



Discharge of Condition

Site Address: 5-7 Byrom Street, Manchester, M3 4PF

Client Name: T A Knox Limited

Project Reference No: NP-011858



Authorisation and Version Control

Revision	Reported By	Checked By
01	R. Chamberlain BSc, MIOA	T. Watkin, MSc, MIOA

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Contact Details

NOVA Acoustics Ltd,
Suite 13, Crown House,
94 Armley Road,
Leeds,
LS12 2EJ

0113 322 7977

www.novaacoustics.co.uk
technical@novaacoustics.co.uk

Delivering sustainable development by promoting good health and well-being through effective management of noise.

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1. Introduction

NOVA Acoustics Ltd has been commissioned to provide evidence that Condition 5 placed on the proposed development by Manchester City Council can be discharged. These conditions relate to planning application No. 139981/FO/2024 ('the application') which contained proposals for general refurbishment works ('the proposed development') at 5-7 Byrom Street, Manchester, M3 4PF ('the site').

A noise survey has been undertaken to establish the prevailing background sound levels at the closest Noise Sensitive Receptors ('NSRs'). The report details the existing background sound climate and provides a plant noise limit level for the noise emissions associated with the proposed development.

This noise assessment is necessarily technical in nature; therefore, a glossary of terms is included in Appendix A to assist the reader.

1.1 Standards, Legislation, Policy & Guidance

The following performance standards, legislation, policy and guidance have been considered to ensure good acoustic design in the assessment:

- The LPA conditional approval; specifically, 'Condition 5'.
- The LPA technical guidance, specifically; Manchester City Council's guidance document 'Planning and Noise Technical Guidance' (2022).
- National Planning Policy Framework (2023).
- Noise Policy Statement for England (2010).
- British Standard BS4142:2014+A1:2019 – 'Methods for rating and assessing industrial and commercial sound'.
- British Standard BS8233:2014 – 'Guidance on sound insulation and noise reduction for buildings'.

Further information on the legislation can be found in Appendix B.

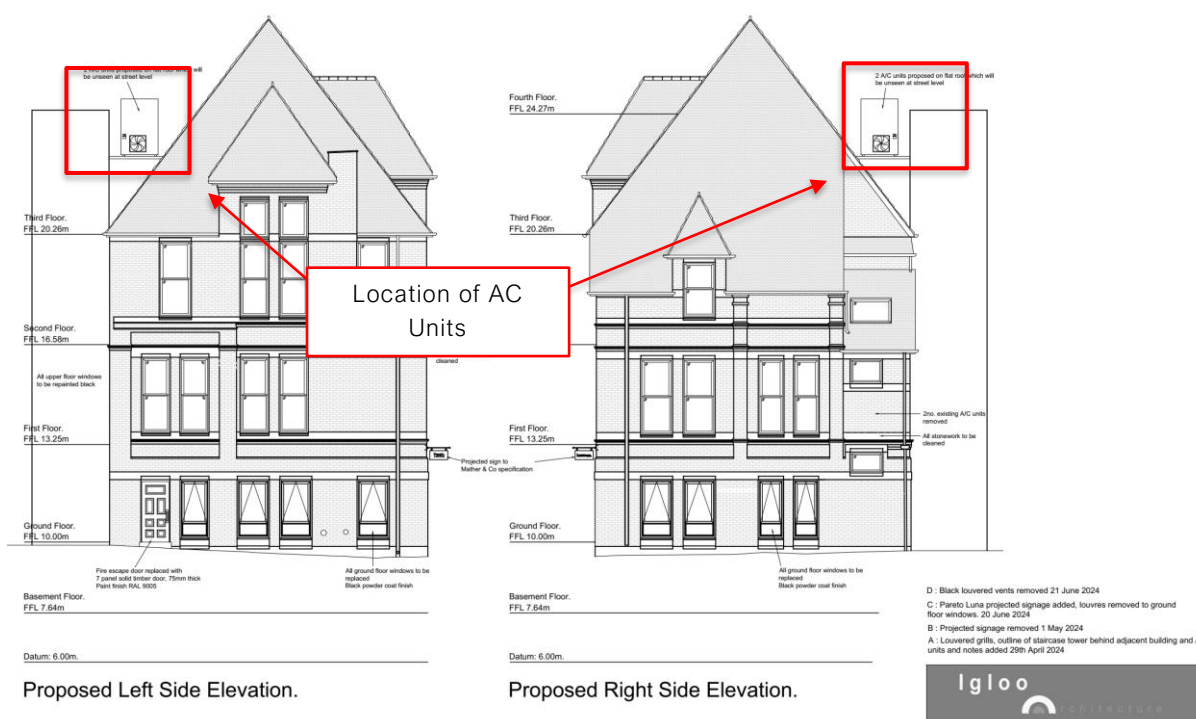
1.2 Proposal Brief

The general proposals for the site included for external alterations comprising of the installation of new double doors, replacement windows with louvres and the relocation of air conditioning ('AC') units.

The following items of plant were installed at the development:

- 2no. Mitsubishi PURY-P900YSNW-A (-BS)

The plant operates from 09:00 to 17:00, Monday to Friday. The figure below shows the development and the location of the plant items. Manufacturer datasheets are provided in Appendix E for reference.



