

**35 Garratt Way. Gorton
Manchester, M18 8HD**

**Proposed Quick Lane Centre
Planning Noise Impact Assessment**

Report ref.

RK2941/20067/Rev 0

Issued to

Jones Lang LaSalle

Prepared by

Rob Kirkaldy BSc (Hons) MIOA
Senior Consultant

Version	Remarks	Date
Rev 0	Initial report issue.	05.03.2020



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1. INTRODUCTION

Jones Lang LaSalle's client Quick Lane are seeking planning permission to redevelop a former retail unit located at 35 Garratt Way in Gorton, Manchester into a new vehicle maintenance workshop. The site is located opposite residential properties. Accordingly, a noise impact assessment is required.

Spectrum Acoustic Consultants have been instructed by Jones Lang LaSalle to carry out a Noise Impact Assessment to support the application. This report is submitted with the intention of providing sufficient information to both inform and satisfy the requirements of the Local Planning Authority.

2. SITE DESCRIPTION & PROPOSALS

The development site is located at 35 Garratt Way, Gorton, Manchester, M18 8HD. Garratt Way bounds the site to the north and has a number of commercial properties and houses located along it. The commercial properties include an Aldi supermarket, petrol filling station, drive-thru restaurant, Police Station, Tesco supermarket and Gorton Market. Bounding the site to the south is Hyde Road, a busy road leading to the centre of Manchester, which also has a number of other commercial properties located along it. Bounding the site to the east is the drive-thru restaurant. To the west is the petrol filling station which operates twenty-four hours per day. An existing site location plan is included in Appendix A.

Proposals involve converting the property to create a vehicle maintenance workshop. The workshop would include three vehicle bays, an MOT station, reception, office, welfare facilities and storage areas. The main workshop would be accessed via three roller shutter doors on the east side of the building. Access to the site would be retained via Garratt Way. The proposed operational hours for the site are 07:00 to 20:00, Mondays to Saturdays, and 08:00 to 17:00 on Sundays. Scheme proposals are included in Appendix B.

3. NOISE CRITERIA

3.1 NATIONAL PLANNING POLICY FRAMEWORK (NPPF), FEBRUARY 2019

The National Planning Policy Framework (NPPF) sets out the government's guidance for local planning authorities and planning application decision-takers.

It says that the planning system should contribute to and enhance the environment by (among other things) preventing development from contributing to, being put at risk from, or being adversely affected by unacceptable levels of noise pollution. (Para. 170.e)

Paragraph 180 states that:

- Mitigate and reduce to a minimum potential adverse impacts resulting from noise from new development – and avoid noise giving rise to significant adverse impacts on health and the quality of life;
- Identify and protect areas of tranquillity which have remained relatively undisturbed by noise and are prized for their recreational and amenity value for this reason."



Paragraph 182 states that planning policies and decisions should ensure that:

- New development can be integrated effectively with existing businesses and community facilities (such as places of worship, pubs, music venues and sports clubs). Existing businesses and facilities should not have unreasonable restrictions placed on them as a result of development permitted after they were established. Where the operation of an existing business or community facility could have a significant adverse effect on new development (including changes of use) in its vicinity, the applicant (or 'agent of change') should be required to provide suitable mitigation before the development has been completed.

3.2 NOISE POLICY STATEMENT FOR ENGLAND (NPSE), DEFRA, MARCH 2010

The NPPF refers to the Noise Policy Statement for England (NPSE) which sets out the long term vision of Government noise policy as follows: *Promote good health and a good quality of life through the effective management of noise within the context of Government policy on sustainable development.*

The first aim of the Noise Policy Statement for England

Avoid significant adverse impacts on health and quality of life from environmental, neighbour and neighbourhood noise within the context of Government policy on sustainable development.

- 2.23 The first aim of the NPSE states that significant adverse effects on health and quality of life should be avoided while also taking into account the guiding principles of sustainable development (paragraph 1.8).

The second aim of the Noise Policy Statement for England

Mitigate and minimise adverse impacts on health and quality of life from environmental, neighbour and neighbourhood noise within the context of Government policy on sustainable development.

