

Solar Photovoltaic Glint and Glare Study

Praxis Real Estate Management Ltd

Dakota House

March 2023

PLANNING SOLUTIONS FOR:

- Solar
- Telecoms
- Railways
- Defence
- Buildings
- Wind
- Airports
- Radar
- Mitigation

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ADMINISTRATION PAGE

Job Reference:	12163A
Date:	March 2023
Author:	James Plumb
Telephone:	01787 319001
Email:	james@pagerpower.com

Reviewed By:	Hannah McNaul; Danny Scrivener; Abdul Wadud
Email:	hannahm@pagerpower.com; danny@pagerpower.com; abdul@pagerpower.com

Issue	Date	Detail of Changes
1	March 2023	Initial issue

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Stour Valley Business Centre, Brundon Lane, Sudbury, CO10 7GB

T: +44 (0)1787 319001 E: info@pagerpower.com W: www.pagerpower.com

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EXECUTIVE SUMMARY

Report Purpose

Pager Power has been retained to assess the possible effects of glint and glare from a rooftop solar photovoltaic development, located in Wythenshawe, Manchester, UK. This assessment pertains to the potential impact upon aviation activity associated with Manchester Airport.

Overall Conclusions

No significant impacts are predicted upon aviation activity at Manchester Airport and no mitigation is required. It is recommended that these results are shared with Manchester Airport to understand their position towards the proposed development.

Guidance and Studies

Guidelines exist in the UK (produced by the Civil Aviation Authority) and in the USA (produced by the Federal Aviation Administration) with respect to solar developments and aviation activity. The UK CAA guidance is relatively high-level and does not prescribe a formal methodology. A specific national guidance policy for determining the impact of glint and glare on road safety, railway safety, and residential amenity has also not been produced to date. Therefore, in the absence of this, Pager Power reviewed more general existing planning guidelines and the available studies (discussed below) in the process of defining its own glint and glare assessment guidance and methodology¹. This methodology defines the process for determining the impact upon aviation activity.

Pager Power's approach is to undertake geometric reflection calculations and, where a solar reflection is predicted, consider the screening (existing and/or proposed) between the receptor and the reflecting solar panels. Where appropriate, solar intensity calculations are undertaken in line with the Sandia National Laboratories' FAA methodology². The scenario in which a solar reflection can occur for all receptors is then identified and discussed, and a comparison is made against the available solar panel reflection studies to determine the overall impact.

The available studies have measured the intensity of reflections from solar panels with respect to other naturally occurring and manmade surfaces. The results show that the reflections produced are of intensity similar to or less than those produced from still water and significantly less than reflections from glass and steel³.

¹ Pager Power Glint and Glare Guidance, Fourth Edition, September 2022.

² Formerly mandatory for on-airfield solar developments in the USA under the FAA's interim policy, superseded in 2021 with a policy that effectively requires individual airports to sign off on their on-airfield development as they see fit.

³ SunPower, 2009, SunPower Solar Module Glare and Reflectance (appendix to Solargen Energy, 2010).

Assessment Conclusions – Manchester Airport

Dakota House

Solar reflections are not geometrically possible towards the ATC Tower at Manchester Airport. No impact is predicted, and no mitigation is required.

The analysis has shown that solar reflections are predicted towards sections of the 10NM approach and departure paths for runways 23L and 23R. It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards these runway approaches, which is acceptable in accordance with the associated guidance (appendix D) and industry best practice pertaining to 2-mile approach paths, which state that this level of glare intensity is acceptable. A low impact is predicted for these approaches, and no mitigation is required.

Glare intensities of 'low potential for temporary after-image' are predicted upon sections of the Civil Aviation (CA) and General Aviation (GA) left-hand circuits for runways 05L and 05R, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

Glare intensities of 'low potential for temporary after-image' are predicted upon sections of the 5km x 5km overhead area centred upon the proposed development, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

Rowan Court

Solar reflections are not geometrically possible towards the ATC Tower at Manchester Airport. No impact is predicted, and no mitigation is required.

The analysis has shown that solar reflections are predicted towards sections of the 10NM approach and departure paths for runways 23L and 23R. It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards these runway approaches, which is acceptable in accordance with the associated guidance and industry best practice pertaining to 2-mile approach paths, which state that this level of glare intensity is acceptable. A low impact is predicted for these approaches, and no mitigation is required.

Glare intensities of 'low potential for temporary after-image' are predicted upon sections of the CA and GA left-hand circuits for runways 05L and 05R, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

Glare intensities of 'low potential for temporary after-image' are predicted upon sections of the 5km x 5km overhead area centred upon the proposed development, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

Coffee Shop

Solar reflections are not geometrically possible towards the ATC Tower at Manchester Airport. No impact is predicted, and no mitigation is required.

The analysis has shown that solar reflections are predicted towards sections of the 10NM approach and departure paths for runways 23L and 23R. It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards these runway approaches, which is acceptable in accordance with the associated guidance and industry best practice pertaining to 2-mile approach paths, which state that this level of glare intensity is acceptable. A low impact is predicted for these approaches, and no mitigation is required.

Glare intensities of 'low potential for temporary after-image' are predicted upon sections of the CA and GA left-hand circuits for runways 05L and 05R, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

Glare intensities of 'low potential for temporary after-image' are predicted upon sections of the 5km x 5km overhead area centred upon the proposed development, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

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ABOUT PAGER POWER

Pager Power is a dedicated consultancy company based in Suffolk, UK. The company has undertaken projects in 56 countries within Europe, Africa, America, Asia and Australasia.

The company comprises a team of experts to provide technical expertise and guidance on a range of planning issues for large and small developments.

Pager Power was established in 1997. Initially the company focus was on modelling the impact of wind turbines on radar systems. Over the years, the company has expanded into numerous fields including:

- Renewable energy projects;
- Building developments;
- Aviation and telecommunication systems.

Pager Power prides itself on providing comprehensive, understandable and accurate assessments of complex issues in line with national and international standards. This is underpinned by its custom software, longstanding relationships with stakeholders and active role in conferences and research efforts around the world.

Pager Power's assessments withstand legal scrutiny and the company can provide support for a project at any stage.

1 INTRODUCTION

1.1 Overview

Pager Power has been retained to assess the possible effects of glint and glare from a rooftop solar photovoltaic development, located in Wythenshawe, Manchester, UK. This assessment pertains to the potential impact upon aviation activity associated with Manchester Airport.

This report contains the following:

- Solar development details;
- Explanation of glint and glare;
- Overview of relevant guidance and relevant studies;
- Overview of Sun movement;
- Assessment methodology;
- Identification of receptors;
- Glint and glare assessment for identified receptors;
- Results discussion.

The relevant technical analysis is presented in each section. Following the assessment, conclusions and recommendations are made.

1.2 Pager Power's Experience

Pager Power has undertaken over 1,000 Glint and Glare assessments in the UK and internationally. The studies have included assessment of civil and military aerodromes, railway infrastructure and other ground-based receptors including roads and dwellings.

1.3 Glint and Glare Definition

The definition of glint and glare is as follows⁴:

- Glint – a momentary flash of bright light typically received by moving receptors or from moving reflectors;
- Glare – a continuous source of bright light typically received by static receptors or from large reflective surfaces.

The term 'solar reflection' is used in this report to refer to both reflection types i.e. glint and glare.

⁴ These definitions are aligned with those of the Draft National Policy Statement for Renewable Energy Infrastructure and the Federal Aviation Administration (FAA) in the United States of America.

2 SOLAR DEVELOPMENT LOCATION AND DETAILS

2.1 Proposed Development Site Layout

Figures 1 to 3 below and on the following pages show the roof layouts⁵ for the proposed development.

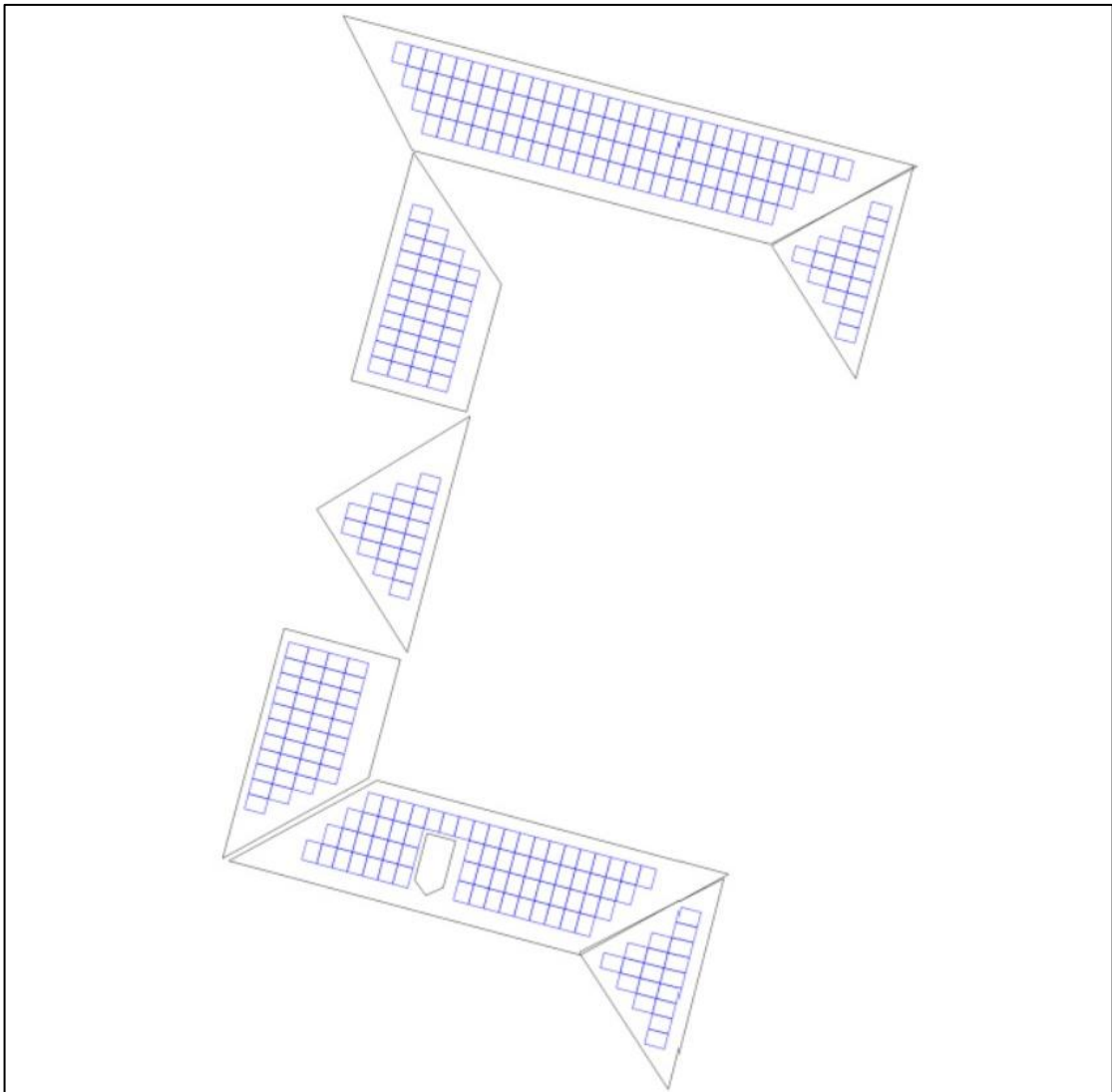


Figure 1 Proposed roof layout – Dakota House

⁵ Source: 84398439-BOW-A0-00DR-A-0023_P3_Proposed Site Layout PDF (cropped)

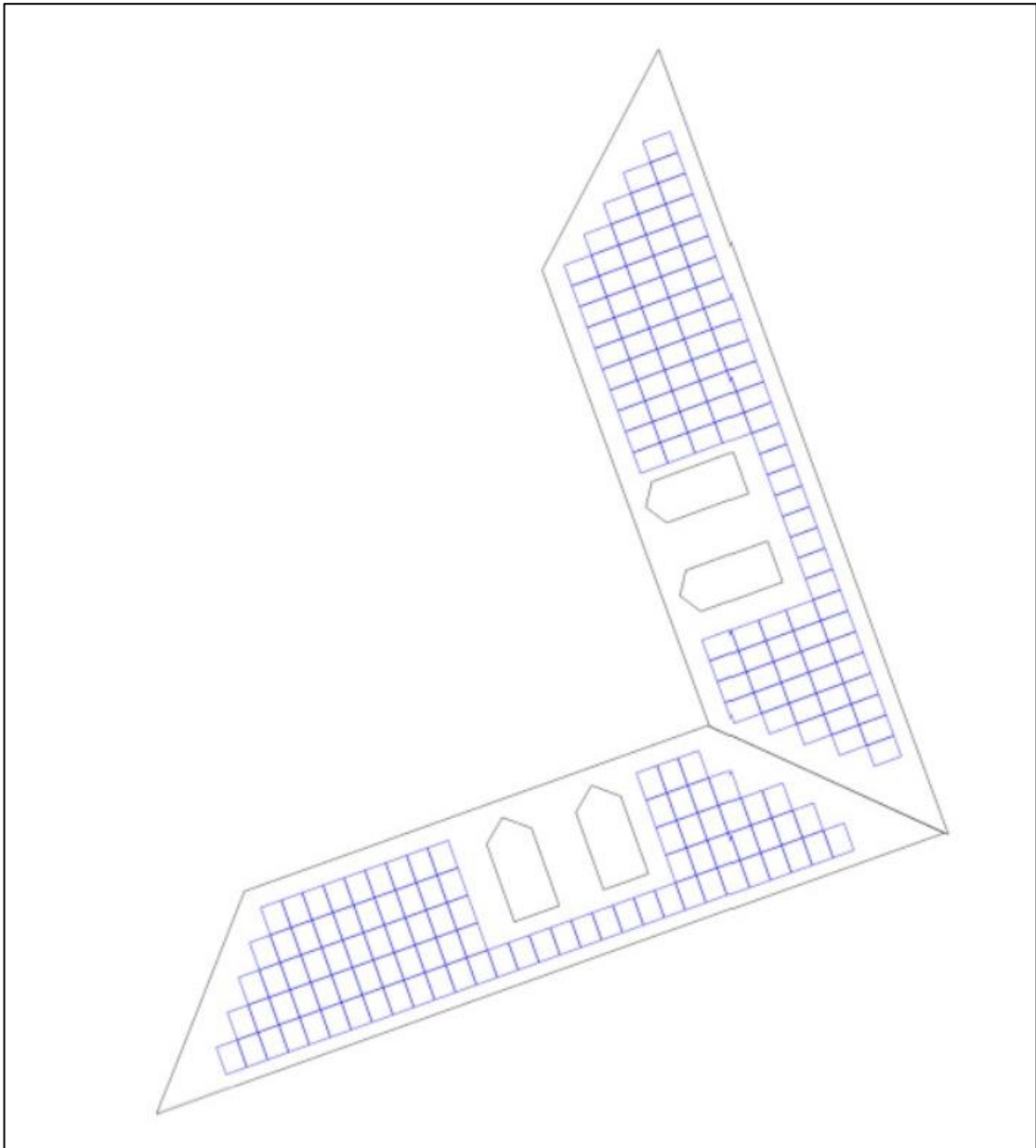


Figure 2 Proposed roof layout – Rowan Court

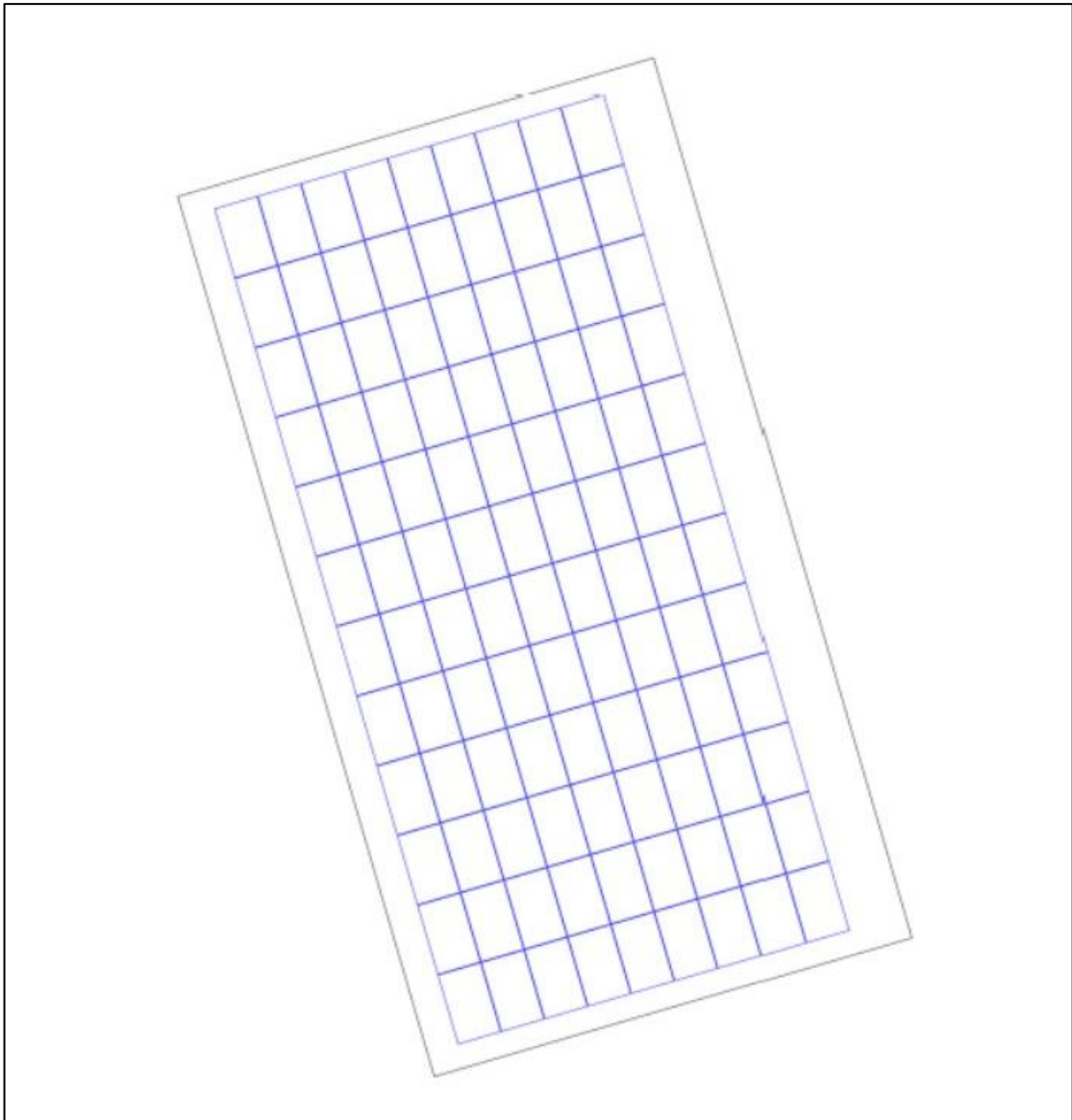


Figure 3 *Proposed roof layout – Coffee Shop*

Figure 4 below shows the proposed development panel areas overlayed on to aerial imagery.