Drawing Ref No. P1276/18 from 'Igloo'

Figure 1 – Proposed Development

1.3 Local Planning Authority & Background

The following planning condition imposed on the application by the LPA requires discharging:

"5) a) Externally mounted ancillary plant, equipment and servicing shall be selected and/or acoustically treated in accordance with a scheme designed so as to achieve a rating level of 5dB (L_{Aeq}) below the typical background (LA_{90}) level at the nearest noise sensitive location. a) Prior to commencement of the use hereby approved the scheme shall be submitted to and approved in writing by the City Council as local planning authority in order to secure a reduction in the level of noise emanating from the site. The scheme shall be implemented in full before the use commences or as otherwise agreed in writing by the City Council as local planning authority.

b) Prior to the operation of the scheme a verification report shall be submitted to and approved in writing by the City Council as local planning authority to validate that the work undertaken throughout the development conforms to the recommendations and requirements in the approved acoustic report. The

report shall also undertake post completion testing to confirm that the noise criteria have been met. Any instances of non-conformity with the recommendations in the report shall be detailed along with any measures required to ensure compliance with the agreed noise criteria.

Reason - To minimise the impact of the development and to prevent a general increase in pre-existing background noise levels around the site pursuant to policies DM1 and SP1 of the Manchester Core Strategy (2012)."

2. Environmental Noise Survey

2.1 Measurement Methodology

Unattended and attended noise monitoring was undertaken at the site to measure the background sound levels at the NSR's and measure the noise levels from the proposed items of plant.

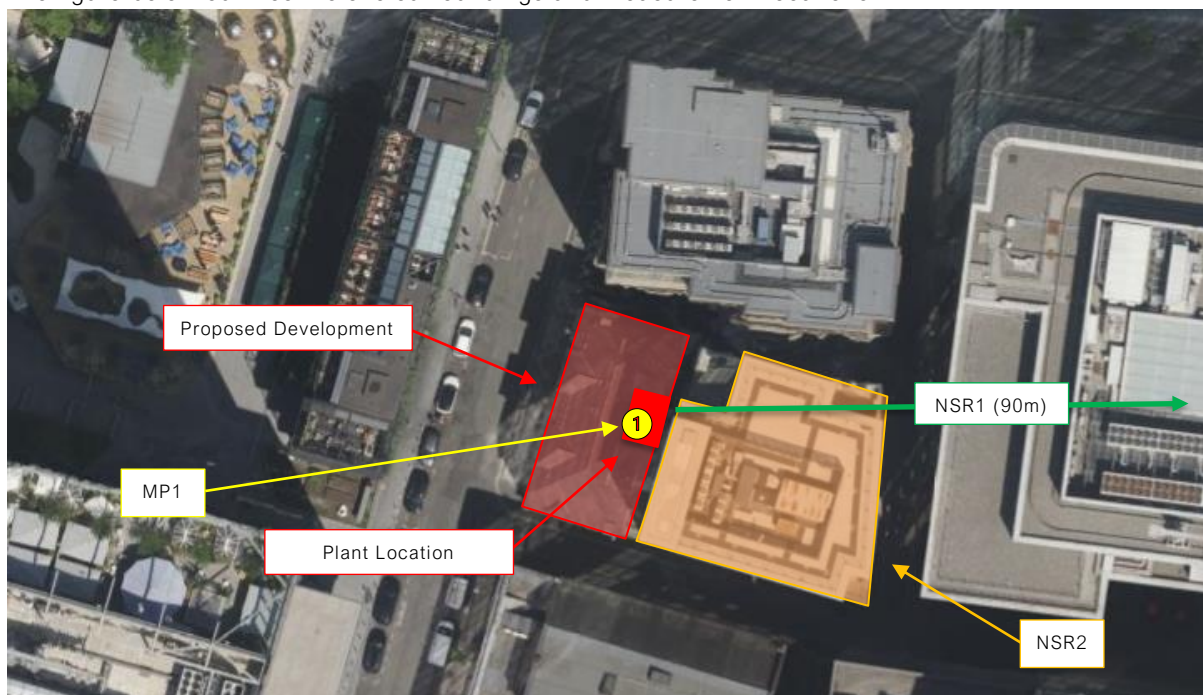
The unattended monitoring was undertaken at measurement position (MP) 1 in a location that was deemed representative of the noise climate at all NSR's. The plant items were switched off during this. Spot measurements were also carried out in proximity to the plant items with them switched on and off.

The following table outlines the measurement dates and particulars. Weather conditions during the environmental sound survey can be found in Appendix D.

Location	Survey Dates	Measurement Particulars
MP1	30-31/10/2024	Equipment mounted on a tripod at 3m above rooftop level in a free-field monitoring location. A 130mm diameter windshield was fitted to the microphone. The equipment was field calibrated before and after the survey; negligible drift was noted.

Table 1 – Measurement Methodology

The figure below outlines the site surroundings and measurement locations:



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Figure 2 – Measurement Locations and Site Surroundings

2.2 Context & Subjective Impression

The plant is installed on the rooftop rear side (eastern) of the building.

The noise profile in the area is considered high and is dominated by road traffic noise from the surrounding road networks.