- 2.24 The second aim of the NPSE refers to the situation where the impact lies somewhere between LOAEL and SOAEL. It requires that all reasonable steps should be taken to mitigate and minimise adverse effects on health and quality of life while also taking into account the guiding principles of sustainable development (paragraph 1.8). This does not mean that such adverse effects cannot occur.

The third aim of the Noise Policy Statement for England

Where possible, contribute to the improvement of health and quality of life through the effective management and control of environmental, neighbour and neighbourhood noise within the context of Government policy on sustainable development.

- 2.25 This aim seeks, where possible, positively to improve health and quality of life through the proactive management of noise while also taking into account the guiding principles of sustainable development (paragraph 1.8), recognising that there will be opportunities for such measures to be taken and that they will deliver potential benefits to society. The protection of quiet places and quiet times as well as the enhancement of the acoustic environment will assist with delivering this aim.



3.3 PLANNING PRACTICE GUIDANCE (PPG)

The Planning Practice Guidance (PPG) refers to the NPPF and provides further guidance on the interpretation of no, lowest and significant observed adverse effect level described in the NPSE.

The PPG provides a commentary on the noise exposure hierarchy, based on the 'likely average response'.

The PPG recognises a broad range of factors which can influence the relationship between noise level and the impact on those affected. Accordingly, the examples in Table 1 below, copied from the PPG, may not be relevant to a specific development, which should be considered on its merits within the specific context under consideration.



Perception	Examples of Outcomes	Increasing Effect Level	Action
Not noticeable	No Effect	No Observed Effect	No specific measures required
Noticeable and not intrusive	Noise can be heard, but does not cause any change in behaviour or attitude. Can slightly affect the acoustic character of the area but not such that there is a perceived change in the quality of life.	No Observed Adverse Effect	No specific measures required
Noticeable and intrusive	Noise can be heard and causes small changes in behaviour and/or attitude, e.g. turning up volume of television; speaking more loudly; where there is no alternative ventilation, having to close windows for some of the time because of the noise. Potential for some reported sleep disturbance. Affects the acoustic character of the area such that there is a perceived change in the quality of life.	Lowest Observed Adverse Effect Level Observed Adverse Effect	Mitigate and reduce to a minimum
Noticeable and disruptive	The noise causes a material change in behaviour and/or attitude, e.g. avoiding certain activities during periods of intrusion; where there is no alternative ventilation, having to keep windows closed most of the time because of the noise. Potential for sleep disturbance resulting in difficulty in getting to sleep, premature awakening and difficulty in getting back to sleep. Quality of life diminished due to change in acoustic character of the area.	Significant Observed Adverse Effect Level Significant Observed Adverse Effect	Avoid
Noticeable and very disruptive	Extensive and regular changes in behaviour and/or an inability to mitigate effect of noise leading to psychological stress or physiological effects, e.g. regular sleep deprivation/awakening; loss of appetite, significant, medically definable harm, e.g. auditory and non-auditory	Unacceptable Adverse Effect	Prevent

Table 1: Summary of noise exposure hierarchy, based on likely response

3.4 BS 4142:2014 METHODS FOR RATING AND ASSESSING INDUSTRIAL AND COMMERCIAL SOUND

The noise impact assessment relating to the proposed development will be carried out in accordance with the procedures set out in BS 4142:2014 *Methods for rating and assessing industrial and commercial sound*. The principle of BS 4142 is to determine an initial estimate of impact of industrial/commercial sound on nearby residents by comparing the Rating Level (sound level from the industrial/commercial source, with a correction applied for any acoustic features that characterise the sound) with the Background Sound Level (L_{A90} as measured in absence of the industrial/commercial source).