Figure 4 Solar panel areas for the proposed development

2.2 Solar Panel Technical Information

Table 1 below summarises the technical information of the modelled solar panels used in the assessment.

Panel Information										
Panel area	1.1	1.2	1.3	1.4	1.5	1.6	1.7	2.1	2.2	3.1
Azimuth angle	194°	195°	105°	195°			105°	250°	160°	164°
Elevation angle	35°									3°
Assessed centre height (agl ⁶)	11m				13m	11m		8m		4.5m

Table 1 Solar panel technical information

⁶ Above ground level

3 GLINT AND GLARE ASSESSMENT METHODOLOGY

3.1 Guidance and Studies

Appendices A and B present a review of relevant guidance and independent studies with regard to glint and glare issues from solar panels. The overall conclusions from the available studies are as follows:

- Specular reflections of the Sun from solar panels are possible;
- The measured intensity of a reflection from solar panels can vary from 2% to 30% depending on the angle of incidence;
- Published guidance shows that the intensity of solar reflections from solar panels are equal to or less than those from water. It also shows that reflections from solar panels are significantly less intense than many other reflective surfaces, which are common in an outdoor environment.

3.2 Background

Details of the Sun's movements and solar reflections are presented in Appendix C.

3.3 Methodology

3.3.1 Pager Power's Methodology

The glint and glare assessment methodology has been derived from the information provided to Pager Power through consultation with stakeholders and by reviewing the available guidance and studies. The methodology for this glint and glare assessment is as follows:

- Identify receptors in the area surrounding the solar development;
- Consider direct solar reflections from the solar development towards the identified receptors by undertaking geometric calculations;
- Consider the visibility of the panels from the receptor's location. If the panels are not visible from the receptor then no reflection can occur;
- Based on the results of the geometric calculations, determine whether a reflection can occur, and if so, at what time it will occur;
- Consider both the solar reflection from the solar development and the location of the direct sunlight with respect to the receptor's position;
- Consider the solar reflection with respect to the published studies and guidance - including intensity calculations where appropriate;
- Determine whether a significant detrimental impact is expected in line with the process presented in Appendix D.

3.3.2 Sandia National Laboratories' Methodology

Sandia National Laboratories developed the Solar Glare Hazard Analysis Tool (SGHAT) which is no longer freely available however it is now developed by Forge Solar. Pager Power uses this model where required for aviation receptors. Whilst strictly applicable in the USA and to solar photovoltaic developments only, the methodology is widely used by aviation stakeholders internationally.

3.4 Assessment Methodology and Limitations

Further technical details regarding the methodology of the geometric calculations and limitations are presented in Appendix E and F.

4 IDENTIFICATION OF RECEPTORS

4.1 Aviation Receptors

Manchester Airport is a Civil Aviation Authority (CAA) licenced airport, situated approximately 1.2km south-west of the proposed solar development. It has one ATC Tower and two runways, the details of which are presented below:

- 05L/23R measuring 3,048m by 45m (concrete and asphalt);
- 05R/23L measuring 3,050m by 45m (concrete and asphalt).

The aerodrome chart for Manchester Airport⁷ is shown in Figure 9, on page 23.

These runways each have two associated approach paths, one for each bearing. It is Pager Power's methodology to assess whether a solar reflection can be experienced on the approach paths for the associated runways. This is considered to be the most critical stage of the flight.

A geometric glint and glare assessment has been undertaken for the approach and departure paths for runways 05L/23R and 05R/23L. Locations have been selected along the extended runway centre line from 50ft above the runway threshold out to a distance of ten nautical miles. The height of the aircraft is determined by using a 3-degree descent path. The receptor details for each runway approach are presented in Appendix G.

In addition to the approach and departure paths, receptors have been identified along the Civil Aviation (CA) and General Aviation (GA) circuits at Manchester Airport, and in a 5km x 5km lattice centred above the proposed development.

Figures 5 to 8, on the following pages, show the assessed aircraft approach paths, circuits, and 5km x 5km lattice relative to the proposed solar development.

⁷ <https://www.aurora.nats.co.uk/htmlAIP/Publications/2023-02-23-AIRAC/graphics/321208.pdf>

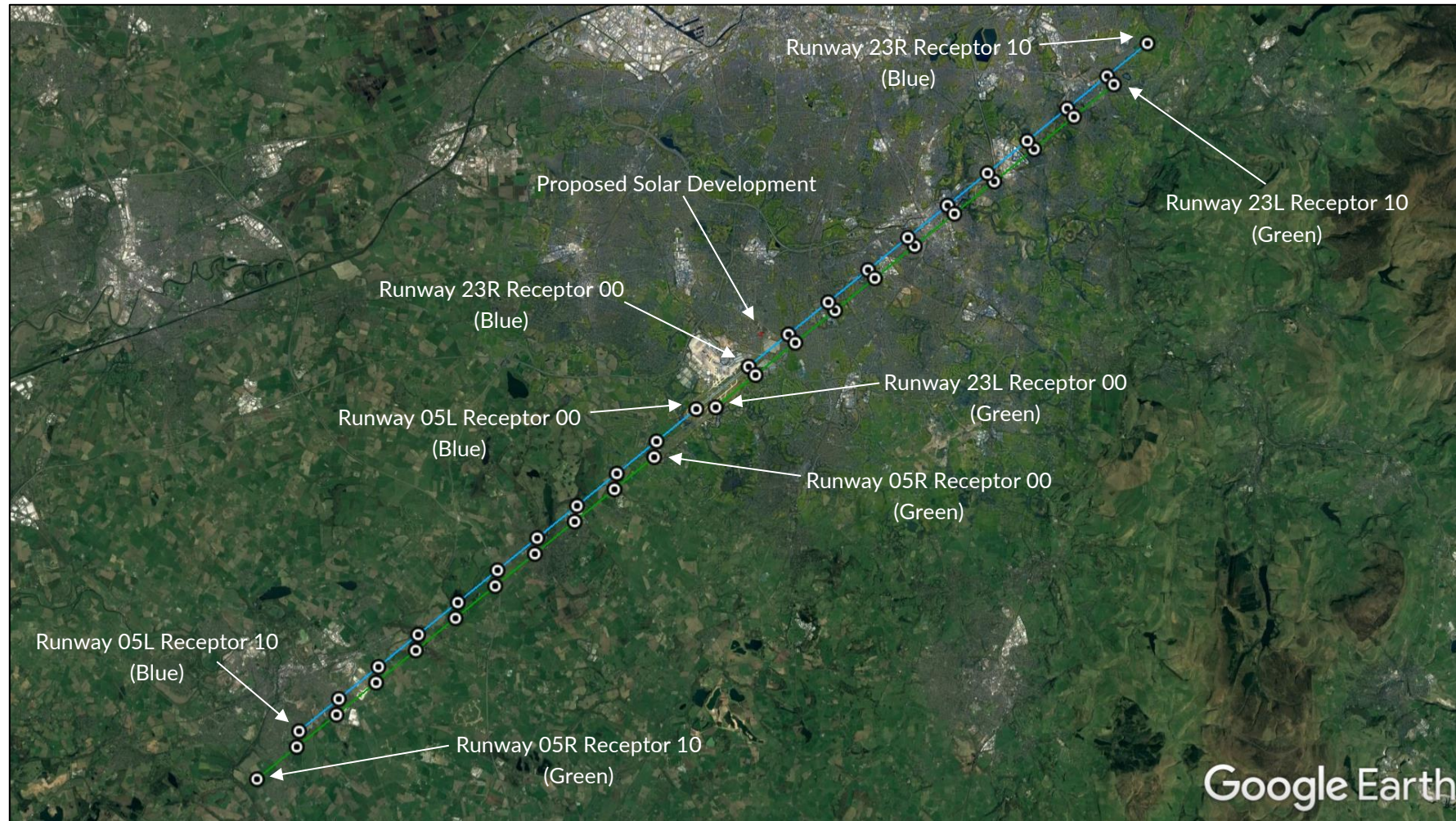


Figure 5 Manchester Airport approach path receptors

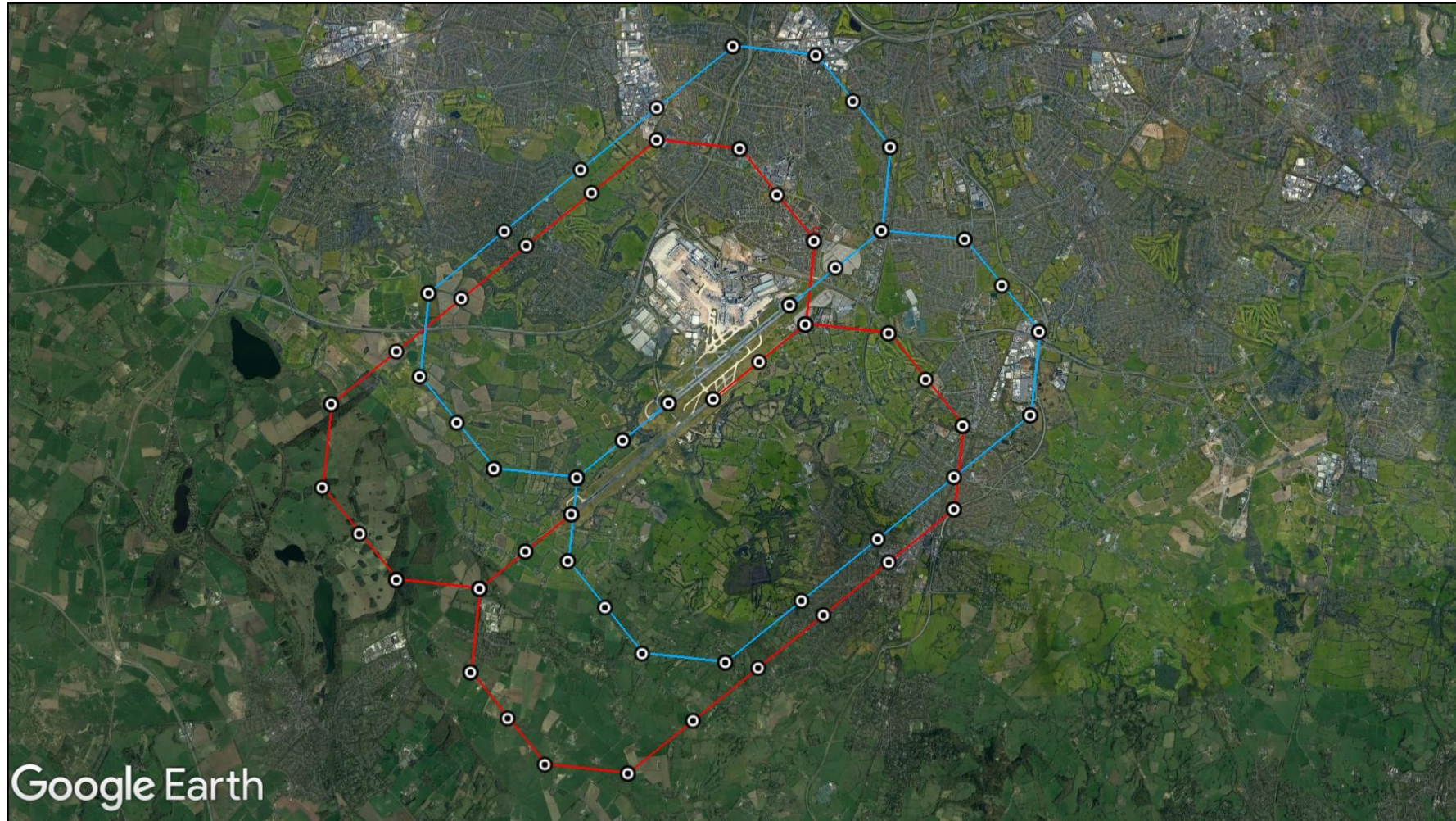


Figure 6 Manchester Airport CA circuit receptors



Figure 7 Manchester Airport GA circuit receptors

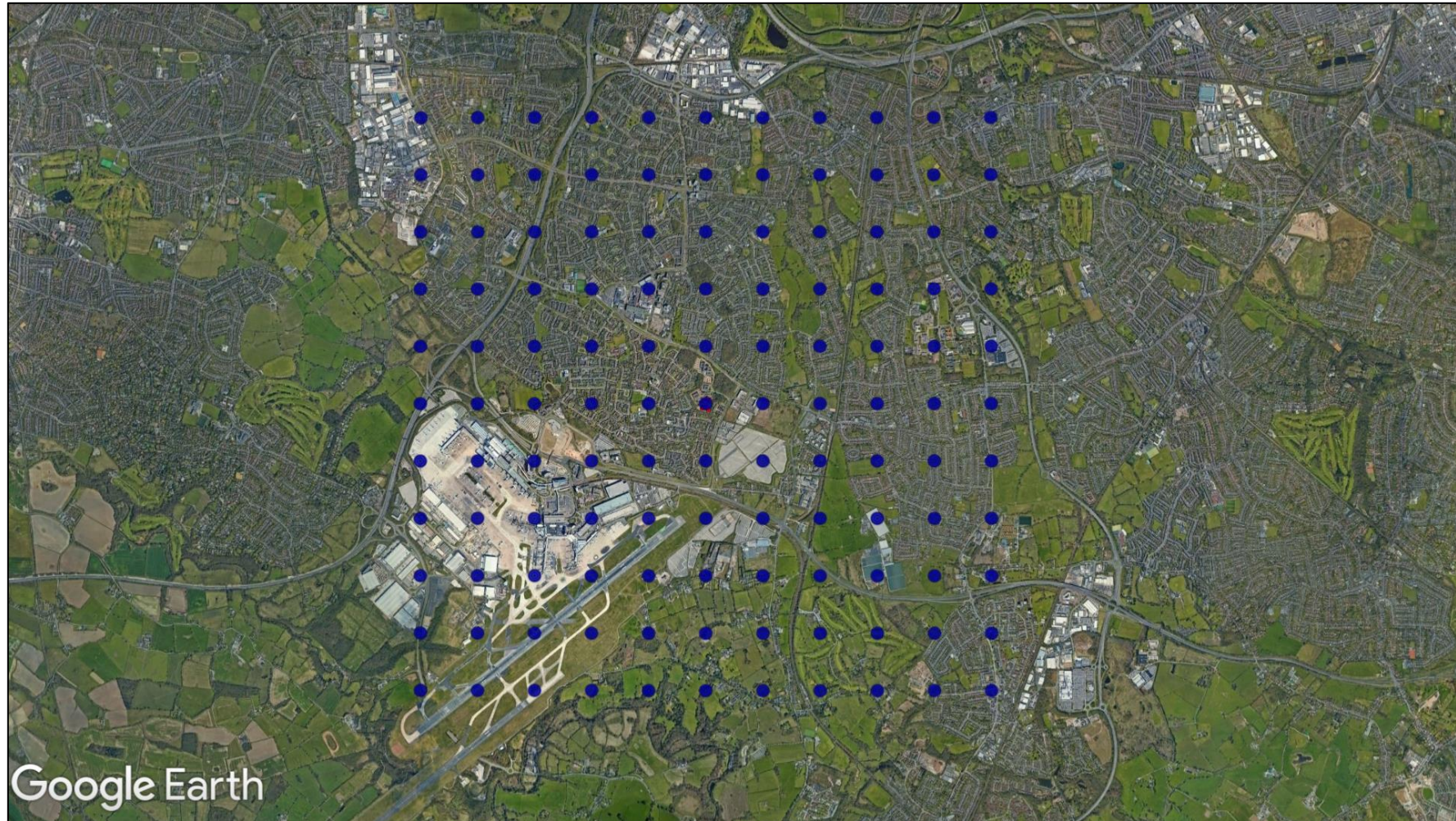
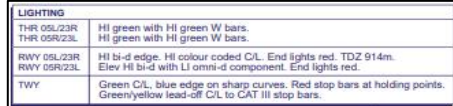
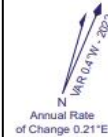


Figure 8 Manchester Airport 5km x 5km Lattice

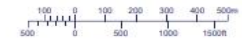


COM			
ARRIVAL ATIS	128.180	MANCHESTER INFO	
DEPARTURE ATIS	121.980	MANCHESTER DEPARTURE INFO	
TWR	118.630	119.405	MANCHESTER TOWER
	121.855		MANCHESTER GROUND
	121.705		MANCHESTER DELIVERY
	121.600		MANCHESTER FIRE

GL/ND (Geoid Undulation) = The height of the Geoid (MSL) above the Reference Ellipsoid (WGS 84) at the stated position.	
BEARINGS ARE MAGNETIC ELEVATIONS AND HEIGHTS ARE IN FEET	
ELEVATIONS IN FEET AMSL HEIGHTS IN FEET ABOVE AD	434 (177)



RUNWAY/TAXIWAY/APRON PHYSICAL CHARACTERISTICS				
APRON / RWY / TWY	SURFACE	BEARING STRENGTH	ELEVATION	
RWY 05L/23R	Concrete/Un grooved Asphalt	94/F/CW/T	-	-
RWY 05R/23L	Concrete/Grooved Asphalt	79/F/CW/T	-	-
Apron	Concrete	56/R/CW/T	-	-
Apron	Concrete	97/R/BW/T	-	-
Taxiway A	Concrete/Asphalt	66/F/CW/T	-	-
Taxiway A (between AC & B)	Concrete/Asphalt	66/F/CW/T	-	-
Taxiway S/T/U	Concrete/Asphalt	79/R/CW/T	-	-
Taxiway V/Y/A	Concrete/Asphalt	79/R/CW/T	-	-
Taxiway V/B/V/C	Concrete/Asphalt	79/R/CW/T	-	-
Taxiway W/Y	Concrete/Asphalt	79/R/CW/T	-	-
Taxiway (All other)	Concrete/Asphalt	95/R/CW/T	-	-



Solar Photovoltaic Glint and Glare Study

4.1.1 ATC Tower Details

Manchester Airport has one ATC Tower, which is 57m tall and located approximately 1.08km north of the runway 23L threshold. The location of the ATC Tower is shown in Figure 10 below, and a ground-based view of the ATC Tower is shown in Figure 11 on the following page.



Figure 10 Location of the ATC Tower within Manchester Airport



Figure 11 Ground-based view of the ATC Tower at Manchester Airport (visual control room circled)

5 ASSESSED REFLECTOR AREAS

5.1 Reflector Areas

The bounding coordinates for the proposed development have been extrapolated from the site plans. The data can be found in Appendix G. Figure 12 below shows the assessed reflector areas that have been used for modelling purposes.

The Pager Power model has used a resolution of 1m for this assessment. This means that a geometric calculation is undertaken for each identified receptor every 1m from within the defined areas. This resolution is sufficiently high to maximise the accuracy of the results – increasing the resolution further would not significantly change the modelling output. If a reflection is experienced from an assessed panel location, then it is likely that a reflection will be viewable from similarly located panels within the proposed solar development.