The nearest *residential* receptor to the site is at the Moxy Manchester City hotel (NSR1) situated approximately 90m away to the east. The nearest non-residential receptors to the plant are the office buildings immediately to the east (NSR2), approximately 5m away.

2.3 Environmental Noise Survey Results

Background Sound Level Analysis

The following section outlines the measured background sound levels that have been used as the baseline for the subsequent BS4142 noise assessment.

The figure below shows a histogram graph of the background sound levels measured during the proposed operational period of 09:00 – 17:00 hours throughout the entire measurement period. The time history results can be found in Appendix D. The below noise levels were recorded with the plant items switched off throughout the measurement duration.

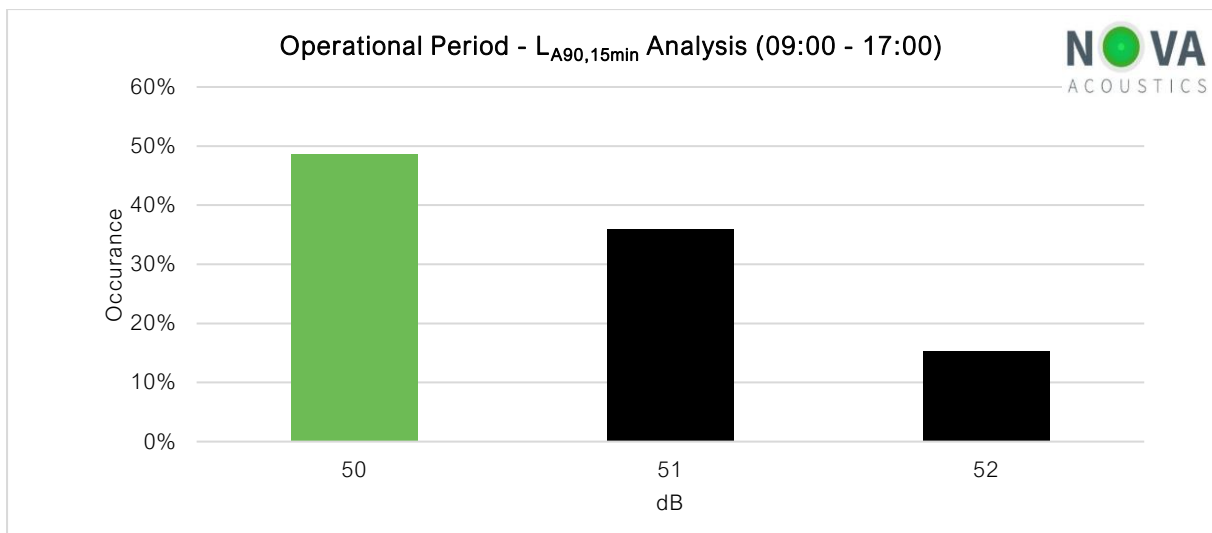


Figure 3 – MP1 Daytime Operational Hours Background Sound Level Analysis

As can be seen in Figure 3, the modal $LA_{90,15min}$ measurement of 50 dB has been used as the baseline for the daytime BS4142 assessments.

2.4 Receptor Measurement Results Summary

Measurements were carried out at 1m from the proposed items of plant on 31 November 2024. Ambient measurements were conducted with the plant equipment operating at the maximum permitted capacity. Further residual measurements were conducted at the same location with the plant equipment switched off.

Logarithmically subtracting the measured residual sound levels from the measured ambient sound levels have allowed specific sound levels to be calculated. Presented in the table overleaf are the measured ambient and residual sound levels and the subsequent specific sound levels.

Location	Description	Octave Band (Hz, L _{eq} dB)								Overall (dBA)
		63	125	250	500	1k	2k	4k	8k	
MP1	Both plant Operating (1m)	82	73	74	71	68	64	60	54	73
	Residual Sound Level (1m)	62	57	53	49	49	45	39	29	53
	Specific Sound Level (1m)	82	73	74	71	68	64	60	54	73

Table 2 – Calculated Specific Sound Levels at Source

Based on the datasheets presented in Appendix E, the sound pressure level from one item operating is 73 dB(A), however, no measurement distance is provided. Therefore, there is some uncertainty within the manufacturer data. In any case, a global figure of 76dB(A) has been used as the specific sound level to form a robust assessment.

3. External Plant Noise Impact Assessment

There are two types of NSR to the rooftop items of plant: the residential building 90m away to the east (NSR1), and the nearby office buildings 5m to the east (NSR2). An assessment to each of these is presented below.

3.1 Residential Assessment – NSR1

Based on the requirements of Condition 5, the rating level from any items of fixed mechanical plant should not exceed 5 dB below the background sound level at the receptor. Based on the modal background sound level of 50 dB $L_{A90,T}$, would mean that the rating level should be controlled to not exceed 45 dB $L_{A,r,Tr}$.

By allowing for appropriate distance attenuation ($=20 \times \log(1/90)$), calculations indicate that specific sound levels would be **37 dB $L_{Aeq,Tr}$** external to NSR1 assuming the determined specific level in Table 2 (76dBA).

As the residential receptor is heavily screened from the rooftop plant, no associated BS4142 character corrections would be applied to the specific sound level as they would not be perceptible against the residual acoustic environment.