Generally, the greater the difference by which the Rating Level exceeds the Background Sound Level, the greater the magnitude of impact. BS 4142 states that *'a difference of around +10 dB or more is likely to be an indication of a significant adverse impact [...]. A difference of around +5 dB is likely to be an indication of an adverse impact [...]. Where the rating level does not exceed the background sound level, this is an indication of the specific sound source having a low impact.'*

However, BS 4142 also advises that *'when making assessments and arriving at decisions [...] it is essential to place the sound in context'* so in each case, the context in which the sound is placed must be considered and the initial estimate of impact should be modified accordingly. For example it advises *'Where background sound levels and rating levels are low, absolute levels might be as, or more, relevant than the margin by which the rating level exceeds the background. This is especially true at night.'* It also indicates that impacts estimated during *'the middle of the night can be distinctly different (and potentially of lesser importance) compared to the start or end of the night-time period for sleep purposes.'*

3.5 WHO – ENVIRONMENTAL NOISE GUIDELINES FOR THE EUROPEAN REGION 2018 (ENG)

New guidance from WHO titled Environmental Noise Guidelines for the European Region (ENG) was published in 2018. The document takes a very different approach to guidance set out in the previous WHO Guidelines for Community Noise 1999 (GCN) document by identifying separate thresholds for specific sources, rather than for community noise as a whole. Consequently, much of the earlier guidance set out in GCN is now absent from ENG. While ENG was intended to supersede GCN, it recognises this absence and states that *'indoor guideline values and any values not covered by the current guidelines (such as industrial noise and shopping areas) should remain valid.'*

3.6 GUIDELINES FOR COMMUNITY NOISE - WORLD HEALTH ORGANIZATION, 1999 (GCN)

Table 4.1 of GCN references a guideline façade level of $L_{Aeq,8 \text{ hour}}$ 45dB outside of bedrooms during the night time to avoid sleep disturbance. During the daytime and evening, Table 4.1 recommends a guideline noise level of $L_{Aeq,16 \text{ hour}}$ 55dB for outdoor living areas to avoid serious annoyance. Whilst noise levels outside of living rooms during the daytime are not listed in Table 4.1, a guideline internal level of $L_{Aeq,16 \text{ hour}}$ 35dB for habitable rooms is provided to avoid moderate annoyance. Given that a difference of 15dB(A) between noise levels outside and inside of bedrooms during the night time is stated, a guideline noise level of $L_{Aeq,16 \text{ hour}}$ 50dB outside of living rooms may be assumed.

4. BACKGROUND NOISE MEASUREMENT SURVEY

To inform the noise impact assessment, measurements of existing background noise levels were carried out during a noise survey conducted at the site from Thursday 27 February to Monday 2 March 2020. Weather conditions during the survey were mild and dry, with low to moderate wind speeds, presenting good conditions for noise measurement purposes.

Measurements of noise were carried out at the rear of the building within a secure compound located opposite the houses on Garratt Way, in accordance with BS 4142:2014 using an unattended noise logger. The monitoring location is considered representative of the nearest noise sensitive residential receptor locations to the proposed development. Measurements consisted of continuous 15 minute periods. The microphone was mounted on a pole, 2m above ground level. The location of the microphone is shown on the existing site location plan included in Appendix A.



The following instrumentation was used during the survey.

- Bruel & Kjaer Type 2250 Light Sound Level Meter s/n 3006954
- Bruel & Kjaer Type 4952 Microphone s/n 2922639

Before and after the survey, the sound level meter was field-calibrated in accordance with the manufacturer's guidelines, and no significant drift was observed. The meter, microphone and field calibrator are laboratory calibrated biennially in accordance with UKAS procedures or to traceable National Standards.

Measurements made were of the following parameters:

- Maximum Noise Level – defined as the maximum (L_{Amax} the maximum noise level)
- Residual Noise Level – defined as the Energy Average Level of a period, in the absence of noise from the proposed development (L_{Aeq})
- Background Noise Level – defined as level exceeded for 90% of a period, in the absence of the noise from the proposed development (L_{A90})

The measured noise profile at the noise monitoring location is shown in the following chart.