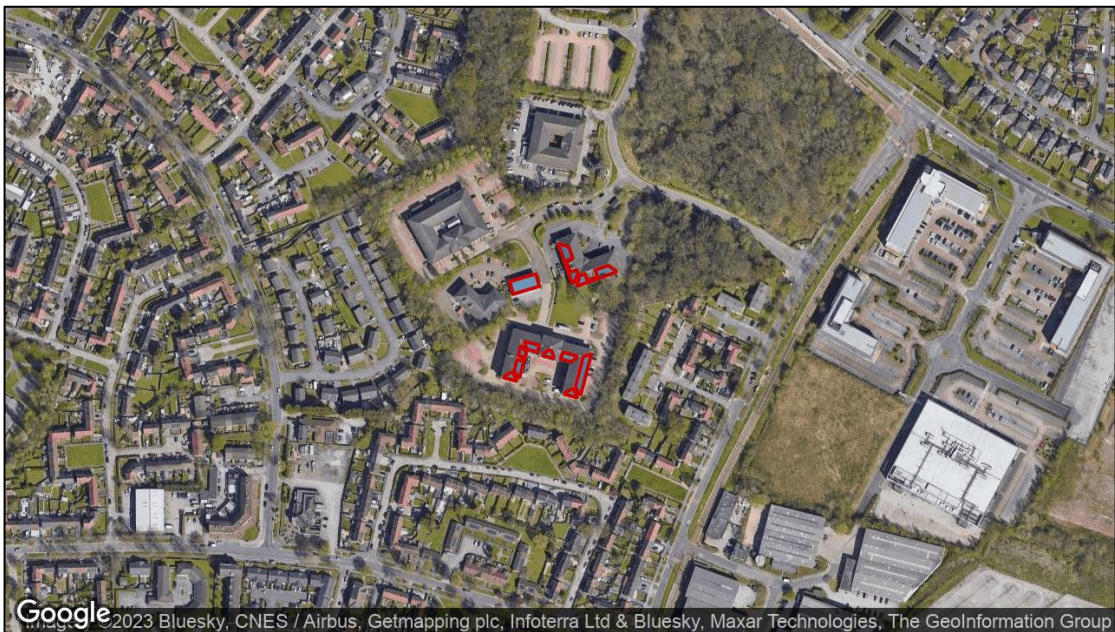


Figure 12 Assessed reflector areas

6 GLINT AND GLARE ASSESSMENT – TECHNICAL RESULTS

6.1 Overview

The Pager Power and Forge model has been used to determine whether reflections are possible. Intensity calculations in line with the Sandia National Laboratories methodology have been undertaken for aviation receptors. These calculations are routinely required for solar photovoltaic developments on or near aerodromes. The intensity model calculates the expected intensity of a reflection with respect to the potential for an after-image (or worse) occurring. The designation used by the model is presented in Table 2 below along with the associated colour coding.

Coding Used	Intensity Key
Glare beyond 50°	
Low potential	 Glare beyond 50 deg from pilot line-of-sight
Potential	 Low potential for temporary after-image
Potential for permanent eye damage	 Potential for temporary after-image
	 Potential for permanent eye damage

Table 2 Glare intensity designation

This coding has been used in the table where a reflection has been calculated and is in accordance with Sandia National Laboratories' methodology.

In addition, the intensity model allows for assessment of a variety of solar panel surface materials. In the first instance, a surface material of 'smooth glass without an anti-reflective coating' is assessed. This is the most reflective surface and allows for a 'worst case' assessment. Other surfaces that could be modelled include:

- Smooth glass with an anti-reflective coating;
- Light textured glass without an anti-reflective coating;
- Light textured glass with an anti-reflective coating; or
- Deeply textured glass.

If significant glare is predicted, modelling of less reflective surfaces could be undertaken.

The tables in the following subsections summarise the results of the assessment. The predicted glare times are based solely on bare-earth terrain i.e. without consideration of screening from buildings and vegetation. The final column summarises the predicted impact considering the level of predicted screening based on a desk-based review of the available imagery. The significance of any predicted impact is discussed in the subsequent report sections.

The modelling output showing the precise predicted times and the reflecting panel areas are shown in Appendix H.

6.2 Geometric Calculation Results – Aviation

6.2.1 Dakota House

The results of the geometric calculations for Dakota House are presented in Table 3 below.

Receptor/Runway	Geometric Modelling Result	Glare Intensity	Comment	Impact Classification	Mitigation Recommended?
ATC Tower	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 05L 10NM Approach	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 23R 10NM Approach	Solar reflections are geometrically possible between 2 nautical miles from the threshold and 10 nautical miles from the threshold		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible along this approach path	Low impact	No
Runway 05R 10NM Approach	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 23L 10NM Approach	Solar reflections are geometrically possible between 3 nautical miles from the threshold and 10 nautical miles from the threshold		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards this approach path	Low impact	No

Receptor/Runway	Geometric Modelling Result	Glare Intensity	Comment	Impact Classification	Mitigation Recommended?
Runway 05L 10NM Departure	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 23R 10NM Departure	Solar reflections are geometrically possible between 2 nautical miles from the threshold and 10 nautical miles from the threshold		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards this departure path	Low impact	No
Runway 05R 10NM Departure	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 23L 10NM Departure	Solar reflections are geometrically possible between 3 nautical miles from the threshold and 10 nautical miles from the threshold		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards this departure path	Low impact	No
Runway 05L/23R CA Circuits	Solar reflections are geometrically possible towards sections of the left-hand circuit for runway 05L		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards sections of this circuit	Low impact	No

Receptor/Runway	Geometric Modelling Result	Glare Intensity	Comment	Impact Classification	Mitigation Recommended?
Runway 05R/23L CA Circuits	Solar reflections are geometrically possible towards sections of the left-hand circuit for runway 05R		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards sections of this circuit	Low impact	No
Runway 05L/23R GA Circuits	Solar reflections are geometrically possible towards sections of the left-hand circuit for runway 05L		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards sections of this circuit	Low impact	No
Runway 05R/23L GA Circuits	Solar reflections are geometrically possible towards sections of the left-hand circuit for runway 05R		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards sections of this circuit	Low impact	No
5km x 5km Overhead Area	Solar reflections are geometrically possible towards sections of the lattice		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards the overhead area	Low impact	No

Table 3 Geometric analysis results – Dakota House

6.2.2 Rowan Court

The results of the geometric calculations for Rowan Court are presented in Table 4 below.

Receptor/Runway	Geometric Modelling Result	Glare Intensity	Comment	Impact Classification	Mitigation Recommended?
ATC Tower	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 05L 10NM Approach	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 23R 10NM Approach	Solar reflections are geometrically possible at 1 nautical mile from the threshold		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards this departure path	Low impact	No
Runway 05R 10NM Approach	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 23L 10NM Approach	Solar reflections are geometrically possible between 2 nautical miles from the threshold and 3 nautical miles from the threshold		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards this departure path	Low impact	No

Receptor/Runway	Geometric Modelling Result	Glare Intensity	Comment	Impact Classification	Mitigation Recommended?
Runway 05L 10NM Departure	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 23R 10NM Departure	Solar reflections are geometrically possible at 1 nautical mile from the threshold		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards this departure path	Low impact	No
Runway 05R 10NM Departure	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 23L 10NM Departure	Solar reflections are geometrically possible between 2 nautical miles from the threshold and 3 nautical miles from the threshold		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards this departure path	Low impact	No
Runway 05L/23R CA Circuits	Solar reflections are geometrically possible towards sections of the left-hand circuit for runway 05L		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards sections of this circuit	Low impact	No

Receptor/Runway	Geometric Modelling Result	Glare Intensity	Comment	Impact Classification	Mitigation Recommended?
Runway 05R/23L CA Circuits	Solar reflections are geometrically possible towards sections of the left-hand circuit for runway 05R		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards sections of this circuit	Low impact	No
Runway 05L/23R GA Circuits	Solar reflections are geometrically possible towards sections of the left-hand circuit for runway 05L		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards sections of this circuit	Low impact	No
Runway 05R/23L GA Circuits	Solar reflections are geometrically possible towards sections of the left-hand circuit for runway 05R		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards sections of this circuit	Low impact	No
5km x 5km Overhead Area	Solar reflections are geometrically possible towards sections of the lattice		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards the overhead area	Low impact	No

Table 4 Geometric analysis results – Rowan Court

6.2.3 Coffee Shop

The results of the geometric calculations for the Coffee Shop are presented in Table 5 below.

Receptor/Runway	Geometric Modelling Result	Glare Intensity	Comment	Impact Classification	Mitigation Recommended?
ATC Tower	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 05L 10NM Approach	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 23R 10NM Approach	Solar reflections are geometrically possible between the threshold and 10 nautical miles from the threshold		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards this approach path	Low impact	No
Runway 05R 10NM Approach	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 23L 10NM Approach	Solar reflections are geometrically possible between 2 nautical miles from the threshold and 10 nautical miles from the threshold		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards this approach path	Low impact	No

Receptor/Runway	Geometric Modelling Result	Glare Intensity	Comment	Impact Classification	Mitigation Recommended?
Runway 05L 10NM Departure	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 23R 10NM Departure	Solar reflections are geometrically possible between 1 nautical mile from the threshold and 4 nautical miles from the threshold		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards this departure path	Low impact	No
Runway 05R 10NM Departure	No solar reflections geometrically possible	N/A	N/A	No impact	No
Runway 23L 10NM Departure	Solar reflections are geometrically possible between 2 nautical miles from the threshold and 8 nautical miles from the threshold		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards this departure path	Low impact	No
Runway 05L/23R CA Circuits	Solar reflections are geometrically possible towards sections of the left-hand circuit for runway 05L		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards sections of this circuit	Low impact	No

Receptor/Runway	Geometric Modelling Result	Glare Intensity	Comment	Impact Classification	Mitigation Recommended?
Runway 05R/23L CA Circuits	Solar reflections are geometrically possible towards sections of the left-hand circuit for runway 05R		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards sections of this circuit	Low impact	No
Runway 05L/23R GA Circuits	Solar reflections are geometrically possible towards sections of the left-hand circuit for runway 05L		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards sections of this circuit	Low impact	No
Runway 05R/23L GA Circuits	Solar reflections are geometrically possible towards sections of the left-hand circuit for runway 05R		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards sections of this circuit	Low impact	No
5km x 5km Overhead Area	Solar reflections are geometrically possible towards sections of the lattice		Solar reflections with a maximum intensity of 'low potential for temporary after-image' are possible towards the overhead area	Low impact	No

Table 5 Geometric analysis results – Coffee Shop

7 GEOMETRIC ASSESSMENT RESULTS AND DISCUSSION

7.1 Overview

The following sub-section presents the significance of any predicted impact in the context of existing screening and the relevant criteria set out in each sub-section. The criteria are determined by the assessment process for each receptor, which are set out in Appendix D.

When determining the visibility of the reflecting panels for an observer, a conservative review of the available imagery and proposed screening has been undertaken, whereby it is assumed views of the panels are possible if it cannot be reliably determined that existing screening will remove effects.

7.2 Dakota House

7.2.1 ATC Tower

The modelling has shown that solar reflections are not geometrically possible towards the ATC Tower.

7.2.2 Runway Approaches

The analysis has shown that solar reflections are predicted towards both the 10NM approach and departure paths for runway 23R, between 2 and 10 nautical miles from the threshold. Solar reflections are also predicted towards the approaches and departures for runway 23L, between 3 and 10 nautical miles from the threshold.

It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards these runway approaches, which is acceptable in accordance with the associated guidance (appendix D) and industry best practice. A low impact is predicted for these approaches, and no mitigation is required.

No solar reflections are predicted towards the CA and GA approaches for runways 05L and 05R. No impact is predicted and no mitigation is required.

7.2.3 Visual Circuits

The analysis has shown that solar reflections are predicted towards sections of the left-hand CA and GA circuits for runways 05L and 05R.

It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards circuits at Manchester Airport, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

7.2.4 5km x 5km Overhead Area

The analysis has shown that solar reflections are predicted towards sections of the 5km x 5km overhead area centred upon the proposed development at 2500ft agl.

It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards this lattice, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

7.3 Rowan Court

7.3.1 ATC Tower

The modelling has shown that solar reflections are not geometrically possible towards the ATC Tower.

7.3.2 Runway Approaches

The analysis has shown that solar reflections are predicted towards both the 10MN approach and departure paths for runway 23R, at 1 nautical mile from the threshold. Solar reflections are also predicted towards the CA and GA approaches for runway 23L, between 2 and 3 nautical miles from the threshold.

It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards these runway approaches, which is acceptable in accordance with the associated guidance (appendix D) and industry best practice. A low impact is predicted for these approaches, and no mitigation is required.

No solar reflections are predicted towards the CA and GA approaches for runways 05L and 05R. No impact is predicted and no mitigation is required.

7.3.3 Visual Circuits

The analysis has shown that solar reflections are predicted towards sections of the left-hand CA and GA circuits for runways 05L and 05R.

It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards circuits at Manchester Airport, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

7.3.4 5km x 5km Overhead Area

The analysis has shown that solar reflections are predicted towards sections of the 5km x 5km overhead area centred upon the proposed development at 2500ft agl.

It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards this lattice, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

7.4 Coffee Shop

7.4.1 ATC Tower

The modelling has shown that solar reflections are not geometrically possible towards the ATC Tower.

7.4.2 Runway Approaches

The analysis has shown that solar reflections are predicted towards both the 10NM approach and departure paths for runway 23R, between the threshold and 10 nautical miles from the threshold. Solar reflections are also predicted towards the CA and GA approaches for runway 23L, between 2 and 10 nautical miles from the threshold.

It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards these runway approaches, which is acceptable in accordance with the associated guidance (appendix D) and industry best practice. A low impact is predicted for these approaches, and no mitigation is required.

No solar reflections are predicted towards the CA and GA approaches for runways 05L and 05R. No impact is predicted and no mitigation is required.

7.4.3 Visual Circuits

The analysis has shown that solar reflections are predicted towards sections of the left-hand CA and GA circuits for runways 05L and 05R.

It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards circuits at Manchester Airport, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

7.4.4 5km x 5km Overhead Area

The analysis has shown that solar reflections are predicted towards sections of the 5km x 5km overhead area centred upon the proposed development at 2500ft agl.

It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards this lattice, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

8 OVERALL CONCLUSIONS

8.1 Assessment Conclusions – Manchester Airport

8.1.1 Dakota House

Solar reflections are not geometrically possible towards the ATC Tower at Manchester Airport. No impact is predicted, and no mitigation is required.

The analysis has shown that solar reflections are predicted towards sections of the 10NM approach and departure paths for runways 23L and 23R. It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards these runway approaches, which is acceptable in accordance with the associated guidance (appendix D) and industry best practice pertaining to 2-mile approach paths, which state that this level of glare intensity is acceptable. A low impact is predicted for these approaches, and no mitigation is required.

Glare intensities of 'low potential for temporary after-image' are predicted upon sections of the Civil Aviation (CA) and General Aviation (GA) left-hand circuits for runways 05L and 05R, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

Glare intensities of 'low potential for temporary after-image' are predicted upon sections of the 5km x 5km overhead area centred upon the proposed development, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

8.1.2 Rowan Court

Solar reflections are not geometrically possible towards the ATC Tower at Manchester Airport. No impact is predicted, and no mitigation is required.

The analysis has shown that solar reflections are predicted towards sections of the 10NM approach and departure paths for runways 23L and 23R. It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards these runway approaches, which is acceptable in accordance with the associated guidance and industry best practice pertaining to 2-mile approach paths, which state that this level of glare intensity is acceptable. A low impact is predicted for these approaches, and no mitigation is required.

Glare intensities of 'low potential for temporary after-image' are predicted upon sections of the CA and GA left-hand circuits for runways 05L and 05R, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

Glare intensities of 'low potential for temporary after-image' are predicted upon sections of the 5km x 5km overhead area centred upon the proposed development, which is acceptable in

accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

8.1.3 Coffee Shop

Solar reflections are not geometrically possible towards the ATC Tower at Manchester Airport. No impact is predicted, and no mitigation is required.

The analysis has shown that solar reflections are predicted towards sections of the 10NM approach and departure paths for runways 23L and 23R. It is predicted that solar reflections with glare intensities no greater than 'low potential for temporary after-image' will be experienced towards these runway approaches, which is acceptable in accordance with the associated guidance and industry best practice pertaining to 2-mile approach paths, which state that this level of glare intensity is acceptable. A low impact is predicted for these approaches, and no mitigation is required.

Glare intensities of 'low potential for temporary after-image' are predicted upon sections of the CA and GA left-hand circuits for runways 05L and 05R, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

Glare intensities of 'low potential for temporary after-image' are predicted upon sections of the 5km x 5km overhead area centred upon the proposed development, which is acceptable in accordance with the associated guidance and industry best practice. A low impact is predicted, and no mitigation is required.

8.2 Overall Conclusions

No significant impacts are predicted upon aviation activity at Manchester Airport and no mitigation is required. It is recommended that these results are shared with Manchester Airport to understand their position towards the proposed development.

APPENDIX A – OVERVIEW OF GLINT AND GLARE GUIDANCE

Overview

This section presents details regarding the relevant guidance and studies with respect to the considerations and effects of solar reflections from solar panels, known as 'Glint and Glare'.

This is not a comprehensive review of the data sources, rather it is intended to give an overview of the important parameters and considerations that have informed this assessment.

UK Planning Policy

Renewable and Low Carbon Energy

The National Planning Policy Framework under the planning practice guidance for Renewable and Low Carbon Energy⁸ (specifically regarding the consideration of solar farms, paragraph 013) states:

'What are the particular planning considerations that relate to large scale ground-mounted solar photovoltaic Farms?

The deployment of large-scale solar farms can have a negative impact on the rural environment, particularly in undulating landscapes. However, the visual impact of a well-planned and well-screened solar farm can be properly addressed within the landscape if planned sensitively.

Particular factors a local planning authority will need to consider include:

...

- the proposal's visual impact, the effect on landscape of glint and glare (see guidance on landscape assessment) and on **neighbouring uses and aircraft safety**;
- the extent to which there may be additional impacts if solar arrays follow the daily movement of the sun;

...

The approach to assessing cumulative landscape and visual impact of large scale solar farms is likely to be the same as assessing the impact of wind turbines. However, in the case of ground-mounted solar panels it should be noted that with effective screening and appropriate land topography the area of a zone of visual influence could be zero.'