Based on the above, a rating level of 37 dB $L_{A,r,Tr}$ would be determined at NSR1 which is significantly below the target criterion of 45 dB $L_{A,r,Tr}$. Therefore, the requirements have been met.

3.2 Office Development Assessment – NSR2

The nearest office building is located 5m away to the east. From on-site observations, these areas are all ventilated via mechanical ventilation and all windows are force closed. As such, noise break in via the closed windows has been considered.

As the windows are force closed, the criterion to ensure the rating sound level does not exceed 5 dB below the background sound level would not be appropriate nor relevant. Based on guidance presented in BS 8233:2014, internal noise levels within staff/meeting rooms should not exceed 35 – 45 dB $L_{Aeq,T}$. As the noise source in question relates to mechanical plant, it is proposed that a figure of **40 dB $L_{Aeq,T}$** is targeted internally (NR35) for external plant noise break-in.

By allowing for appropriate distance attenuation ($=20 \times \log(1/5)$), calculations indicate that noise levels would be **62 dB(A)** external to these office windows assuming the determined specific level in Table 2 (76dBA).

It was observed on-site that the entire external envelope of these offices is glazed. Assuming standard double glazing (31 dB R_w) and glazed percentage areas of >90%, noise break-in calculations are presented below.

Staff / Meeting Room Day Time Leq

Item / Description	dB(A)	63	125	250	500	1k	2k	4k	8k
Corrected Leq,T Spectrum	62	70	62	62	60	57	53	49	42
Glazing Noise Ingress	37	50	41	44	31	18	19	10	4
Ventilation Noise Ingress									
Wall Noise Ingress	-3	17	3	2	-11	-14	-18	-23	-29
Roof Noise Ingress									
Room Absorption Correction		0	0	-1	-1	-1	-2	-3	-4
Total Noise Ingress	39	53	44	46	33	20	20	11	3
NR35	40	63	52	44	38	35	32	29	28
Exceedance of Criteria	-1	-10	-8	2	-5	-15	-12	-18	-25

Note: 1 - 2 dB exceedences are considered marginal and deemed acceptable.

Based on the above, the requirement to not exceed NR35 would be achieved. large, glazed noted that these calculations assume reasonable worst-case assumptions (low external envelope performances and large glazed areas) and, therefore, the above assessment is sufficiently robust and the requirements have been met.

4. Conclusion and Action Plan

The proposed development has been assessed against the requirements of Condition 5 placed on the scheme by the LPA, and the guidance documents presented in Section 1.1.

In summary, the noise impact assessment has included the following:

1. A noise impact assessment has been completed to the nearest receptors to the rooftop external plant (both residential and otherwise).
2. In summary, the BS4142 rating sound level would not exceed the criterion at the nearest residential receptor specified by the LPA, and Condition 5 can be effectively discharged without any mitigation measures.
3. Plant noise emissions to the nearby offices would be effectively controlled to not exceed appropriate internal noise levels.

The findings of this report will require written approval from the Local Authority prior to work commencing.

Appendix A – Acoustic Terminology

A-weighted sound pressure level, L_{pA}	Quantity of A-weighted sound pressure given by the following formula in decibels (dBA). $L_{pA} = 10 \log_{10} (pA/p_0)^2$. Where: pA is the A-weighted sound pressure in pascals (Pa) and p_0 is the reference sound pressure (20 μ Pa)
Background Sound	Underlying level of sound over a period, T , which might in part be an indication of relative quietness at a given location
Equivalent continuous A-weighted sound pressure level, $L_{Aeq,T}$	Value of the A-weighted sound pressure level in decibels (dB) of a continuous, steady sound that, within a specified time interval, T , has the same mean-squared sound pressure as the sound under consideration that varies with time
Facade level	Sound pressure level 1m in front of the facade
Free-field level	Sound pressure level away from reflecting surfaces
Noise Criteria	Numerical indices used to define design goals in a given space
Noise Rating (NR)	Graphical method for rating a noise by comparing the noise spectrum with a family of noise rating curves
Octave Band	Band of frequencies in which the upper limit of the band is twice the frequency of the lower limit
Percentile Level, $L_{AN,T}$	A-weighted sound pressure level obtained using time-weighting “F”, which is exceeded for $N\%$ of a specified time interval
Rating Level, $L_{Ar,Tr}$	Equivalent continuous A-weighted sound pressure level of the noise, plus any adjustment for the characteristic features of the noise
Sound Pressure, p	root-mean-square value of the variation in air pressure, measured in pascals (Pa) above and below atmospheric pressure, caused by the sound
Sound Pressure Level, L_p	Quantity of sound pressure, in decibels (dB), given by the formula: $L_p = 10 \log_{10} (p/p_0)^2$. Where: p is the root-mean-square sound pressure in pascals (Pa) and p_0 is the reference sound pressure (20 μ Pa)

Appendix B – Standards, Legislation, Policy, and Guidance

This report is to be primarily based on the following standards, legislation, policy and guidance.