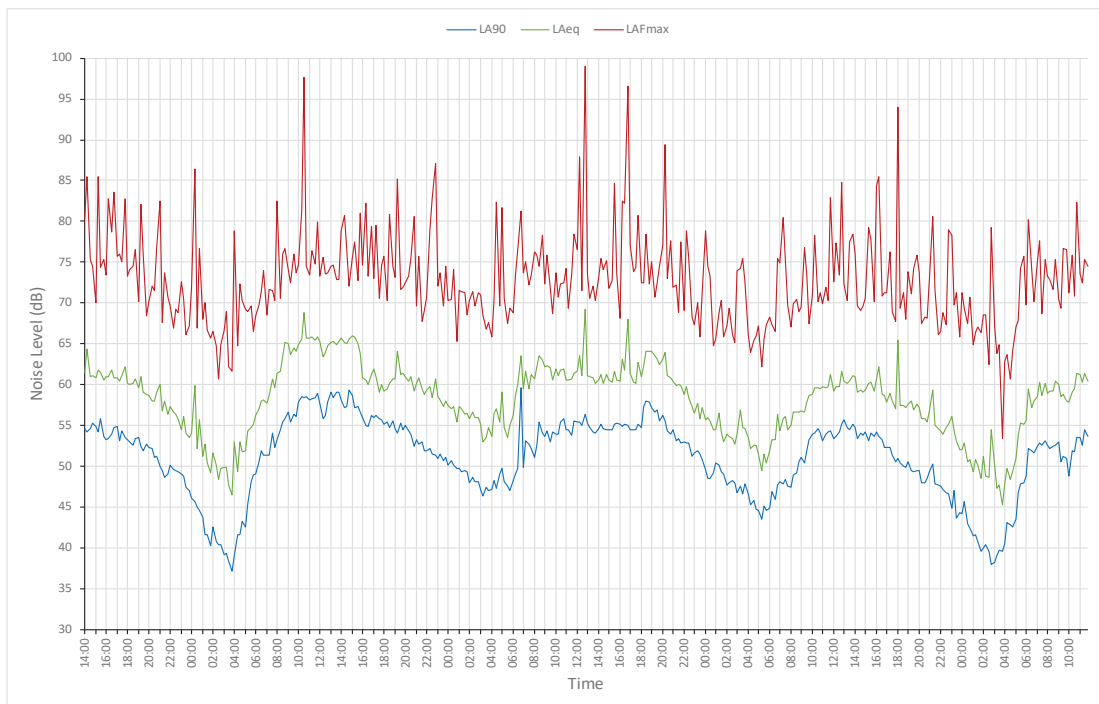


Chart 1: Ambient noise profile – Thursday 27 February to Monday 2 March 2020



When determining the representative background $L_{A90,T}$ level for the relevant period, BS 4142¹ guidance states “a representative level ought to account for the range in background levels and ought not automatically to be assumed to be either the minimum or modal value.” With this in mind, statistical analysis has been used to determine the typical background $L_{A90,T}$ noise level. This analysis derives the Mode, Mean and Mean -1 standard deviation values. Once these three values have been established, a judgement is made as to which value is considered representative. In this instance, the mean value is regarded as being representative.

Table 2 shows the representative background noise level measured at a position representative of the nearest noise sensitive receptor locations, during the proposed trading hours on a Sunday when the development would be operating and have the highest noise impact.

Measurement Location	Period	Background Noise Level
Rear site compound, representative of No.202 Garratt Way	Sunday 08:00 – 17:00	$L_{A90,1hour}$ 53dB

Table 2: Summary of the representative background noise level measured during the proposed trading hours on a Sunday

As shown in Table 2, the representative background noise level at the nearest noise sensitive receptors to the proposed development site is $L_{A90,1hour}$ 53dB during the proposed trading hours on a Sunday when the development would be operating and have the highest noise impact. This reflects a typical steady noise profile controlled by road traffic movements on Hyde Road, as well as other nearby commercial units in the area.

5. PROJECTED NOISE FROM THE PROPOSED USE

In order to establish the typical noise levels inside the proposed workshop, an attended noise measurement survey was carried out at an existing Quick Lane site in Prestwich on 2 March 2020. The measurements included short samples of noise from activities carried out as part of the operations which would be carried out at the proposed new development site.

The following instrumentation was used during the survey.

- Bruel & Kjaer Type 2260 Sound Level Meter s/n 1772232
- Bruel & Kjaer type 4189 Microphone s/n 2469838
- Bruel & Kjaer Type 4230 Acoustic Calibrator s/n 1234621
- Bruel & Kjaer Type ZC 0026 Preamplifier s/n

Before and after the survey, the sound level meter was field-calibrated in accordance with the manufacturer's guidelines, and no significant drift was observed. The meter, microphone and field calibrator are laboratory calibrated biennially in accordance with UKAS procedures or to traceable National Standards.