⁸ [Renewable and low carbon energy](#), Ministry of Housing, Communities & Local Government, date: 18 June 2015, accessed on: 01/11/2021

Draft National Policy Statement for Renewable Energy Infrastructure

The Draft National Policy Statement for Renewable Energy Infrastructure (EN-3)⁹ sets out the primary policy for decisions by the Secretary of State for nationally significant renewable energy infrastructure. Section 2.52 states:

- ‘2.52.1 Solar panels may reflect the sun’s rays, causing glint and glare. Glint is defined as a momentary flash of light that may be produced as a direct reflection of the sun in the solar panel. Glare is a continuous source of excessive brightness experienced by a stationary observer located in the path of reflected sunlight from the face of the panel. The effect occurs when the solar panel is stationed between or at an angle of the sun and the receptor.
- 2.52.2 In some instances, it may be necessary to seek a glint and glare assessment as part of the application. This may need to account for ‘tracking’ panels if they are proposed as these may cause differential diurnal and/or seasonal impacts. The potential for solar PV panels, frames and supports to have a combined reflective quality should be assessed. This assessment needs to consider the likely reflective capacity of all of the materials used¹⁰ in the construction of the solar PV farm.
- 2.52.3 Applicants should consider using, and in some cases the Secretary of State may require, solar panels to be of a non-glare/ non-reflective type and the front face of the panels to comprise of (or be covered) with a non-reflective coating for the lifetime of the permission.
- 2.52.4 Solar PV panels are designed to absorb, not reflect, irradiation. However, the Secretary of State should assess the potential impact of glint and glare on nearby homes and motorists.
- 2.52.5 There is no evidence that glint and glare from solar farms interferes in any way with aviation navigation or pilot and aircraft visibility or safety. Therefore, the Secretary of State is unlikely to have to give any weight to claims of aviation interference as a result of glint and glare from solar farms.’

Consultation to determine whether EN-3 provides a suitable framework to support decision making for nationally significant energy infrastructure ended in November 2021. Pager Power is aware that aviation stakeholders were not consulted prior to the publication of the draft policy and understands that they will still request a glint and glare assessment on the basis that glare may lead to impact upon aviation safety. It is possible that the draft policy will change in light of the consultation responses from aviation stakeholders.

⁹ Draft National Policy Statement for Renewable Energy Infrastructure (EN-3), Department for Business, Energy & Industrial Strategy, date: September 2021, accessed on: 01/11/2021.

¹⁰ In Pager Power’s experience, the solar panels themselves are the overriding source of specular reflections which have the potential to cause significant impacts upon safety or amenity.

Finally, it should be noted that the EN-3 relates solely to nationally significant renewable energy infrastructure and therefore does not apply to all planning applications for solar farms.

Aviation Assessment Guidance

The UK Civil Aviation Authority (CAA) issued interim guidance relating to Solar Photovoltaic Systems (SPV) on 17 December 2010 and was subject to a CAA information alert 2010/53. The formal policy was cancelled on September 7th, 2012¹¹ however the advice is still applicable¹² until a formal policy is developed. The relevant aviation guidance from the CAA is presented in the section below.

CAA Interim Guidance

This interim guidance makes the following recommendations (p.2-3):

'8. It is recommended that, as part of a planning application, the SPV developer provide safety assurance documentation (including risk assessment) regarding the full potential impact of the SPV installation on aviation interests.

9. Guidance on safeguarding procedures at CAA licensed aerodromes is published within CAP 738 Safeguarding of Aerodromes and advice for unlicensed aerodromes is contained within CAP 793 Safe Operating Practices at Unlicensed Aerodromes.

10. Where proposed developments in the vicinity of aerodromes require an application for planning permission the relevant LPA normally consults aerodrome operators or NATS when aeronautical interests might be affected. This consultation procedure is a statutory obligation in the case of certain major airports, and may include military establishments and certain air traffic surveillance technical sites. These arrangements are explained in Department for Transport Circular 1/2003 and for Scotland, Scottish Government Circular 2/2003.

11. In the event of SPV developments proposed under the Electricity Act, the relevant government department should routinely consult with the CAA. There is therefore no requirement for the CAA to be separately consulted for such proposed SPV installations or developments.

12. If an installation of SPV systems is planned on-aerodrome (i.e. within its licensed boundary) then it is recommended that data on the reflectivity of the solar panel material should be included in any assessment before installation approval can be granted. Although approval for installation is the responsibility of the ALH¹³, as part of a condition of a CAA Aerodrome Licence, the ALH is required to obtain prior consent from CAA Aerodrome Standards Department before any work is begun or approval to the developer or LPA is granted, in accordance with the procedures set out in CAP 791 Procedures for Changes to Aerodrome Infrastructure.

¹¹ Archived at Pager Power

¹² Reference email from the CAA dated 19/05/2014.

¹³ Aerodrome Licence Holder.

13. During the installation and associated construction of SPV systems there may also be a need to liaise with nearby aerodromes if cranes are to be used; CAA notification and permission is not required.

14. The CAA aims to replace this informal guidance with formal policy in due course and reserves the right to cancel, amend or alter the guidance provided in this document at its discretion upon receipt of new information.

15. Further guidance may be obtained from CAA's Aerodrome Standards Department via aerodromes@caa.co.uk.

FAA Guidance

The most comprehensive guidelines available for the assessment of solar developments near aerodromes has been produced by the United States Federal Aviation Administration (FAA). The first guidelines were produced initially in November 2010 and updated in 2013. A final policy was released in 2021, which superseded the interim guidance.

The 2010 document is entitled 'Technical Guidance for Evaluating Selected Solar Technologies on Airports'¹⁴, the 2013 update is entitled 'Interim Policy, FAA Review of Solar Energy System Projects on Federally Obligated Airports'¹⁵, and the 2021 final policy is entitled 'Federal Aviation Administration Policy: Review of Solar Energy System Projects on Federally-Obligated Airports'¹⁶.

Key excerpts from the final policy are presented below:

Initially, FAA believed that solar energy systems could introduce a novel glint and glare effect to pilots on final approach. FAA has subsequently concluded that in most cases, the glint and glare from solar energy systems to pilots on final approach is similar to glint and glare pilots routinely experience from water bodies, glass-façade buildings, parking lots, and similar features. However, FAA has continued to receive reports of potential glint and glare from on-airport solar energy systems on personnel working in ATCT cabs. Therefore, FAA has determined the scope of agency policy should be focused on the impact of on-airport solar energy systems to federally-obligated towered airports, specifically the airport's ATCT cab.

The policy in this document updates and replaces the previous policy by encouraging airport sponsors to conduct an ocular analysis of potential impacts to ATCT cabs prior to submittal of a Notice of Proposed Construction or Alteration Form 7460-1 (hereinafter Form 7460-1). Airport sponsors are no longer required to submit the results of an ocular analysis to FAA. Instead, to demonstrate compliance with 14 CFR 77.5(c), FAA will rely on the submittal of Form 7460-1 in which the sponsor confirms that it has analyzed the potential for glint and glare and determined

¹⁴ Archived at Pager Power

¹⁵ [Interim Policy, FAA Review of Solar Energy System Projects on Federally Obligated Airports](#), Department of Transportation, Federal Aviation Administration (FAA), date: 10/2013, accessed on: 08/12/2021.

¹⁶ [Federal Aviation Administration Policy: Review of Solar Energy System Projects on Federally-Obligated Airports](#), Federal Aviation Administration, date: May 2021, accessed on: 08/12/2021.

there is no potential for ocular impact to the airport's ATCT cab. This process will enable FAA to evaluate the solar energy system project, with assurance that the system will not impact the ATCT cab.

FAA encourages airport sponsors of federally-obligated towered airports to conduct a sufficient analysis to support their assertion that a proposed solar energy system will not result in ocular impacts. There are several tools available on the open market to airport sponsors that can analyze potential glint and glare to an ATCT cab. For proposed systems that will clearly not impact ATCT cabs (e.g., on-airport solar energy systems that are blocked from the ATCT cab's view by another structure), the use of such tools may not be necessary to support the assertion that a proposed solar energy system will not result in ocular impacts.

The excerpt above states where a solar PV development is to be located on a federally obligated aerodrome with an ATC Tower, it will require a glint and glare assessment to accompany its application. It states that pilots on approach are no longer a specific assessment requirement due to effects from solar energy systems being similar to glint and glare pilots routinely experience from water bodies, glass-façade buildings, parking lots, and similar features. Ultimately it comes down to the specific aerodrome to ensure it is adequately safeguarded, and it is on this basis that glint and glare assessments are routinely still requested.

The policy also states that several different tools and methodologies can be used to assess the impacts of glint and glare, which was previously required to be undertaken by the Solar Glare Hazard Analysis Tool (SGHAT) using the Sandia National Laboratories methodology.

In 2018, the FAA released the latest version (Version 1.1) of the 'Technical Guidance for Evaluating Selected Solar Technologies on Airports'¹⁷. Whilst the 2021 final policy also supersedes this guidance, many of the points are still relevant because aerodromes are still safeguarding against glint and glare irrespective of the FAA guidance. The key points are presented below for reference:

- Reflectivity refers to light that is reflected off surfaces. The potential effects of reflectivity are glint (a momentary flash of bright light) and glare (a continuous source of bright light). These two effects are referred to hereinafter as "glare," which can cause a brief loss of vision, also known as flash blindness¹⁸.
- The amount of light reflected off a solar panel surface depends on the amount of sunlight hitting the surface, its surface reflectivity, geographic location, time of year, cloud cover, and solar panel orientation.

¹⁷ [Technical Guidance for Evaluating Selected Solar Technologies on Airports](#), Federal Aviation Administration (FAA), date: 04/2018, accessed on: 08/12/2021.

¹⁸ Flash Blindness, as described in the FAA guidelines, can be described as a temporary visual interference effect that persists after the source of illumination has ceased. This occurs from many reflective materials in the ambient environment.

- As illustrated on Figure 16¹⁹, flat, smooth surfaces reflect a more concentrated amount of sunlight back to the receiver, which is referred to as specular reflection. The more a surface is polished, the more it shines. Rough or uneven surfaces reflect light in a diffused or scattered manner and, therefore, the light will not be received as bright.
- Because the FAA has no specific standards for airport solar facilities and potential glare, the type of glare analysis may vary. Depending on site specifics (e.g., existing land uses, location and size of the project) an acceptable evaluation could involve one or more of the following levels of assessment:
 - A qualitative analysis of potential impact in consultation with the Control Tower, pilots and airport officials;
 - A demonstration field test with solar panels at the proposed site in coordination with FAA Tower personnel;
 - A geometric analysis to determine days and times when an impact is predicted.
- The extent of reflectivity analysis required to assess potential impacts will depend on the specific project site and system design.
- **1. Assessing Baseline Reflectivity Conditions** – Reflection in the form of glare is present in current aviation operations. The existing sources of glare come from glass windows, auto surface parking, rooftops, and water bodies. At airports, existing reflecting surfaces may include hangar roofs, surface parking, and glassy office buildings. To minimize unexpected glare, windows of air traffic control towers and airplane cockpits are coated with anti-reflective glazing. Operators also wear polarized eye wear. Potential glare from solar panels should be viewed in this context. Any airport considering a solar PV project should first review existing sources of glare at the airport and the effectiveness of measures used to mitigate that glare.
- **2. Tests in the Field** – Potential glare from solar panels can easily be viewed at the airport through a field test. A few airports have coordinated these tests with FAA Air Traffic Controllers to assess the significance of glare impacts. To conduct such a test, a sponsor can take a solar panel out to proposed location of the solar project, and tilt the panel in different directions to evaluate the potential for glare onto the air traffic control tower. For the two known cases where a field test was conducted, tower personnel determined the glare was not significant. If there is a significant glare impact, the project can be modified by ensuring panels are not directed in that direction.
- **3. Geometric Analysis** – Geometric studies are the most technical approach for reflectivity issues. They are conducted when glare is difficult to assess through other methods. Studies of glare can employ geometry and the known path of the sun to predict when sunlight will reflect off of a fixed surface (like a solar panel) and contact a fixed receptor (e.g., control tower). At any given site, the sun moves across the sky every day and its path in the sky changes throughout year. This in turn alters the

¹⁹ First figure in Appendix B.

destination of the resultant reflections since the angle of reflection for the solar panels will be the same as the angle at which the sun hits the panels. The larger the reflective surface, the greater the likelihood of glare impacts.

- Facilities placed in remote locations, like the desert, will be far from receptors and therefore potential impacts are limited to passing aircraft. Because the intensity of the light reflected from the solar panel decreases with increasing distance, an appropriate question is how far you need to be from a solar reflected surface to avoid flash blindness. It is known that this distance is directly proportional to the size of the array in question²⁰ but still requires further research to definitively answer.
- **Experiences of Existing Airport Solar Projects** – Solar installations are presently operating at a number of airports, including megawatt-sized solar facilities covering multiple acres. Air traffic control towers have expressed concern about glint and glare from a small number of solar installations. These were often instances when solar installations were sited between the tower and airfield, or for installations with inadequate or no reflectivity analysis. Adequate reflectivity analysis and alternative siting addressed initial issues at those installations.

Air Navigation Order (ANO) 2016

In some instances, an aviation stakeholder can refer to the ANO 2016²¹ with regard to safeguarding. Key points from the document are presented below.

Lights liable to endanger

224. (1) A person must not exhibit in the United Kingdom any light which—

(a) by reason of its glare is liable to endanger aircraft taking off from or landing at an aerodrome; or

(b) by reason of its liability to be mistaken for an aeronautical ground light is liable to endanger aircraft.

(2) If any light which appears to the CAA to be a light described in paragraph (1) is exhibited, the CAA may direct the person who is the occupier of the place where the light is exhibited or who has charge of the light, to take such steps within a reasonable time as are specified in the direction—

(a) to extinguish or screen the light; and

(b) to prevent in the future the exhibition of any other light which may similarly endanger aircraft.

²⁰ Ho, Clifford, Cheryl Ghanbari, and Richard Diver. 2009. Hazard Analysis of Glint and Glare From Concentrating Solar Power Plants. SolarPACES 2009, Berlin Germany. Sandia National Laboratories.

²¹ The Air Navigation Order 2016. [online] Available at: <<https://www.legislation.gov.uk/uksi/2016/765/contents/made>> [Accessed 4 February 2022].

(3) The direction may be served either personally or by post, or by affixing it in some conspicuous place near to the light to which it relates.

(4) In the case of a light which is or may be visible from any waters within the area of a general lighthouse authority, the power of the CAA under this article must not be exercised except with the consent of that authority.

Lights which dazzle or distract

225. A person must not in the United Kingdom direct or shine any light at any aircraft in flight so as to dazzle or distract the pilot of the aircraft.'

The document states that no 'light', 'dazzle' or 'glare' should be produced which will create a detrimental impact upon aircraft safety.

Endangering safety of an aircraft

240. A person must not recklessly or negligently act in a manner likely to endanger an aircraft, or any person in an aircraft.

Endangering safety of any person or property

241. A person must not recklessly or negligently cause or permit an aircraft to endanger any person or property

APPENDIX B – OVERVIEW OF GLINT AND GLARE STUDIES

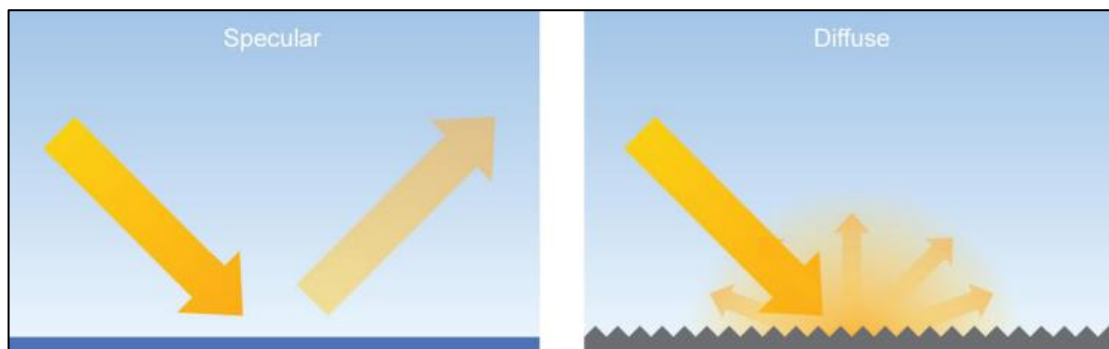
Overview

Studies have been undertaken assessing the type and intensity of solar reflections from various surfaces including solar panels and glass. An overview of these studies is presented below.

The guidelines presented are related to aviation safety. The results are applicable for the purpose of this analysis.

Reflection Type from Solar Panels

Based on the surface conditions reflections from light can be specular and diffuse. A specular reflection has a reflection characteristic similar to that of a mirror; a diffuse will reflect the incoming light and scatter it in many directions. The figure below, taken from the FAA guidance²², illustrates the difference between the two types of reflections. Because solar panels are flat and have a smooth surface most of the light reflected is specular, which means that incident light from a specific direction is reradiated in a specific direction.



Specular and diffuse reflections

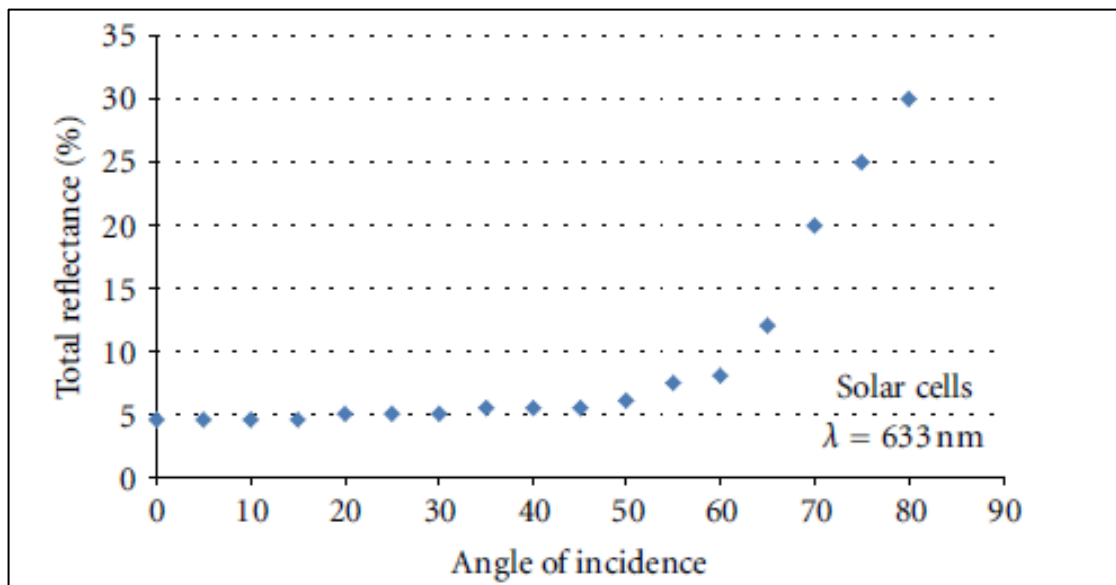
²²Technical Guidance for Evaluating Selected Solar Technologies on Airports, Federal Aviation Administration (FAA), date: 04/2018, accessed on: 20/03/2019.

Solar Reflection Studies

An overview of content from identified solar panel reflectivity studies is presented in the subsections below.

Evan Riley and Scott Olson, "A Study of the Hazardous Glare Potential to Aviators from Utility-Scale Flat-Plate Photovoltaic Systems"

Evan Riley and Scott Olson published in 2011 their study titled: A Study of the Hazardous Glare Potential to Aviators from Utility-Scale Flat-Plate Photovoltaic Systems²³. They researched the potential glare that a pilot could experience from a 25 degree fixed tilt PV system located outside of Las Vegas, Nevada. The theoretical glare was estimated using published ocular safety metrics which quantify the potential for a postflash glare after-image. This was then compared to the postflash glare after-image caused by smooth water. The study demonstrated that the reflectance of the solar cell varied with angle of incidence, with maximum values occurring at angles close to 90 degrees. The reflectance values varied from approximately 5% to 30%. This is shown on the figure below.