B.1 – National Planning Policy Framework (2023)

Government policy on noise is set out in the National Planning Policy Framework (NPPF), published in 2023. This replaced all earlier guidance on noise and places an emphasis on sustainability. In section 15, Conserving and enhancing the natural and local environment, paragraph 180e, it states:

Preventing new and existing development from contributing to, being put at unacceptable risk from, or being adversely affected by, unacceptable levels of soil, air, water or noise pollution or land instability. Development should, wherever possible, help to improve local environmental conditions such as air and water quality, taking into account relevant information such as river basin management plans;

Paragraph 191 states:

Planning policies and decisions should also ensure that new development is appropriate for its location taking into account the likely effects (including cumulative effects) of pollution on health, living conditions and the natural environment, as well as the potential sensitivity of the site or the wider area to impacts that could arise from the development. In doing so they should:

- a) Mitigate and reduce to a minimum potential adverse impact resulting from noise from new development – and avoid noise giving rise to significant adverse impacts on health and the quality of life;*
- b) Identify and protect tranquil areas which have remained relatively undisturbed by noise and are prized for their recreational and amenity value for this reason; and*
- c) Limit the impact of light pollution from artificial light on local amenity, intrinsically dark landscapes and nature conservation.*

B.2 – Noise Policy Statement for England (2010)

Paragraph 191 of the NPPF also refers to advice on adverse effects of noise given in the Noise Policy Statement for England (NPSE). This document sets out a policy vision to:

Promote good health and a good quality of life through the effective management of noise within the context of Government policy on sustainable development.

To achieve this vision the Statement identifies the following three aims:

Through the effective management and control of environmental, neighbour and neighbourhood noise within the context of Government policy on sustainable development:

- 1) Avoid significant adverse impacts on health and quality of life.
- 2) Mitigate and minimise adverse impacts on health and quality of life.
- 3) Where possible, contribute to the improvement of health and quality of life.

In achieving these aims the document introduces significance criteria as follows:

SOAEL – Significant Observed Adverse Effect Level

This is the level above which significant adverse effects on health and quality of life occur. It is stated that *“significant adverse effects on health and quality of life should be avoided while also considering the guiding principles of sustainable development”*.

LOAEL – Lowest Observed Adverse Effect Level

This is the level above which adverse effects on health and quality of life can be detected. It is stated that the second aim refers to the situation where impact lies somewhere between LOAEL and SOAEL and requires that: *“all reasonable steps should be taken to mitigate and minimise adverse effects on health and quality of life while also considering the guiding principles of sustainable development. This does not mean that such adverse effects cannot occur.”*

NOEL – No Observed Effect Level

This is the level below which no effect can be detected. In simple terms, below this level, there is no detectable effect on health and quality of life due to the noise. This can be related to the third aim above, which seeks: *“where possible, positively to improve health and quality of life through the pro-active management of noise while also considering the guiding principles of sustainable development, recognising that there will be opportunities for such measures to be taken and that they will deliver potential benefits to society. The protection of quiet places and quiet times as well as the enhancement of the acoustic environment will assist with delivering this aim”*.

This is further expanded using the updated “Noise Exposure Hierarchy Table” which includes an additional level of impact referred to as the ‘No Observed Adverse Effect Level’ (‘NOAEL’). It is stated that at this level: *“noise can be heard, but does not cause any change in behaviour, attitude or other physiological response”*. In addition, noise at this level *“can slightly affect the acoustic character of the area but not such that there is a change in the quality of life”*.

The NPSE recognises that it is not possible to have a single objective noise-based measure that is mandatory and applicable to all sources of noise in all situations and provides no guidance as to how these criteria should be interpreted. It is clear, however, that there is no requirement to achieve noise levels where there are no observable adverse impacts but that reasonable and practicable steps to reduce adverse noise impacts should be taken in the context of sustainable development and ensure a balance between noise sensitive and the need for noise generating developments.

Any scheme of noise mitigation outlined in this report will, therefore, aim to abide by the above principles of the NPPF and NPSE whilst recognising the constraints of the site.

B.3 – BS4142:2014+A1:2019 – ‘Methods for rating and assessing industrial and commercial sound’

Overview

BS4142 sets out a method to assess the likely effect of sound from factories, industrial premises or fixed installations and sources of an industrial nature in commercial premises, on people who might be inside or outside a dwelling or premises used for residential purposes in the vicinity.

The procedure contained in BS4142 for assessing the effect of sound on residential receptors is to compare the measured or predicted sound level from the source in question, the $L_{Aeq,T}$ ‘specific sound level’, immediately outside the dwelling with the $L_{A90,T}$ background sound level.

Where the sound contains a tonality, impulsivity, intermittency and other sound characteristics, then a correction depending on the grade of the aforementioned characteristics of the sound is added to the specific sound level to obtain the $L_{A,r,T}$ ‘rating sound level’. A correction to include the consideration of a level of uncertainty in sound measurements, data and calculations can also be applied when necessary.

Rating Penalty

Section 9 of BS4142 describes how the rating sound level should be derived from the specific sound level, by deriving a rating penalty.

