--------	--------	--------

 (83)

Total gains – internal and solar (84)m = (73)m + (83)m , watts

(84)m=

673	789.16	908.03	1039.76	1136.27	1129.41	1075.98	985.27	882.52	758.21	665.62	635.34
-----	--------	--------	---------	---------	---------	---------	--------	--------	--------	--------	--------

 (84)

7. Mean internal temperature (heating season)

Temperature during heating periods in the living area from Table 9, Th1 (°C)

21

 (85)

Utilisation factor for gains for living area, h1,m (see Table 9a)

(86)m=

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	1	0.99	0.97	0.89	0.73	0.56	0.63	0.87	0.98	1	1

 (86)

Mean internal temperature in living area T1 (follow steps 3 to 7 in Table 9c)

(87)m=

19.73	19.88	20.13	20.48	20.78	20.95	20.99	20.98	20.85	20.46	20.03	19.7
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	------

 (87)

Temperature during heating periods in rest of dwelling from Table 9, Th2 (°C)

(88)m=

19.98	19.98	19.98	19.99	19.99	20	20	20	20	19.99	19.99	19.99
-------	-------	-------	-------	-------	----	----	----	----	-------	-------	-------

 (88)

Utilisation factor for gains for rest of dwelling, h2,m (see Table 9a)

(89)m=

1	1	0.99	0.96	0.85	0.64	0.44	0.5	0.81	0.98	1	1
---	---	------	------	------	------	------	-----	------	------	---	---

 (89)

Mean internal temperature in the rest of dwelling T2 (follow steps 3 to 7 in Table 9c)

TER WorkSheet: New dwelling design stage

(90)m=	18.27	18.49	18.87	19.37	19.77	19.96	20	19.99	19.88	19.36	18.73	18.24	(90)
fLA = Living area ÷ (4) =												0.14	(91)

Mean internal temperature (for the whole dwelling) = fLA × T1 + (1 – fLA) × T2

(92)m=	18.48	18.69	19.05	19.52	19.91	20.1	20.14	20.13	20.01	19.51	18.91	18.44	(92)
--------	-------	-------	-------	-------	-------	------	-------	-------	-------	-------	-------	-------	------

Apply adjustment to the mean internal temperature from Table 4e, where appropriate

(93)m=	18.48	18.69	19.05	19.52	19.91	20.1	20.14	20.13	20.01	19.51	18.91	18.44	(93)
--------	-------	-------	-------	-------	-------	------	-------	-------	-------	-------	-------	-------	------

8. Space heating requirement

Set Ti to the mean internal temperature obtained at step 11 of Table 9b, so that Ti,m=(76)m and re-calculate the utilisation factor for gains using Table 9a

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

Utilisation factor for gains, hm:

(94)m=	1	0.99	0.98	0.95	0.85	0.65	0.46	0.52	0.81	0.97	0.99	1	(94)
--------	---	------	------	------	------	------	------	------	------	------	------	---	------

Useful gains, hmGm , W = (94)m x (84)m

(95)m=	671.41	784.79	894.06	986.41	961.56	733.35	490.25	512.59	716.57	735.25	662.16	634.22	(95)
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	------

Monthly average external temperature from Table 8

(96)m=	4.3	4.9	6.5	8.9	11.7	14.6	16.6	16.4	14.1	10.6	7.1	4.2	(96)
--------	-----	-----	-----	-----	------	------	------	------	------	------	-----	-----	------

Heat loss rate for mean internal temperature, Lm , W =[(39)m x [(93)m– (96)m]

(97)m=	2030.91	1971.45	1790.31	1501.7	1158.88	770.05	494.96	521.65	830.17	1257.46	1672.35	2024.47	(97)
--------	---------	---------	---------	--------	---------	--------	--------	--------	--------	---------	---------	---------	------

Space heating requirement for each month, kWh/month = 0.024 x [(97)m – (95)m] x (41)m

(98)m=	1011.47	797.43	666.8	371.01	146.81	0	0	0	0	388.52	727.33	1034.35	
Total per year (kWh/year) = Sum(98) _{1...5,9...12} =												5143.73	(98)

Space heating requirement in kWh/m²/year

40.41	(99)
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9a. Energy requirements – Individual heating systems including micro-CHP)

Space heating:

Fraction of space heat from secondary/supplementary system 0 (201)

Fraction of space heat from main system(s) (202) = 1 – (201) = 1 (202)

Fraction of total heating from main system 1 (204) = (202) × [1 – (203)] = 1 (204)

Efficiency of main space heating system 1 93.5 (206)

Efficiency of secondary/supplementary heating system, % 0 (208)

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	kWh/year
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	----------

Space heating requirement (calculated above)

1011.47	797.43	666.8	371.01	146.81	0	0	0	0	388.52	727.33	1034.35
---------	--------	-------	--------	--------	---	---	---	---	--------	--------	---------

(211)m = {[(98)m x (204)] } x 100 ÷ (206) (211)

1081.79	852.87	713.16	396.8	157.01	0	0	0	0	415.53	777.9	1106.26
---------	--------	--------	-------	--------	---	---	---	---	--------	-------	---------

Total (kWh/year) =Sum(211)_{1...5,10...12} = 5501.32 (211)

Space heating fuel (secondary), kWh/month

= {[(98)m x (201)] } x 100 ÷ (208)

(215)m=	0	0	0	0	0	0	0	0	0	0	0		
Total (kWh/year) =Sum(215) _{1...5,10...12} =												0	(215)

Water heating

Output from water heater (calculated above)

222.57	196.23	206.22	185.06	181.49	162.37	156.13	171.06	170.67	191.88	202.66	217.28
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

Efficiency of water heater 79.8 (216)

TER WorkSheet: New dwelling design stage

(217)m=

88.36	88.17	87.72	86.63	84.25	79.8	79.8	79.8	79.8	86.66	87.93	88.44
-------	-------	-------	-------	-------	------	------	------	------	-------	-------	-------

 (217)

Fuel for water heating, kWh/month

(219)m = (64)m x 100 ÷ (217)m

(219)m=

251.88	222.57	235.09	213.61	215.41	203.47	195.65	214.36	213.88	221.43	230.47	245.67
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

Total = Sum(219a)_{1...12} =

2663.47

 (219)

Annual totals

Space heating fuel used, main system 1

kWh/year

kWh/year

Water heating fuel used

Electricity for pumps, fans and electric keep-hot

central heating pump:

30

(230c)

boiler with a fan-assisted flue

45

(230e)

Total electricity for the above, kWh/year

sum of (230a)...(230g) =

75

(231)

Electricity for lighting

477.47

(232)

Total delivered energy for all uses (211)...(221) + (231) + (232)...(237b) =

8717.26

(238)

12a. CO2 emissions – Individual heating systems including micro-CHP

	Energy kWh/year	Emission factor kg CO2/kWh		Emissions kg CO2/year
Space heating (main system 1)	(211) x	0.216	=	1188.28 (261)
Space heating (secondary)	(215) x	0.519	=	0 (263)
Water heating	(219) x	0.216	=	575.31 (264)
Space and water heating	(261) + (262) + (263) + (264) =			1763.6 (265)
Electricity for pumps, fans and electric keep-hot	(231) x	0.519	=	38.93 (267)
Electricity for lighting	(232) x	0.519	=	247.81 (268)
Total CO2, kg/year	sum of (265)...(271) =			2050.33 (272)

TER =

23.73 (273)