Total reflectance % when compared to angle of incidence

The conclusions of the research study were:

- The potential for hazardous glare from flat-plate PV systems is similar to that of smooth water;
- Portland white cement concrete (which is a common concrete for runways), snow, and structural glass all have a reflectivity greater than water and flat plate PV modules.

²³ Evan Riley and Scott Olson, "A Study of the Hazardous Glare Potential to Aviators from Utility-Scale Flat-Plate Photovoltaic Systems," ISRN Renewable Energy, vol. 2011, Article ID 651857, 6 pages, 2011. doi:10.5402/2011/651857

FAA Guidance – “Technical Guidance for Evaluating Selected Solar Technologies on Airports”²⁴

The 2010 FAA Guidance included a diagram which illustrates the relative reflectance of solar panels compared to other surfaces. The figure shows the relative reflectance of solar panels compared to other surfaces. Surfaces in this figure produce reflections which are specular and diffuse. A specular reflection (those made by most solar panels) has a reflection characteristic similar to that of a mirror. A diffuse reflection will reflect the incoming light and scatter it in many directions. A table of reflectivity values, sourced from the figure within the FAA guidance, is presented below.

Surface	Approximate Percentage of Light Reflected ²⁵
Snow	80
White Concrete	77
Bare Aluminium	74
Vegetation	50
Bare Soil	30
Wood Shingle	17
Water	5
Solar Panels	5
Black Asphalt	2

Relative reflectivity of various surfaces

Note that the data above does not appear to consider the reflection type (specular or diffuse).

An important comparison in this table is the reflectivity compared to water which will produce a reflection of very similar intensity when compared to that from a solar panel. The study by Riley and Olsen study (2011) also concludes that still water has a very similar reflectivity to solar panels.

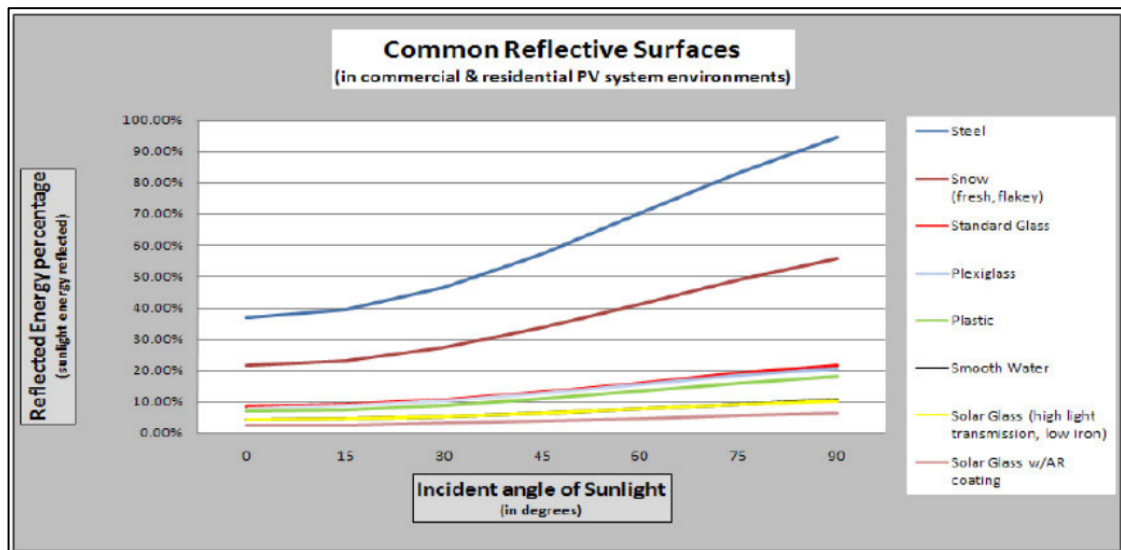
²⁴ Technical Guidance for Evaluating Selected Solar Technologies on Airports, Federal Aviation Administration (FAA), date: 04/2018, accessed on: 20/03/2019.

²⁵ Extrapolated data, baseline of 1,000 W/m² for incoming sunlight.

SunPower Technical Notification (2009)

SunPower published a technical notification²⁶ to 'increase awareness concerning the possible glare and reflectance impact of PV Systems on their surrounding environment'.

The figure presented below shows the relative reflectivity of solar panels compared to other natural and manmade materials including smooth water, standard glass and steel.



Common reflective surfaces

The results, similarly to those from Riley and Olsen study (2011) and the FAA (2010), show that solar panels produce a reflection that is less intense than those of 'standard glass and other common reflective surfaces'.

With respect to aviation and solar reflections observed from the air, SunPower has developed several large installations near airports or on Air Force bases. It is stated that these developments have all passed FAA or Air Force standards with all developments considered "No Hazard to Air Navigation". The note suggests that developers discuss any possible concerns with stakeholders near proposed solar farms.

²⁶ Source: Technical Support, 2009. SunPower Technical Notification – Solar Module Glare and Reflectance.

APPENDIX C – OVERVIEW OF SUN MOVEMENTS AND RELATIVE REFLECTIONS

The Sun's position in the sky can be accurately described by its azimuth and elevation. Azimuth is a direction relative to true north (horizontal angle i.e. from left to right) and elevation describes the Sun's angle relative to the horizon (vertical angle i.e. up and down).

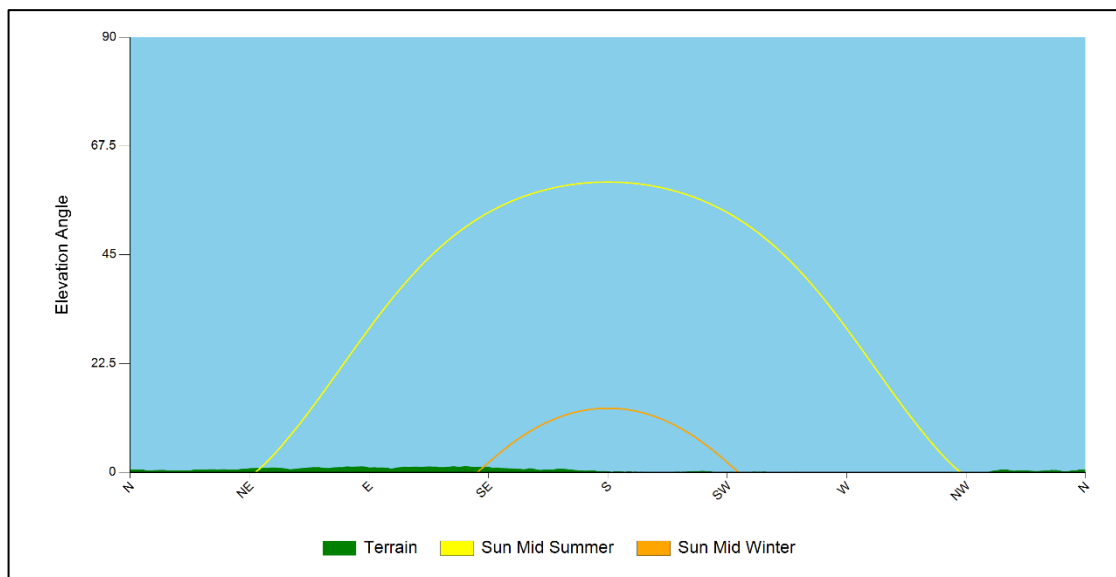
The Sun's position can be accurately calculated for a specific location. The following data being used for the calculation:

- Time;
- Date;
- Latitude;
- Longitude.

The following is true at the location of the solar development:

- The Sun is at its highest around midday and is to the south at this time;
- The Sun rises highest on 21 June (longest day);
- On 21 December, the maximum elevation reached by the Sun is at its lowest (shortest day).

The combination of the Sun's azimuth angle and vertical elevation will affect the direction and angle of the reflection from a reflector. The figure below shows terrain at the horizon from the proposed development location as well as the sunrise and sunset curves throughout the year.



Sunrise and sunset curves

APPENDIX D – GLINT AND GLARE IMPACT SIGNIFICANCE

Overview

The significance of glint and glare will vary for different receptors. The following section presents a general overview of the significance criteria with respect to experiencing a solar reflection.

Impact Significance Definition

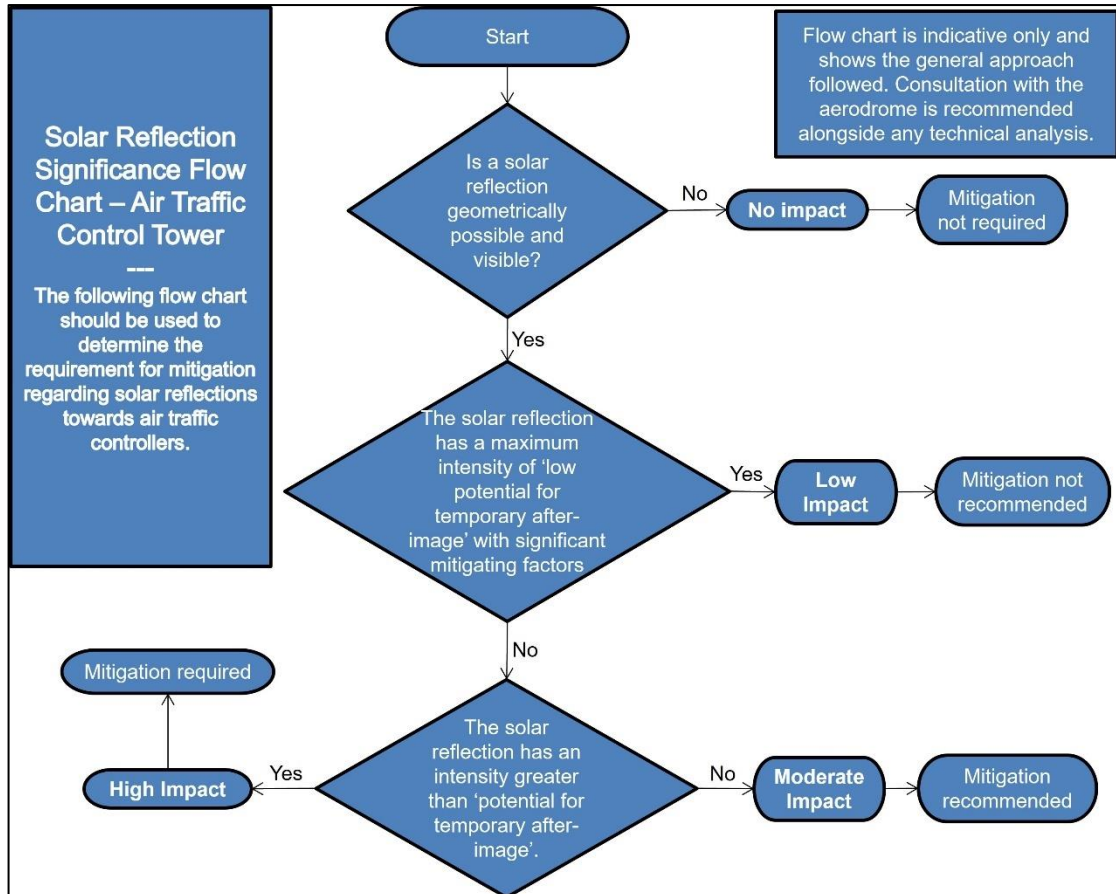
The table below presents the recommended definition of 'impact significance' in glint and glare terms and the requirement for mitigation under each.

Impact Significance	Definition	Mitigation
No Impact	A solar reflection is not geometrically possible or will not be visible from the assessed receptor.	No mitigation required.
Low	A solar reflection is geometrically possible however any impact is considered to be small such that mitigation is not required e.g. intervening screening will limit the view of the reflecting solar panels significantly.	No mitigation recommended.
Moderate	A solar reflection is geometrically possible and visible however it occurs under conditions that do not represent a worst-case given individual receptor criteria.	Mitigation recommended.
High	A solar reflection is geometrically possible and visible under worst-case conditions that will produce a significant impact given individual receptor criteria	Mitigation will be required if the proposed development is to proceed.

Impact significance definition

Impact Significance Determination for ATC Towers

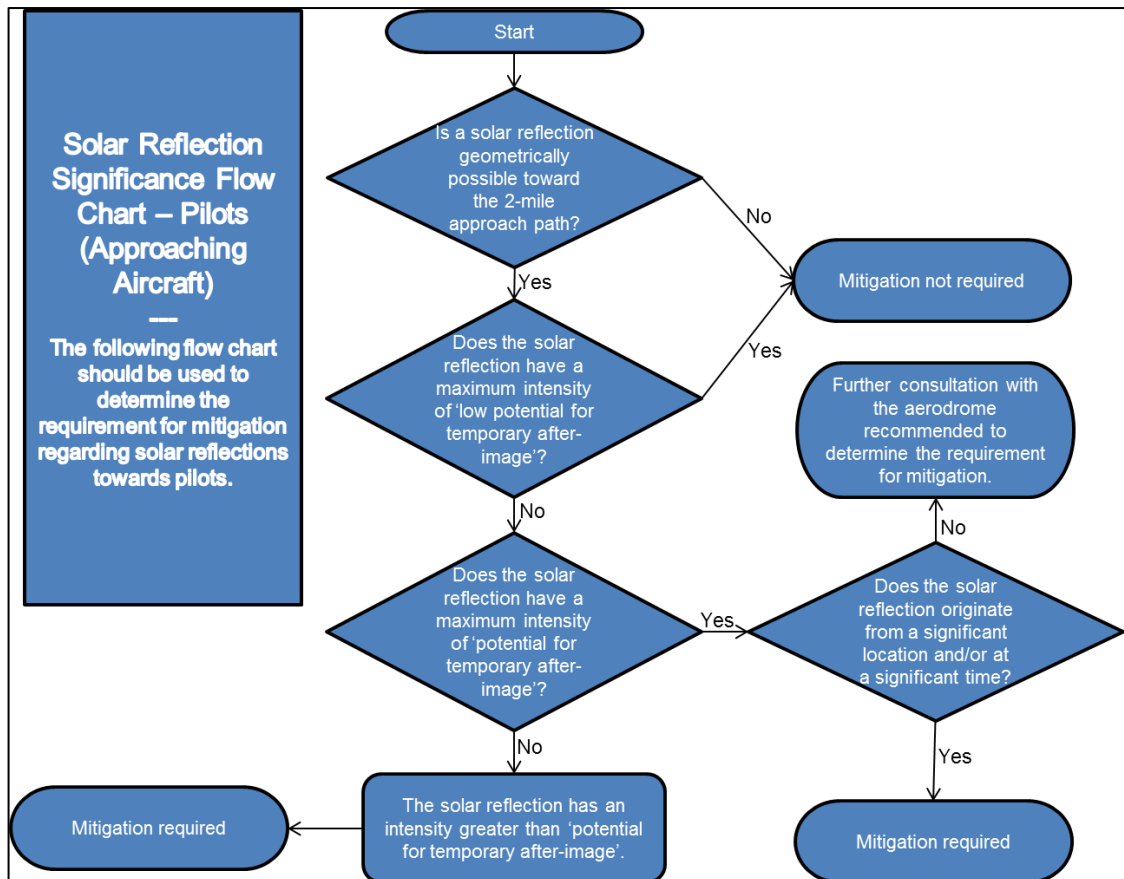
The flow chart presented below has been followed when determining the mitigation requirement for ATC Towers.



ATC Tower receptor mitigation requirement flow chart

Impact Significance Determination for Approaching Aircraft

The flow chart presented below has been followed when determining the mitigation requirement for approaching aircraft.



Approaching aircraft receptor mitigation requirement flow chart

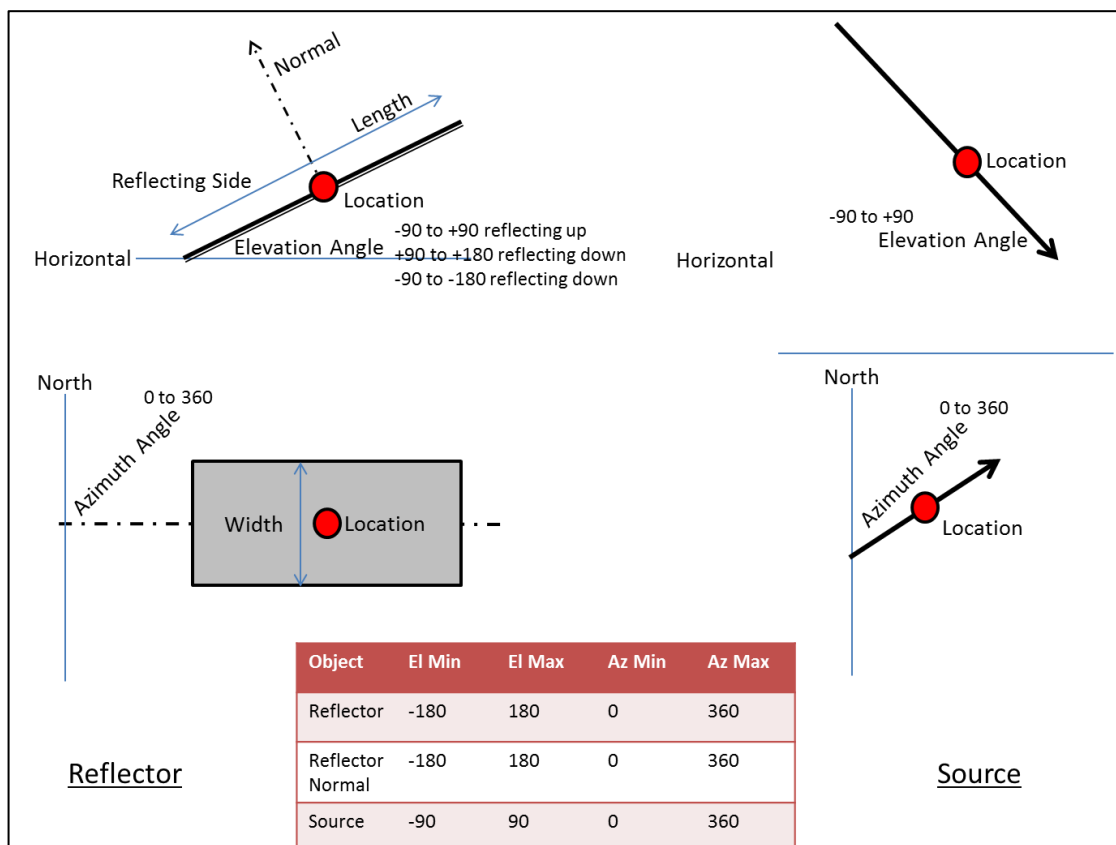
APPENDIX E – REFLECTION CALCULATIONS METHODOLOGY

Pager Power Methodology

The calculations are three dimensional and complex, accounting for:

- The Earth's orbit around the Sun;
- The Earth's rotation;
- The Earth's orientation;
- The reflector's location;
- The reflector's 3D Orientation.

Reflections from a flat reflector are calculated by considering the normal which is an imaginary line that is perpendicular to the reflective surface and originates from it. The diagram below may be used to aid understanding of the reflection calculation process.