BS4142 states:

“Certain acoustic features can increase the significance of impact over that expected from a basic comparison between the specific sound level and the background sound level. Where such features are present at the assessment location, add a character correction to the specific sound level to obtain the rating level. This can be approached in three ways:

- a) subjective method;*
- b) objective method for tonality;*
- c) reference method.”*

Due to the nature of the development the subjective method has been adopted to derive the rating sound level from the specific sound level. This is discussed in Section 9.2 of BS4142, which states:

“Where appropriate, establish a rating penalty for sound based on a subjective assessment of its characteristics. This would also be appropriate where a new source cannot be measured because it is only proposed at that time, but the characteristics of similar sources can subjectively be assessed. Correct the specific sound level if a tone, impulse or other characteristics occurs, or is expected to be present, for new or modified sound sources.”

BS4142 defines four characteristics that should be considered when deriving a rating penalty, namely; tonality; impulsivity; intermittency; and other sound characteristics, which are defined as:

- a) Tonality*

A rating penalty of +2dB is applicable for a tone which is “just perceptible”, +4dB where a tone is “clearly perceptible”, and +6dB where a tone is “highly perceptible”.

b) Impulsivity

A rating penalty of +3dB is applicable for impulsivity which is “just perceptible”, +6dB where it is “clearly perceptible”, and +9dB where it is “highly perceptible”.

c) Other Sound Characteristics

BS4142 states that where “the specific sound features characteristics that are neither tonal nor impulsive, though otherwise are readily distance against the residual acoustic environment, a penalty of +3dB can be applied.”

d) Intermittency

BS4142 states that when the “specific sound has identifiable on/off conditions, the specific sound level ought to be representative of the time period of length equal to the reference time interval which contains the greatest total amount of on time ... if the intermittency is readily distinctive against the residual acoustic environment, a penalty of +3dB can be applied.”

Background Sound Level

The background sound level is the underlying level of sound over a period, T, and is indicative of the relative quietness at a given location. It does not reflect the occurrence of transient and/or higher sound level events and is generally governed by continuous or semi-continuous sounds.

To ensure the background sound level values used within the assessment are reliable and suitably represent both the particular circumstance and periods of interest, efforts have been made to quantify a ‘typical’ background sound level for a given period. The purpose has not been to simply select the lowest measured value. Diurnal patterns have also been considered as they can have a major influence on background sound levels, for example, the middle of the night can be distinctly different (and potentially of lesser importance) compared to the start or end of the night time period for sleep purposes.

Since the intention is to determine a background sound level in the absence of the specific sound that is under consideration, it is necessary to understand that the background sound level can in some circumstances legitimately include industrial and/or commercial sounds that are present as separate to the specific sound.

Assessment of Impact

BS4142 states: “*The significance of sound of an industrial and/or commercial nature depends upon both the margin by which the rating level of the specific sound source exceeds the background sound level and the context in which the sound occurs*”. An estimation of the impact of the specific sound can be obtained by the difference of the rating sound level and the background sound level and considering the following:

- “Typically, the greater this difference, the greater the magnitude of the impact.”
- “A difference of around +10dB or more is likely to be an indication of a significant adverse impact, depending on the context.”
- “A difference of around +5dB is likely to be an indication of an adverse impact, depending on the context.”

- “The lower the rating level is relative to the measured background sound level, the less likely it is that the specific sound source will have an adverse impact or a significant adverse impact. Where the rating level does not exceed the background sound level, this is an indication of the specific sound source having a low impact, depending on the context.”

Interpreting the guidance given in BS4142, with consideration of the guidance given in the NPSE and NPPG Noise, an estimation of the impact of the rating sound is summarised in the following text:

- A rating sound level that is +10dB above the background sound level is likely to be an indication of a ‘Significant Observed Adverse Effect Level’;
- A rating sound level that is +5dB above the background sound level is likely to be an indication of a ‘Lowest Observed Adverse Effect Level’;
- The lower the rating sound level is relative to the measured background sound level, the less likely it is that the specific sound source will have an adverse impact or a significant adverse impact. Where the rating sound level does not exceed the background sound level, this is an indication of the specific sound source having a low impact and would therefore classify as ‘No Observed Adverse Effect Level’;
- At levels significantly below the measured background sound level (i.e. greater than 10dB), this is an indication of a ‘No Adverse Effect Level’.

During the daytime, the assessment is carried out over a reference time period of 1-hour. The periods associated with day or night, for the purposes of the Standard, are 07.00 to 23.00 and 23.00 to 07.00, respectively.