¹ BS 4142:2014 Methods for rating and assessing industrial and commercial sound

Simulated operations carried out during the survey included using an air-wrench to take off wheel nuts, using a hammer to remove brake discs, vehicles moving within the workshop, inflating tyres using a pneumatic air-line and removing tyres using an air-wrench.

A summary of the measured noise levels recorded inside the workshop are shown in Table 3 below.

Operation	Sample Time	Measured Reverberant Sound Pressure Level $L_{Aeq,T}$ (dB)
Air-Wrench taking off wheel Nuts.	1 min 49 secs	80
Hammering Discs of Brakes.	1 min 37 secs	80
Van driven into Bay 4, operator shouting instructions.	45 secs	74
Tyre Fit. Blowing up tyre with pneumatic air-line.	17 secs	69
Tyre removal using air-wrench.	34 secs	77
No activity. General Ambient due to fans.	38 secs	70

Table 3: Sample noise levels measured inside the existing Quick Lane workshop in Prestwich

To fit in the with the daytime assessment period in line with BS 4142:2014, the sample noise measurements have been corrected to be representative of a typical worst case one hour period when the workshop would be busiest. These are shown in Table 4 below.

Operation	Measured Reverberant Sound Pressure Level $L_{Aeq,T}$ (dB)	% On-Time	Time Corrected Reverberant Sound Pressure Level $L_{Aeq,1 \text{ hour}}$ (dB)
Air-Wrench taking off wheel Nuts.	80	5	67
Hammering Discs of Brakes.	80	5	67
Van driven into Bay 4, operator shouting instructions.	74	3	59
Tyre Fit. Blowing up tyre with pneumatic air-line.	69	2	52
Tyre removal using air-wrench.	77	2	60
No activity. General Ambient due to fans.	70	100	70
Total			73

Table 4: Sample noise levels measured inside the existing Quick Lane workshop in Prestwich, corrected to be representative of a typical worst case one hour period, in line with BS 4142:2014.

To accurately evaluate the overall effect of the operation of the proposed development, it is necessary to consider the noise levels that are likely to be generated by the operation, at the nearby residential locations.

Predictions of how the noise from the proposed development propagates to the sensitive receptors and the cumulative effect of all the noise sources is determined through modelling undertaken using proprietary software (Predictor²) which meets the requirements of ISO 9613 Part 2:1996³. The noise model takes account of the following in its calculations procedures:

- Source sound power level (for point, line and area sources)
- Reflection from nearby structures and source directivity
- Distance from noise source (geometric spreading)
- Atmospheric absorption
- Acoustic screening of intervening structures and topography
- Ground absorption
- Ground effects (which includes the height of ground relative to the noise source)

The noise prediction model uses the worst case total reverberant $L_{Aeq,1hour}$ shown in Table 4 as a basis for the prediction. Typical sound insulation properties for the building's façade elements such as the walls, roof and roller shutter doors are used in the model. It is anticipated that operations would be carried out with the roller shutter doors closed. However, during periods of hot weather, the doors may need to be open for short periods to prevent overheating. Therefore, a separate prediction which assumes the doors would be open has also been carried out. The sound insulation properties assumed in the model for the façade elements are set out in Table 5 below.

Element	Transmission loss dB - Octave band centre frequency							
	63	125	250	500	1k	2k	4k	8k
Walls (280mm brick, 56mm cavity, strip ties, outer faces plastered 12mm)	28	34	34	40	56	73	76	78
Roof (Profiled metal sheeting)	13	18	20	21	21	25	25	25
Roller Shutter doors (Typical for Roller Shutter Door)	13	18	19	20	22	24	25	25

Table 5: Sound insulation properties of the building's façade elements.

Detailed noise calculations of the totals at each receptor location are then computed. To illustrate the scheme, a diagram showing the distribution and locations of the emitting façade element noise sources, superimposed on a 3D view of the site, is included in Appendix C. The model results are also included in Appendix C.