Reflection calculation process

The following process is used to determine the 3D Azimuth and Elevation of a reflection:

- Use the Latitude and Longitude of reflector as the reference for calculation purposes;
- Calculate the Azimuth and Elevation of the normal to the reflector;
- Calculate the 3D angle between the source and the normal;
- If this angle is less than 90 degrees a reflection will occur. If it is greater than 90 degrees no reflection will occur because the source is behind the reflector;
- Calculate the Azimuth and Elevation of the reflection in accordance with the following:
 - The angle between source and normal is equal to angle between normal and reflection;
 - Source, Normal and Reflection are in the same plane.

APPENDIX F – ASSESSMENT LIMITATIONS AND ASSUMPTIONS

Pager Power's Model

The model considers 100% sunlight during daylight hours which is highly conservative.

The model does not account for terrain between the reflecting solar panels and the assessed receptor where a solar reflection is geometrically possible.

The model considers terrain between the reflecting solar panels and the visible horizon (where the sun may be obstructed from view of the panels)²⁷.

It is assumed that the panel elevation angle assessed represents the elevation angle for all of the panels within each solar panel area defined.

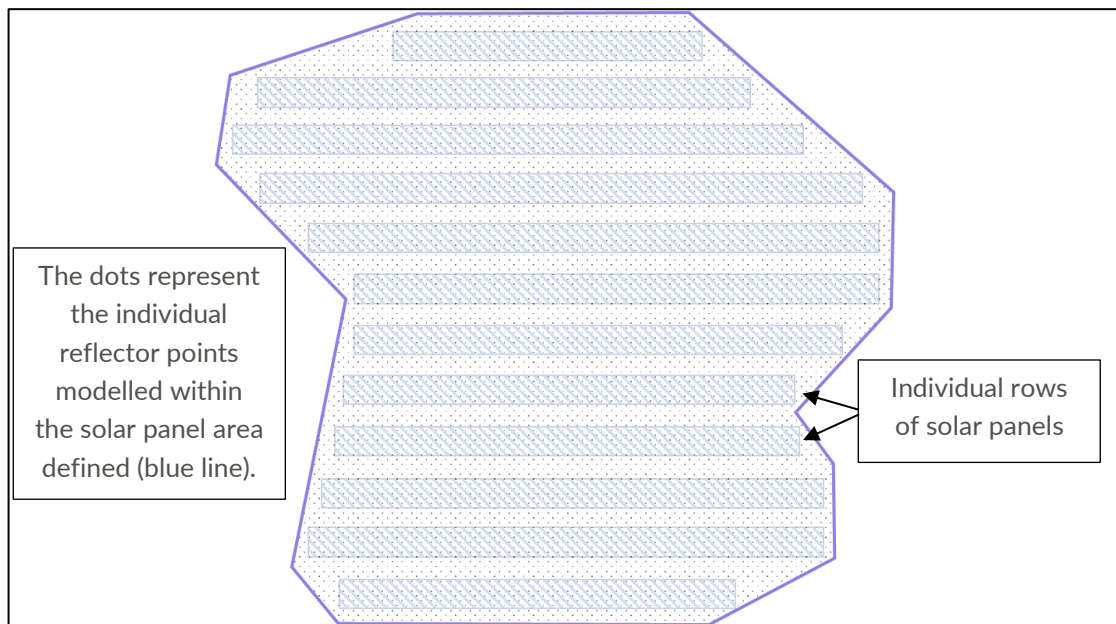
It is assumed that the panel azimuth angle assessed represents the azimuth angle for all of the panels within each solar panel area defined.

Only a reflection from the face of the panel has been considered. The frame or the reverse or frame of the solar panel has not been considered.

The model assumes that a receptor can view the face of every panel (point, defined in the following paragraph) within the development area whilst in reality this, in the majority of cases, will not occur. Therefore any predicted solar reflection from the face of a solar panel that is not visible to a receptor will not occur in practice.

A finite number of points within each solar panel area defined is chosen based on an assessment resolution so that a comprehensive understanding of the entire development can be formed. This determines whether a solar reflection could ever occur at a chosen receptor. The model does not consider the specific panel rows or the entire face of the solar panel within the development outline, rather a single point is defined every 'x' metres (based on the assessment resolution) with the geometric characteristics of the panel. A panel area is however defined to encapsulate all possible panel locations. See the figure below which illustrates this process.

²⁷ UK only.



Solar panel area modelling overview

A single reflection point is chosen for the geometric calculations. This suitably determines whether a solar reflection can be experienced at a receptor location and the time of year and duration of the solar reflection. Increased accuracy could be achieved by increasing the number of heights assessed however this would only marginally change the results and is not considered significant.

The available street view imagery, satellite mapping, terrain and any site imagery provided by the developer has been used to assess line of sight from the assessed receptors to the modelled solar panel area, unless stated otherwise. In some cases, this imagery may not be up to date and may not give the full perspective of the installation from the location of the assessed receptor.

Any screening in the form of trees, buildings etc. that may obstruct the Sun from view of the solar panels is not within the modelling unless stated otherwise. The terrain profile at the horizon is considered if stated.

Forge's Sandia National Laboratories' (SGHAT) Model

The following text is taken from Forge²⁸ and is presented for reference.

Summary of assumptions and abstractions required by the SGHAT/ForgeSolar analysis methodology

1. Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
2. Result data files and plots are now retained for two years after analysis completion. Files should be downloaded and saved if additional persistence is required.
3. The algorithm does not rigorously represent the detailed geometry of a system; detailed features such as gaps between modules, variable height of the PV array, and support structures may impact actual glare results. However, we have validated our models against several systems, including a PV array causing glare to the air-traffic control tower at Manchester-Boston Regional Airport and several sites in Albuquerque, and the tool accurately predicted the occurrence and intensity of glare at different times and days of the year.
4. Several calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for large PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare. This primarily affects analyses of path receptors.
5. Random number computations are utilized by various steps of the annual hazard analysis algorithm. Predicted minutes of glare can vary between runs as a result. This limitation primarily affects analyses of Observation Point receptors, including ATCTs. Note that the SGHAT/ForgeSolar methodology has always relied on an analytical, qualitative approach to accurately determine the overall hazard (i.e. green vs. yellow) of expected glare on an annual basis.
6. The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
7. The algorithm assumes that the PV array is aligned with a plane defined by the total heights of the coordinates outlined in the Google map. For more accuracy, the user should perform runs using minimum and maximum values for the vertex heights to bound the height of the plane containing the solar array. Doing so will expand the range of observed solar glare when compared to results using a single height value.
8. The algorithm does not consider obstacles (either man-made or natural) between the observation points and the prescribed solar installation that may obstruct observed glare, such as trees, hills, buildings, etc.
9. The variable direct normal irradiance (DNI) feature (if selected) scales the user-prescribed peak DNI using a typical clear-day irradiance profile. This profile has a lower DNI in the mornings and evenings and a maximum at solar noon. The scaling uses a clear-day irradiance profile based on a normalized time relative to sunrise, solar noon, and sunset, which are prescribed by a sun-position algorithm and the latitude and longitude obtained from Google maps. The actual DNI on any given day can be affected by cloud cover, atmospheric attenuation, and other environmental factors.
10. The ocular hazard predicted by the tool depends on a number of environmental, optical, and human factors, which can be uncertain. We provide input fields and typical ranges of values for these factors so that the user can vary these parameters to see if they have an impact on the results. The speed of SGHAT allows expedited sensitivity and parametric analyses.
11. The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
12. Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.
13. Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
14. Glare vector plots are simplified representations of analysis data. Actual glare emanations and results may differ.
15. PV array tracking assumes the modules move instantly when tracking the sun, and when reverting to the rest position.

²⁸ Source: <https://www.forgesolar.com/help/#assumptions>

APPENDIX G – RECEPTOR AND REFLECTOR AREA DETAILS

ATC Receptor Details

The co-ordinates and overall altitude of the ATC Tower has been extrapolated from available maps and imagery. The ground height has been taken from Pager Power's database²⁹ based on the co-ordinates of the ATC Tower. The details are presented in the table below.

Longitude (°)	Latitude (°)	Ground Height Altitude (m) (amsl)	ATC Tower Observer Height ³⁰ (m)	Overall Assessed Height (m)
2.27961	53.35782	69.90	55	124.90

ATC Tower receptor details

Runway Details

The table below presents the runway details for Manchester Airport.

Runway	Longitude (°)	Latitude (°)	Threshold Altitude (ft) (amsl)
05L/23R	-2.28776	53.34756	211.8
	-2.25928	53.36132	249.1
05R/23L	-2.31066	53.33198	186.3
	-2.27721	53.34815	227.0

Runway details for Manchester Airport

Modelled Reflector Areas

The modelled reflector areas are presented in the tables below.

No.	Longitude (°)	Latitude (°)	No.	Longitude (°)	Latitude (°)
1	-2.25391	53.37115	4	-2.25396	53.37121
2	-2.25390	53.37116	5	-2.25405	53.37119
3	-2.25395	53.37121	6	-2.25405	53.37117

²⁹ Based on OS Panorama 50m DTM

³⁰ Estimated based on the available imagery.

Panel Area 1.1

No.	Longitude (°)	Latitude (°)	No.	Longitude (°)	Latitude (°)
1	-2.25330	53.37105	4	-2.25320	53.37109
2	-2.25315	53.37103	5	-2.25321	53.37109
3	-2.25315	53.37104	6	-2.25329	53.37106

Panel Area 1.2

No.	Longitude (°)	Latitude (°)	No.	Longitude (°)	Latitude (°)
1	-2.25317	53.37110	4	-2.25298	53.37134
2	-2.25313	53.37105	5	-2.25300	53.37135
3	-2.25310	53.37105	6	-2.25307	53.37133

Panel Area 1.3

No.	Longitude (°)	Latitude (°)	No.	Longitude (°)	Latitude (°)
1	-2.25335	53.37131	4	-2.25315	53.37133
2	-2.25322	53.37129	5	-2.25333	53.37136
3	-2.25316	53.37132			

Panel Area 1.4

No.	Longitude (°)	Latitude (°)	No.	Longitude (°)	Latitude (°)
1	-2.25357	53.37133	4	-2.25347	53.37137
2	-2.25344	53.37131	5	-2.25350	53.37138
3	-2.25344	53.37133	6	-2.25357	53.37135

Panel Area 1.5

No.	Longitude (°)	Latitude (°)	No.	Longitude (°)	Latitude (°)
1	-2.25380	53.37143	4	-2.25362	53.37141
2	-2.25377	53.37138	5	-2.25380	53.37144
3	-2.25364	53.37136			

Panel Area 1.6

No.	Longitude (°)	Latitude (°)	No.	Longitude (°)	Latitude (°)
1	-2.25378	53.37136	6	-2.25383	53.37130
2	-2.25383	53.37140	7	-2.25389	53.37131
3	-2.25385	53.37140	8	-2.25393	53.37122
4	-2.25388	53.37134	9	-2.25388	53.37118
5	-2.25382	53.37133	10	-2.25386	53.37118

Panel Area 1.7

No.	Longitude (°)	Latitude (°)	No.	Longitude (°)	Latitude (°)
1	-2.25338	53.37215	6	-2.25324	53.37195
2	-2.25321	53.37187	7	-2.25329	53.37203
3	-2.25319	53.37187	8	-2.25320	53.37205
4	-2.25314	53.37194	9	-2.25325	53.37214
5	-2.25315	53.37197	10	-2.25336	53.37216

Panel Area 2.1

No.	Longitude (°)	Latitude (°)	No.	Longitude (°)	Latitude (°)
1	-2.25314	53.37185	6	-2.25290	53.37191
2	-2.25267	53.37195	7	-2.25302	53.37189
3	-2.25267	53.37196	8	-2.25305	53.37194
4	-2.25277	53.37200	9	-2.25312	53.37192
5	-2.25293	53.37196	10	-2.25315	53.37186

Panel Area 2.2

No.	Longitude (°)	Latitude (°)	No.	Longitude (°)	Latitude (°)
1	-2.25394	53.37179	3	-2.25366	53.37194
2	-2.25362	53.37184	4	-2.25398	53.37188

Panel Area 3.1

APPENDIX H – DETAILED MODELLING RESULTS

Overview

The Pager Power charts for receptors are shown on the following pages. Further modelling charts can be provided upon request. Each chart shows:

- The receptor (observer) location – top right image. This also shows the azimuth range of the Sun itself at times when reflections are possible. If sunlight is experienced from the same direction as the reflecting panels, the overall impact of the reflection is reduced as discussed within the body of the report;
- The reflecting panels – bottom right image. The reflecting area is shown in yellow. If the yellow panels are not visible from the observer location, no issues will occur in practice. Additional obstructions which may obscure the panels from view are considered separately within the analysis;
- The reflection date/time graph – left hand side of image. The blue line indicates the dates and times at which geometric reflections are possible. This relates to reflections from the yellow areas;
- The sunrise and sunset curves throughout the year (red and yellow lines).

The Forge charts for the receptors are shown on the following pages. Each chart shows:

- The annual predicted solar reflections.
- The daily duration of the solar reflections.
- The location of the proposed development where glare will originate.
- The calculated intensity of the predicted solar reflections.

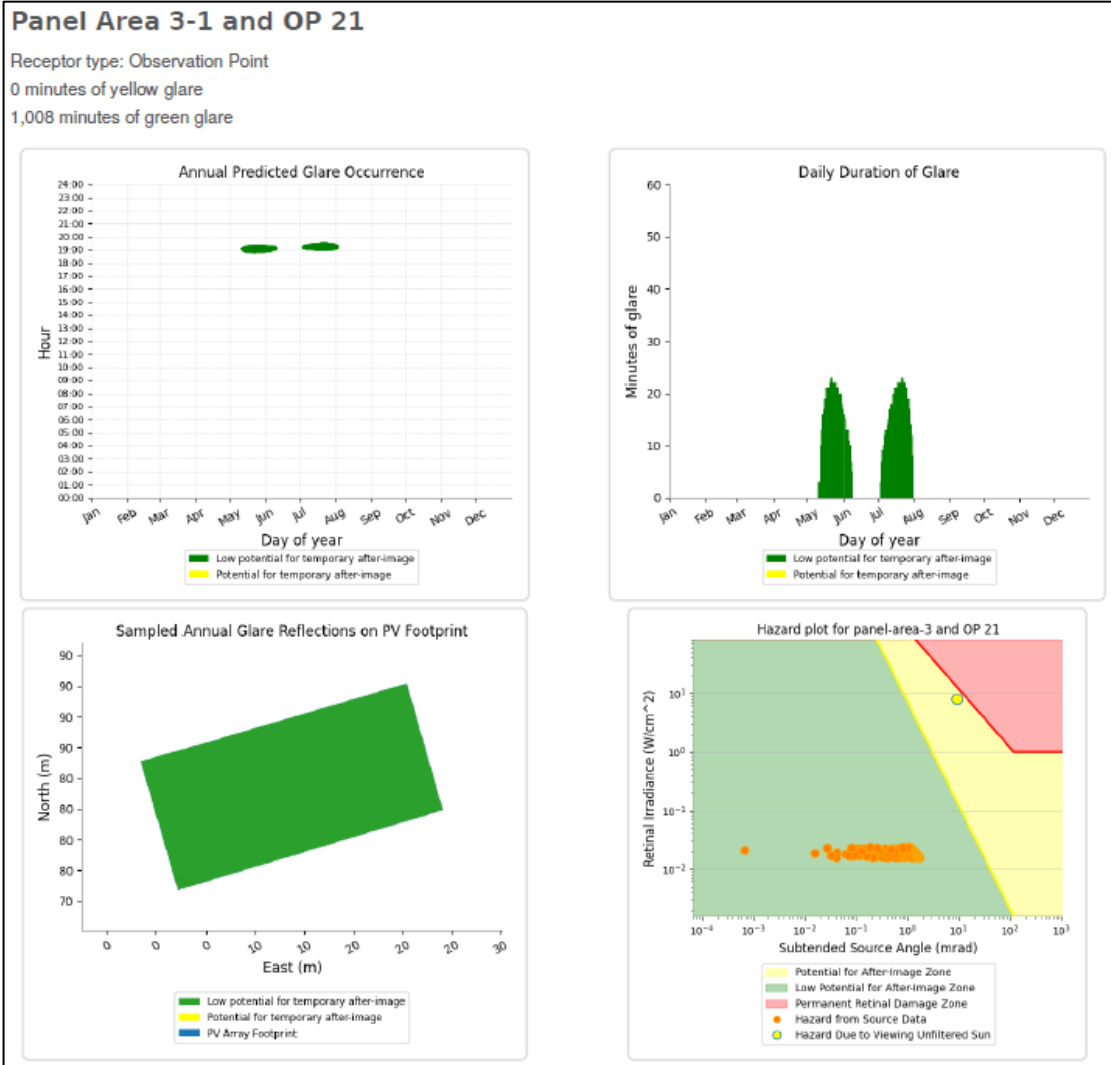
For approach paths, two further charts are shown within the Forge modelling results:

- Locations along the approach path receiving glare.
- The dates when glare would occur at each location along the approach.

Full modelling results can be provided upon request.