Appendix C – Location Plans



Appendix D – Environmental Survey

D.1 – Time History Noise Data

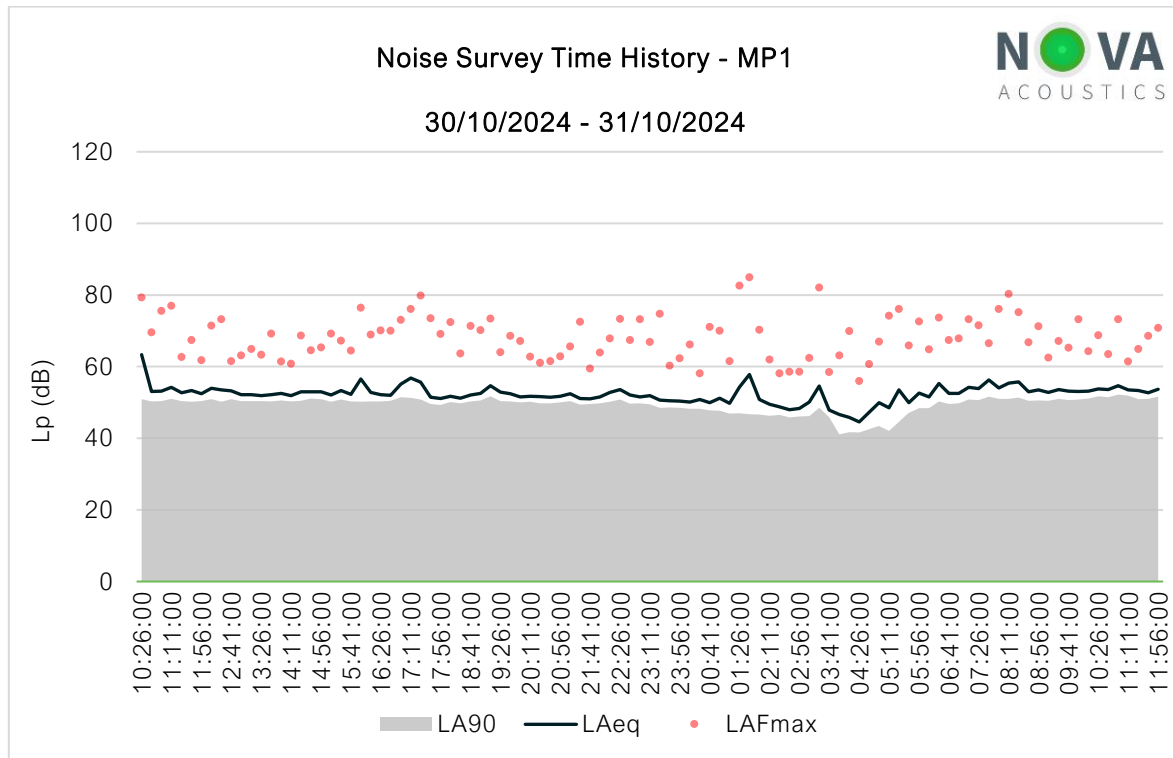


Figure 4 – MP1 Noise Survey Time History

D.2 – Surveying Equipment

Piece of Equipment	Serial No.	Calibration Deviation
Svantek SV971A Class 1 Sound Level Meter	141427	≤0.1
Svantek SV36 Class 1 Calibrator	106876	

Table 3 – Surveying Equipment

All equipment used during the survey was field calibrated at the start and end of the measurement period with negligible deviation noted. All sound level meters are calibrated every 24 months and all calibrators are calibrated every 12 months by a third-party calibration laboratory. All microphones were fitted with a protective windshield for the entire measurements period. Calibration certificates can be provided upon request.

D.3 – Meteorological Conditions

As the environmental noise survey was carried out over a long un-manned period no localised records of weather conditions were taken. However, all measurements have been compared with met office weather data of the area, specifically the closest weather station, and the data from the weather station is outlined in the table below. When reviewing the time history of the noise measurements, any scenarios that were considered potentially to be affected by the local weather conditions have been omitted.

The analysis of the noise data includes statistical and percentile analysis and review of minimum and maximum values, which aids in the preclusion of any periods of undesirable weather conditions. The weather conditions were deemed suitable for the measurement of environmental noise in accordance with BS7445 Description and Measurement of Environmental Noise. The table below presents the average temperature, wind speed and rainfall range for each 24-hour period during the entire measurement.

Weather Conditions – Chorlton (Approx. 4.9km SW of Site)				
Time Period	Air Temp (°C)	Rainfall (mm/h)	Prevailing Wind Direction	Wind Speed (m/s)
30/10/2024: 00:00 – 23:59	10.6 – 12.4	0.0	W	0.0 – 0.2
31/10/2024: 00:00 – 23:59	9.7 – 11.5	0.0 – 1.4 ^[1]	W	0.0 – 0.4
Notes:				
[1] rainfall recorded between 06:00 – 08:00 hours, however, did not impact measurements.				

Table 4 – Weather Conditions

Appendix E – Manufacturer Datasheets

1. SPECIFICATIONS

Outdoor units

Model			PURY-P900YSNW-A (-BS)		
Power source			3-phase 4-wire 380-400-415 V 50/60 Hz		
Cooling capacity (Nominal)	*1	kW	101.0		
		kcal/h	86,900		
		BTU/h	344,600		
		Power input	25.76		
	Current input	A 43.4-41.3-39.8			
Temp. range of cooling	EER	kW/kW 3.92			
	Indoor	W.B.	15.0~24.0°C (59~75°F)		
	Outdoor	D.B.	-5.0~52.0°C (23~126°F)		
Heating capacity (Max)	*2	kW	113.0		
		kcal/h	97,200		
		BTU/h	385,600		
		Power input	28.03		
	Current input	A 47.3-44.9-43.3			
	COP	kW/kW 4.03			
	(Nominal)	*3	kW	101.0	
			kcal/h	86,900	
			BTU/h	344,600	
			Power input	22.74	
		Current input	A 38.3-36.4-35.1		
COP		kW/kW 4.44			
Temp. range of heating		Indoor	D.B.	15.0~27.0°C (59~81°F)	
	Outdoor	W.B.	-20.0~15.5°C (-4~60°F)		
Indoor unit connectable	Total capacity		50~150% of outdoor unit capacity		
	Model/Quantity		P15~P250/2~50		
Sound pressure level (measured in anechoic room) *4		dB <A>	68.5/73.0		
Sound power level (measured in anechoic room) *4		dB <A>	86.0/92.0		
Refrigerant piping diameter	High pressure	mm (in.)	28.58 (1-1/8) Brazed		
	Low pressure	mm (in.)	41.28 (1-5/8) Brazed		