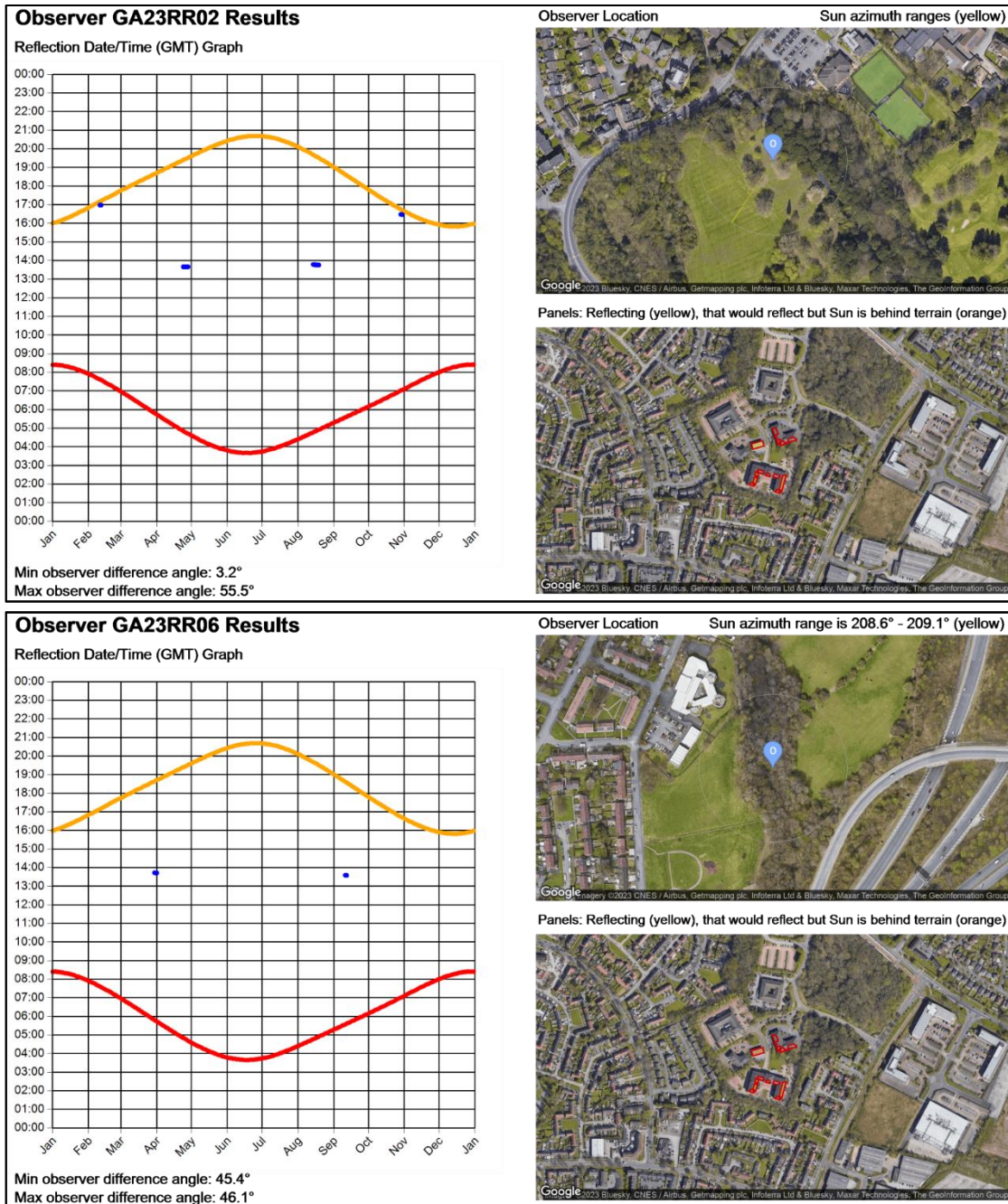
Approach Paths

Forge



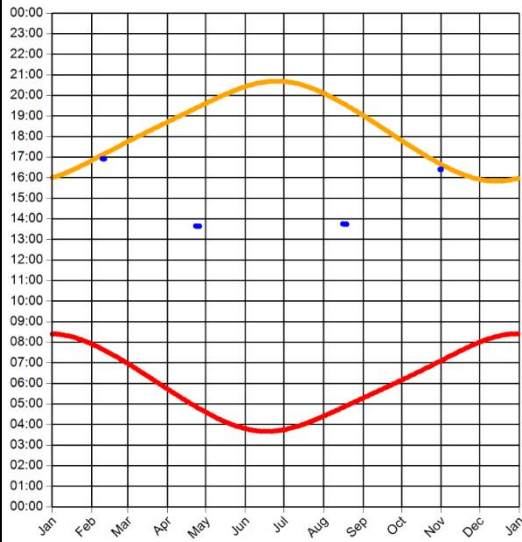
Pager Power

Selected results have been included to show a range of representative results, for completeness.



Observer GA23LR04 Results

Reflection Date/Time (GMT) Graph



Observer Location

Sun azimuth ranges (yellow)

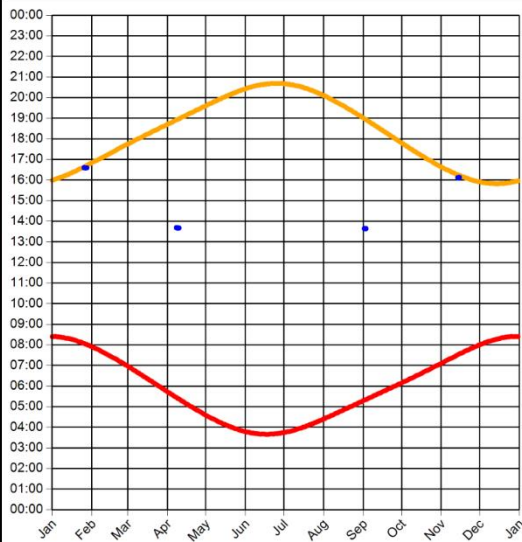


Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



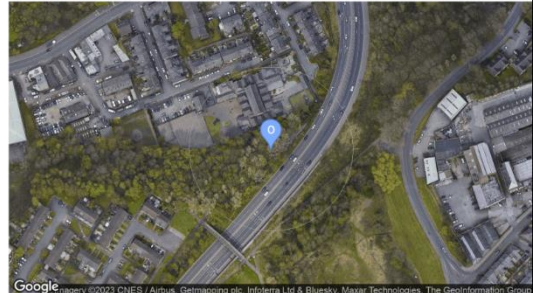
Observer GA23LR06 Results

Reflection Date/Time (GMT) Graph



Observer Location

Sun azimuth ranges (yellow)



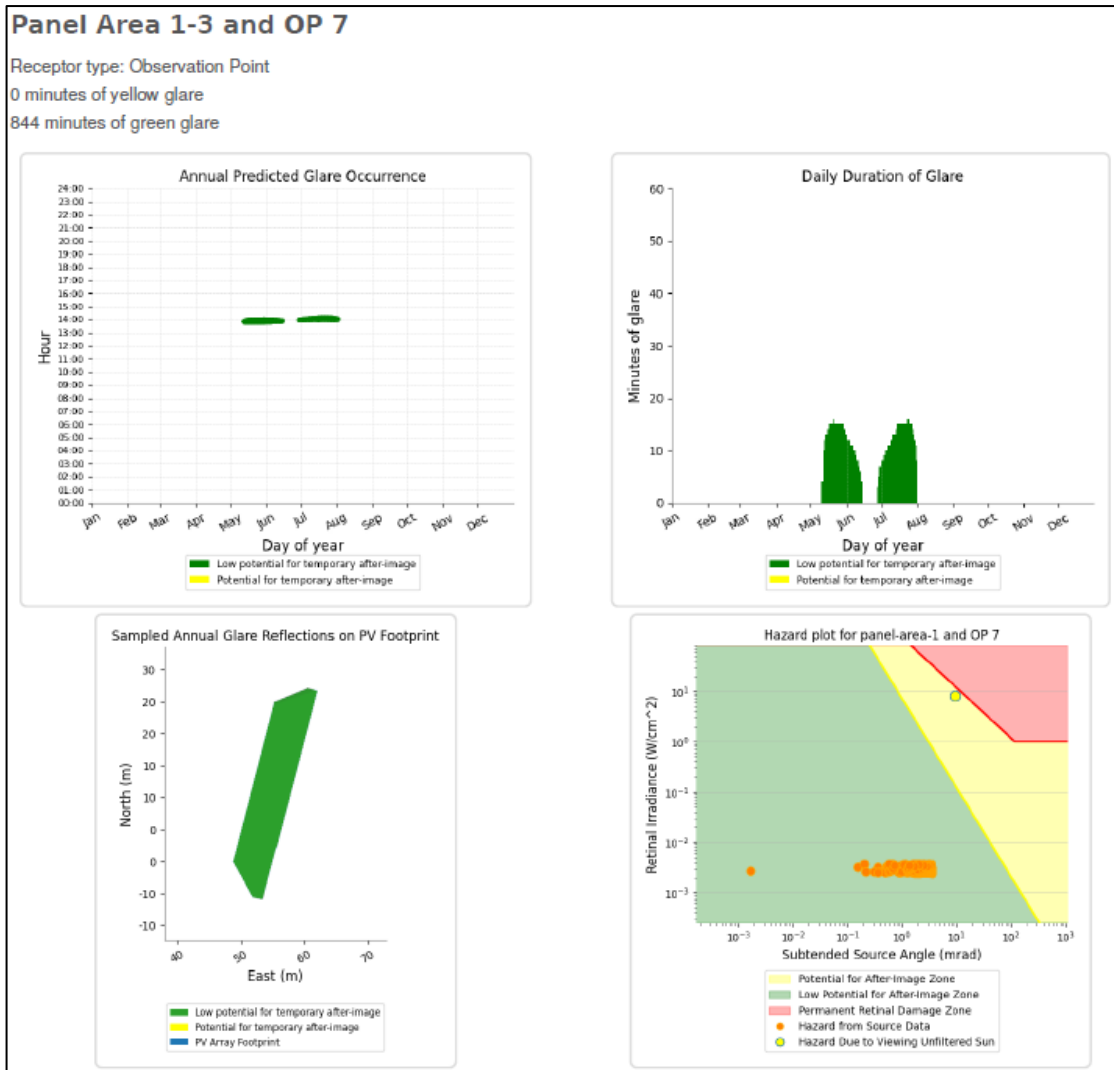
Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



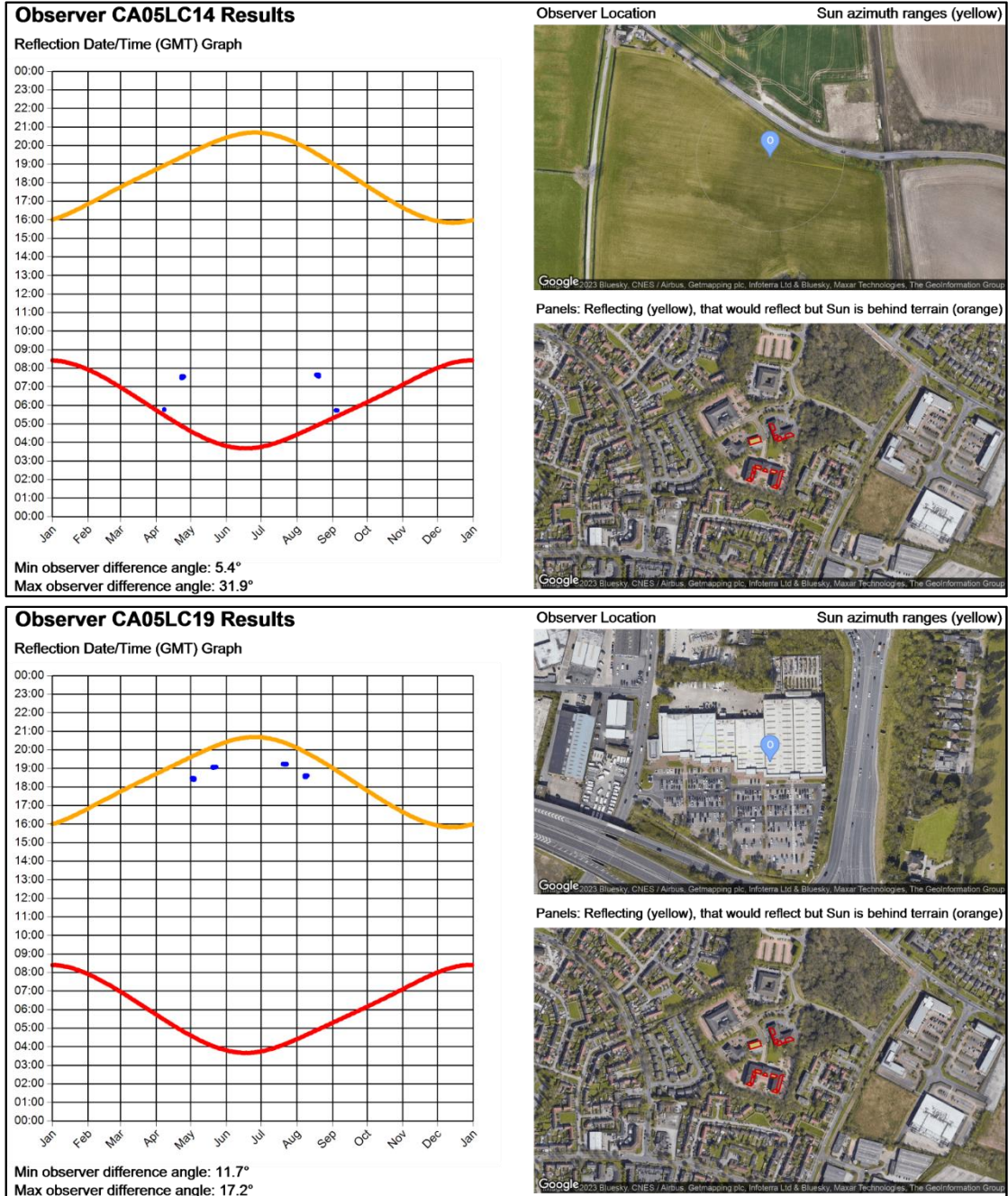
Visual Circuits

Selected results have been included to show a range of representative results, for completeness.

Forge

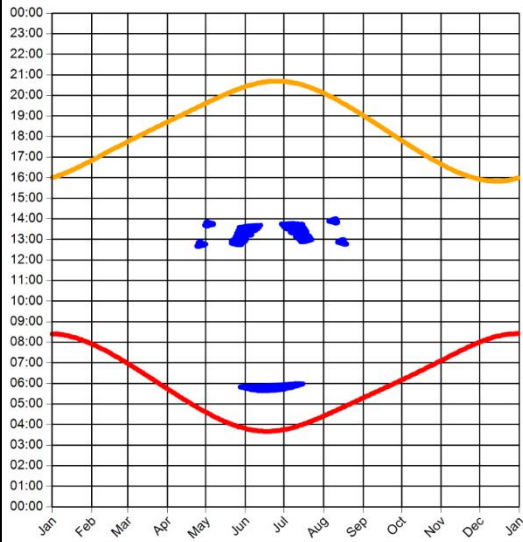


Pager Power



Observer CA05RC26 Results

Reflection Date/Time (GMT) Graph



Observer Location

Sun azimuth ranges (yellow)

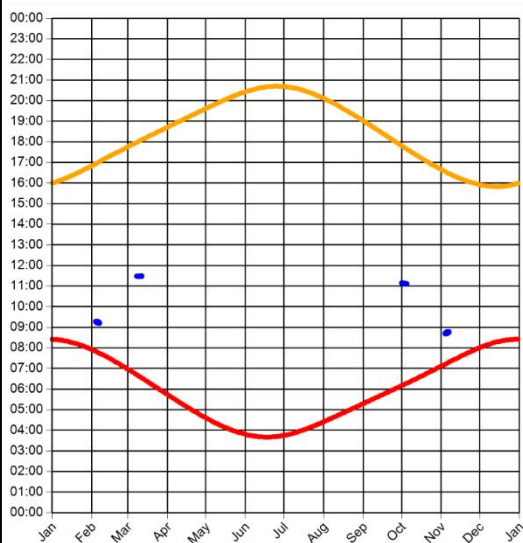


Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



Observer CA05RC25 Results

Reflection Date/Time (GMT) Graph



Observer Location

Sun azimuth ranges (yellow)



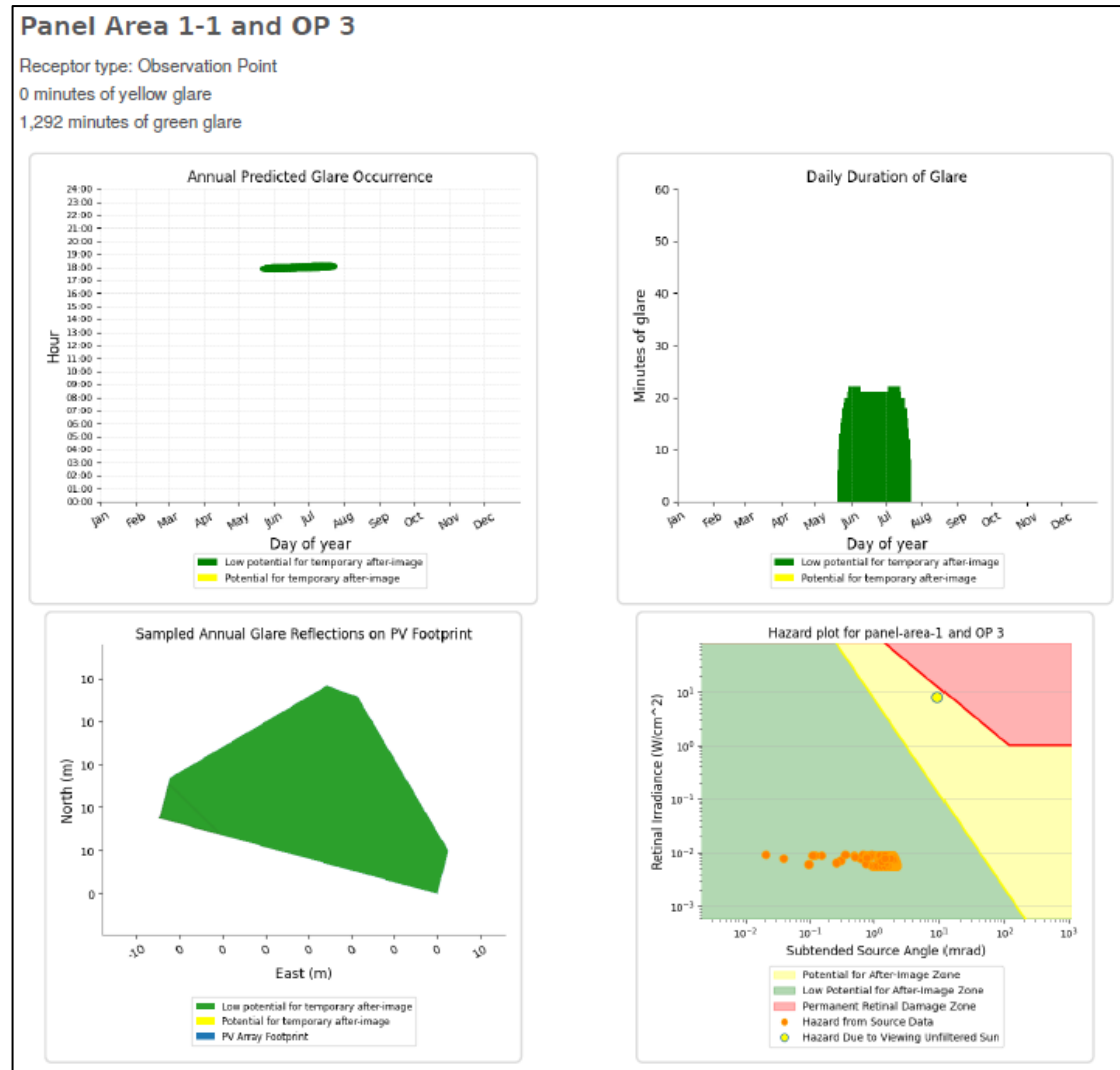
Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