Model			PURY-P450YNW-A (-BS)	PURY-P450YNW-A (-BS)
FAN	Type x Quantity		Propeller fan x 2	Propeller fan x 2
	Air flow rate	m ³ /min	315	315
		L/s	5,250	5,250
		cfm	11,123	11,123
	Control, Driving mechanism		Inverter-control, Direct-driven by motor	Inverter-control, Direct-driven by motor
	Motor output	kW	0.46 x 2	0.46 x 2
Compressor	External static press.		0 Pa (0 mmH ₂ O)	0 Pa (0 mmH ₂ O)
	Type		Inverter scroll hermetic compressor	Inverter scroll hermetic compressor
	Manufacture		AC&R Works, MITSUBISHI ELECTRIC CORPORATION	AC&R Works, MITSUBISHI ELECTRIC CORPORATION
	Starting method		Inverter	Inverter
	Motor output	kW	12.4	12.4
	Case heater	kW	-	-
External finish	Lubricant		MEL32	MEL32
			Pre-coated galvanized steel sheets (+powder coating for -BS type) <MUNSELL 5Y 8/1 or similar>	Pre-coated galvanized steel sheets (+powder coating for -BS type) <MUNSELL 5Y 8/1 or similar>
	External dimension H x W x D	mm	1,858 (1,798 without legs) x 1,240 x 740	1,858 (1,798 without legs) x 1,240 x 740
		in.	73-3/16 (70-13/16 without legs) x 48-7/8 x 29-3/16	73-3/16 (70-13/16 without legs) x 48-7/8 x 29-3/16
	Protection devices	High pressure protection	High pressure sensor, High pressure switch at 4.15 MPa (601 psi)	High pressure sensor, High pressure switch at 4.15 MPa (601 psi)
		Inverter circuit (COMP./FAN)	Over-heat protection, Over-current protection	Over-heat protection, Over-current protection
Refrigerant	Compressor		-	-
	Fan motor		-	-
	Type x original charge		R410A x 10.8 kg (24 lbs)	R410A x 10.8 kg (24 lbs)
	Control		Indoor LEV and BC controller	
	Net weight	kg (lbs)	293 (646)	293 (646)
	Heat exchanger		Salt-resistant cross fin & copper tube	Salt-resistant cross fin & copper tube
Pipe between unit and distributor	HIC circuit (HIC: Heat Inter-Change)		-	-
	High pressure	mm (in.)	22.2 (7/8) Braze	22.2 (7/8) Braze
	Low pressure	mm (in.)	28.58 (1-1/8) Braze	28.58 (1-1/8) Braze
	Defrosting method		Auto-defrost mode (Reversed refrigerant cycle)	
	Drawing	External	WKS94T753	
		Wiring	WKE94G341	WKE94G341
Optional parts	Standard attachment	Document	Installation Manual	
		Accessory	-	
	Outdoor Twinning kit: CMY-R200VBK4 Joint: CMY-Y102SS-G2, CMY-Y102LS-G2, CMY-R160-J1 Main BC controller: CMB-P108, 1012, 1016V-JA, CMB-P1016V-KA Sub BC controller: CMB-P104, 108V-KB			
	Remarks			
	Details on foundation work, duct work, insulation work, electrical wiring, power source switch, and other items shall be referred to the Installation Manual. Due to continuing improvement, above specifications may be subject to change without notice.			

Notes:	Unit converter
1. Nominal cooling conditions (subject to JIS B8615-2) Indoor: 27°C D.B./19°C W.B. (81°F D.B./66°F W.B.), Outdoor: 35°C D.B./24°C W.B. (95°F D.B./75°F W.B.) Pipe length: 7.5 m (24-9/16 ft.), Level difference: 0 m (0 ft.)	BTU/h = kW x 3,412
2. Nominal heating conditions (subject to JIS B8615-2) Indoor: 20°C D.B. (68°F D.B.), Outdoor: 7°C D.B./6°C W.B. (45°F D.B./43°F W.B.) Pipe length: 7.5 m (24-9/16 ft.), Level difference: 0 m (0 ft.)	cfm = m ³ /min x 35.31
3. Nominal heating conditions (subject to JIS B8615-2) Indoor: 20°C D.B. (68°F D.B.), Outdoor: 7°C D.B./6°C W.B. (45°F D.B./43°F W.B.) Pipe length: 7.5 m (24-9/16 ft.), Level difference: 0 m (0 ft.)	lbs = kg/0.4536
4. Cooling mode/heating mode	
5. External static pressure option is available (30 Pa, 60 Pa, 80 Pa/3.1 mmH ₂ O, 6.1 mmH ₂ O, 8.2 mmH ₂ O). Consult your dealer about the specification when setting External static pressure option.	*Above specification data is subject to rounding variation.

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