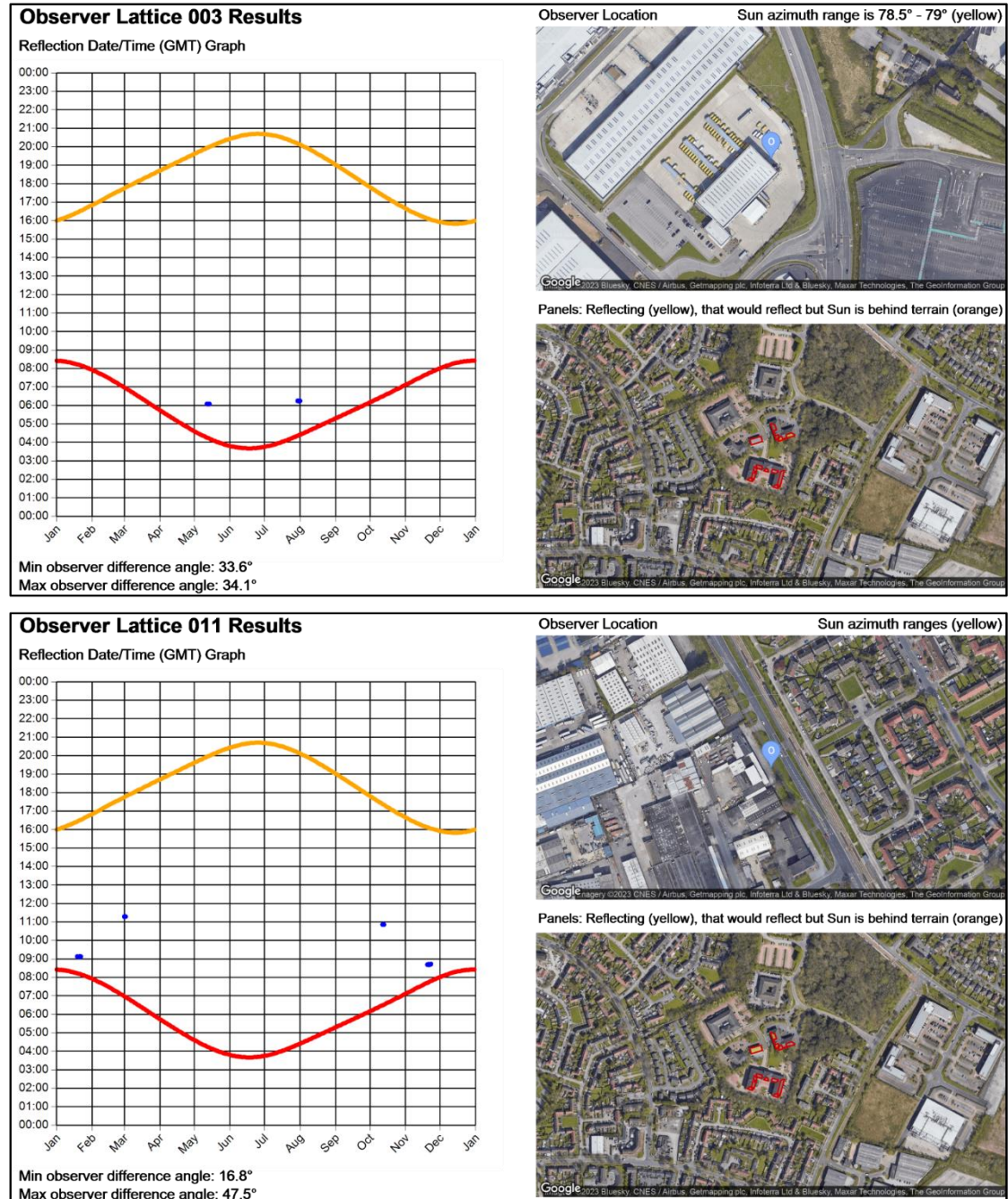
Lattice

Selected results have been included to show a range of representative results.

Forge

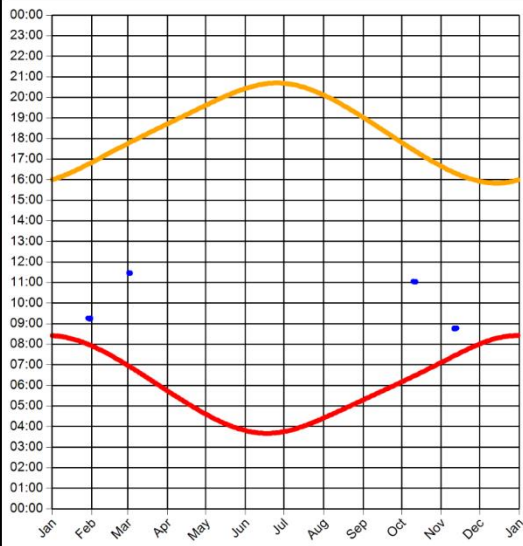


Pager Power



Observer Lattice 021 Results

Reflection Date/Time (GMT) Graph



Observer Location

Sun azimuth ranges (yellow)

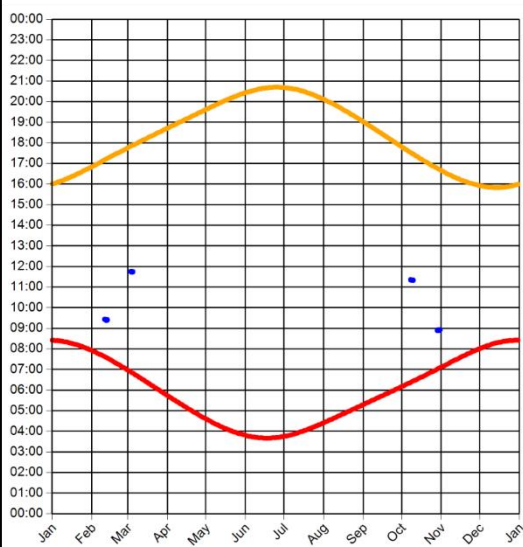


Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



Observer Lattice 031 Results

Reflection Date/Time (GMT) Graph

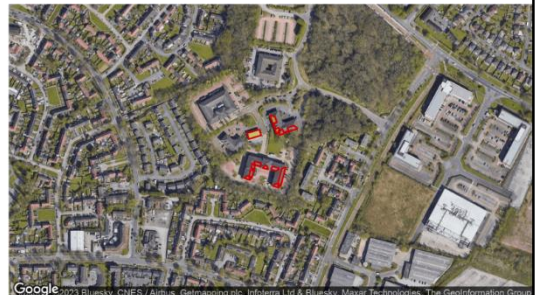


Observer Location

Sun azimuth ranges (yellow)

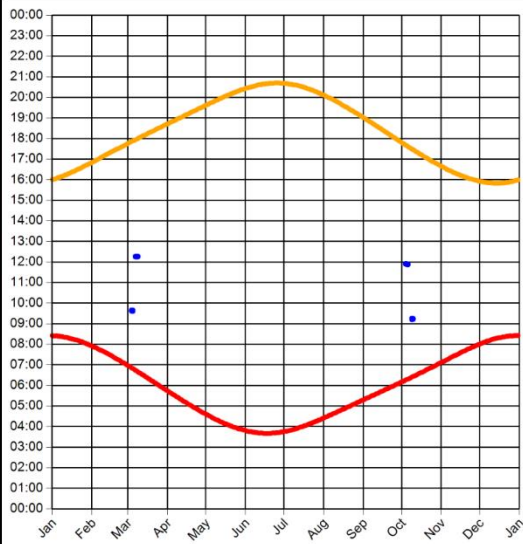


Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



Observer Lattice 041 Results

Reflection Date/Time (GMT) Graph



Observer Location

Sun azimuth ranges (yellow)

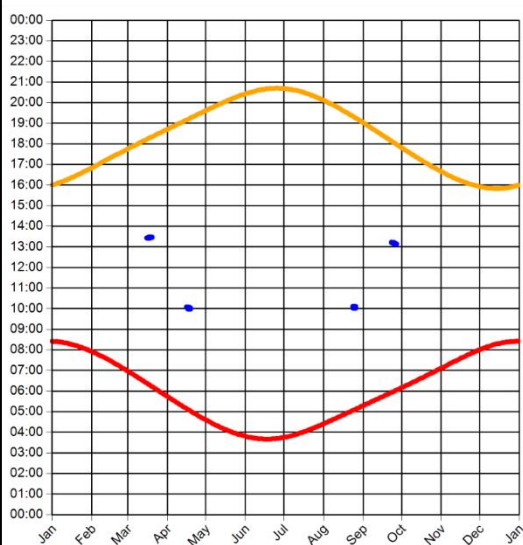


Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



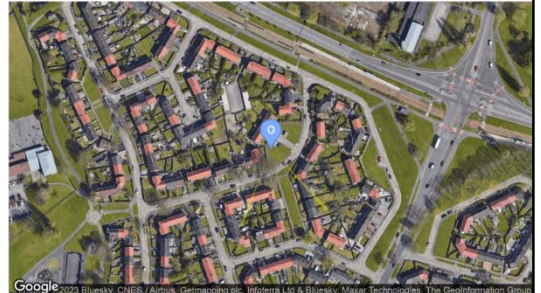
Observer Lattice 051 Results

Reflection Date/Time (GMT) Graph

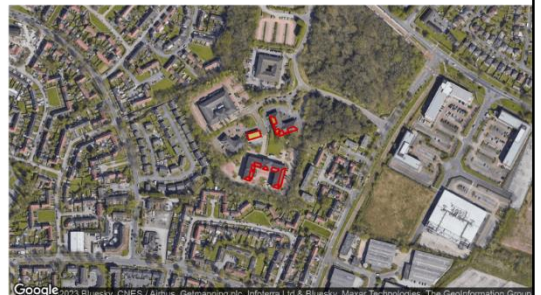


Observer Location

Sun azimuth ranges (yellow)

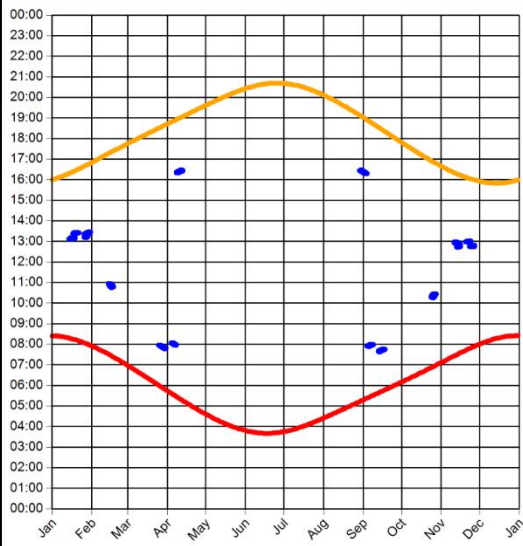


Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



Observer Lattice 061 Results

Reflection Date/Time (GMT) Graph



Min observer difference angle: 90°
Max observer difference angle: 96.4°

Observer Location

Sun azimuth ranges (yellow)

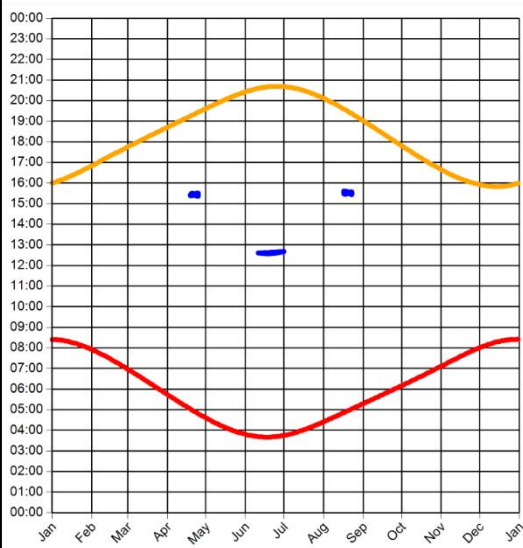


Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



Observer Lattice 071 Results

Reflection Date/Time (GMT) Graph



Min observer difference angle: 97.1°
Max observer difference angle: 125.6°

Observer Location

Sun azimuth ranges (yellow)

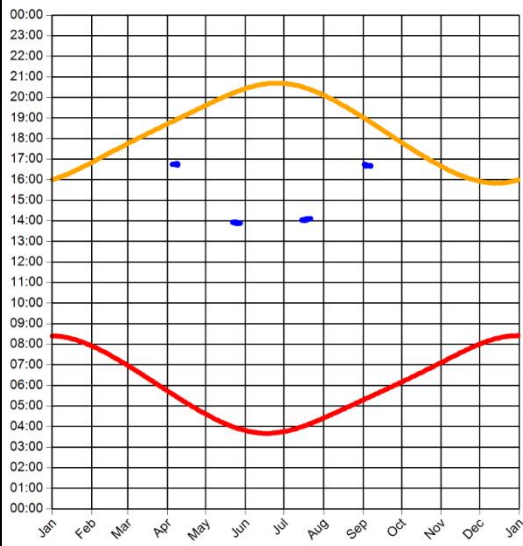


Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



Observer Lattice 082 Results

Reflection Date/Time (GMT) Graph



Observer Location

Sun azimuth ranges (yellow)

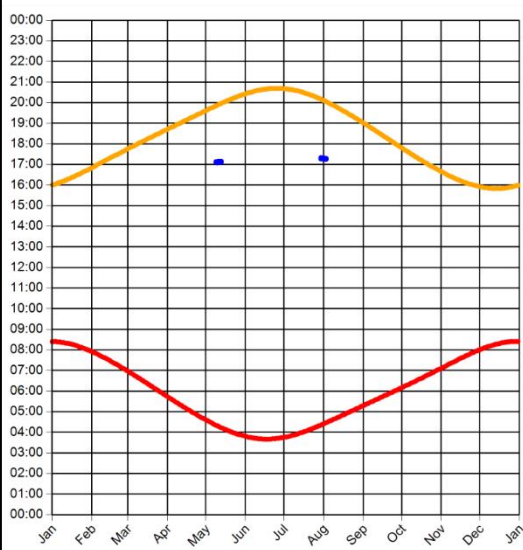


Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



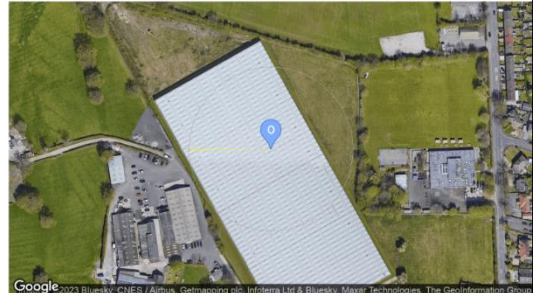
Observer Lattice 092 Results

Reflection Date/Time (GMT) Graph



Observer Location

Sun azimuth range is 268.9° - 270.3° (yellow)

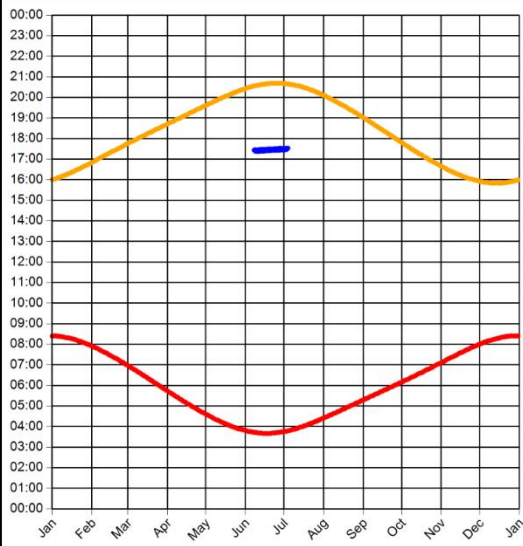


Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



Observer Lattice 102 Results

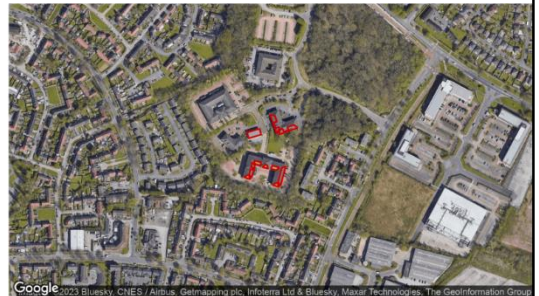
Reflection Date/Time (GMT) Graph



Observer Location Sun azimuth range is 275.6° - 276.7° (yellow)

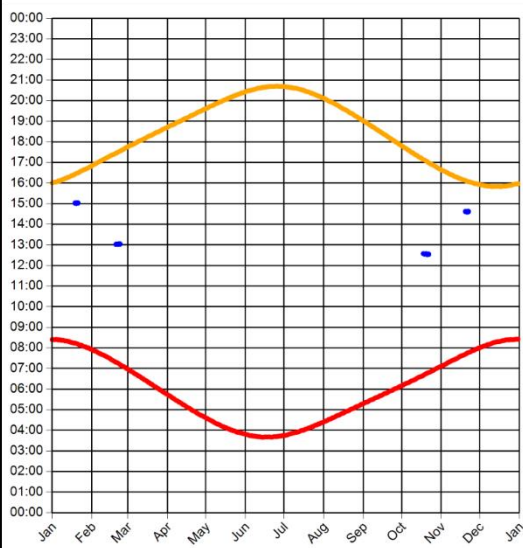


Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)



Observer Lattice 110 Results

Reflection Date/Time (GMT) Graph

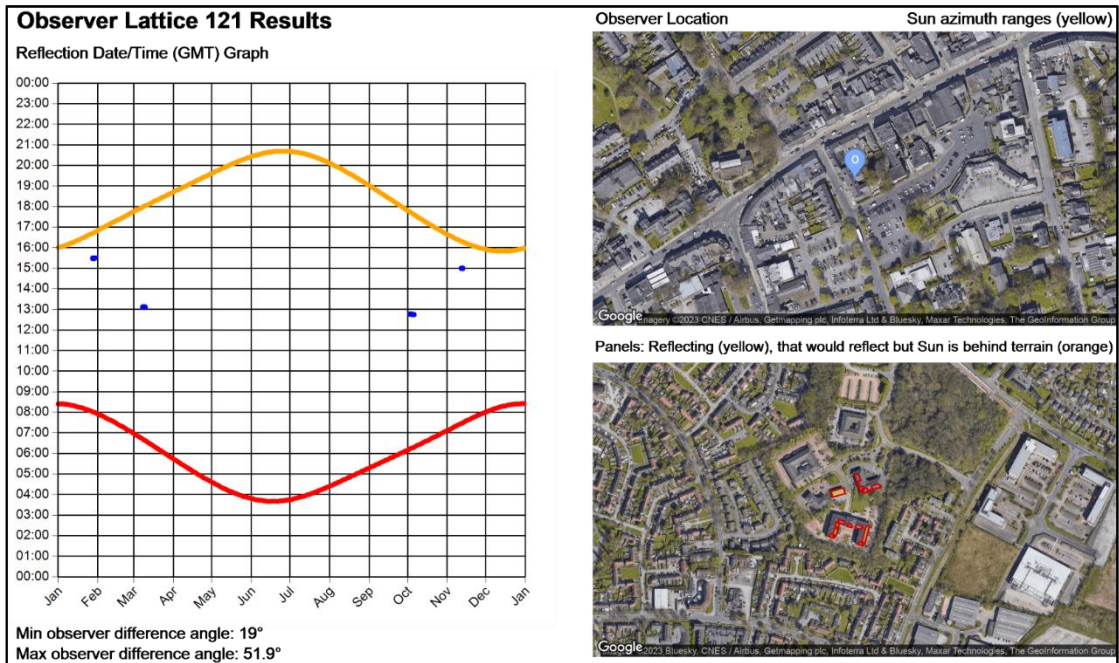


Observer Location Sun azimuth ranges (yellow)



Panels: Reflecting (yellow), that would reflect but Sun is behind terrain (orange)







Pager Power Limited
Stour Valley Business Centre
Sudbury
Suffolk
CO10 7GB

Tel: +44 1787 319001 **Email:** info@pagerpower.com **Web:** www.pagerpower.com