6. NOISE IMPACT ASSESSMENT OF NOISE IMPACT

Table 6 shows a BS 4142:2014 assessment covering the potential noise impact, assuming the roller shutter doors would be closed. As indicated, the predicted rating levels are compared with the representative background $L_{A90,T}$ level measured during the daytime on a Sunday, when background noise levels are lower and the development would be operating at the nearby residential receptor locations.

² *Bruel and Kjaer – Predictor V11 Environmental Noise Calculation Software Package, Type 7810*

³ *ISO 9613-2:1996 "Acoustics – Attenuation of sound during propagation outdoors – Part 2: General method of calculation to determine Noise Levels"*



During the visit to the existing Quick Lane site in Prestwich, it was observed that the equipment used does not emit any distinct impulses or tones. However, a 3dB correction has been applied to account for other characteristics that may be distinctive against the residual acoustic environment experienced at the nearby residential receptor locations.

Residential Position	Specific Level (dB)	Feature Correction (dB)	Rating Level (dB)	Background L_{A90} (dB)	Assessment Level (dB) (Background excess)
R1. No.202 Garratt Way	27	+3	30	53	-23
R2. No.204 Garratt Way	24	+3	27	53	-26
R3. No.206 Garratt Way	24	+3	27	53	-26
R4. No.118 Hampton Crescent	27	+3	30	53	-23
R5. No.120 Hampton Crescent	27	+3	30	53	-23

Table 6: Predicted rating levels from the development (with roller shutter doors closed) at the nearby residential properties, compared with the representative Sunday daytime (08:00-17:00) background $L_{A90,1hour}$ level

The study predicts that at the nearest residential positions, rating levels associated with the proposed development would be comfortably lower than the representative background noise level during the proposed operating hours on a Sunday. The difference between the rating levels and background levels is such that any uncertainty is likely to have no significance on the outcome of the assessment. Furthermore, specific noise levels from the development would be comfortably lower than the GCN $L_{Aeq,16hour}$ 50dB advised criteria at all of the nearby residential receptor locations.

Note the assessment represents a worst case scenario, as it assumes noise levels generated over a busy one hour period on a Sunday when background noise levels are lower. Therefore, the proposed development would have a very low noise impact.

Operations would be carried out with the roller shutter doors closed. However, during periods of hot weather, the doors may occasionally need to be open for short periods to prevent overheating. Therefore, for information purposes, an assessment is provided below which assumes the doors would be open.

Residential Position	Specific Level (dB)	Feature Correction (dB)	Rating Level (dB)	Background L_{A90} (dB)	Assessment Level (dB) (Background excess)
R1. No.202 Garratt Way	46	+3	49	53	-4
R2. No.204 Garratt Way	27	+3	30	53	-23
R3. No.206 Garratt Way	26	+3	29	53	-24
R4. No.118 Hampton Crescent	46	+3	49	53	-4
R5. No.120 Hampton Crescent	46	+3	49	53	-4

Table 7: Predicted rating levels from the development (with roller shutter doors open) at the nearby residential properties, compared with the representative Sunday daytime (08:00-17:00) background $L_{A90,1hour}$ level



For the rare occasions that operations would need to be carried out with the roller shutter doors open, rating levels associated with the proposed development would still be lower than the representative background noise level during the proposed operating hours on a Sunday. Furthermore, specific noise levels from the development would remain be lower than the GCN $L_{Aeq,16\text{ hour}}$ 50dB advised criteria at all of the nearby residential receptor locations. Consequently, in line with BS 4142:2014 the noise impact would remain low even during the short periods when the doors would be open.

7. CONCLUSIONS

At the request of the Local Planning Authority, a noise assessment has been completed in connection with the conversion of a former retail unit located at 35 Garratt Way in Gorton, Manchester into a new vehicle maintenance workshop.

A background noise measurement survey has been conducted at a location representative of the nearest noise sensitive receptors to the proposed development and predictions of noise have been completed.

Noise limits for the proposed development have been established for the most sensitive Sunday daytime period when the development would be in operation, based on the representative background noise level and taking account of BS 4142:2014 and WHO. Predictions have indicated that noise levels from the development would have a low impact and would therefore be acceptable.

APPENDIX A

Existing Site Location Plans



N

Background Noise
Monitoring Location

Proposed
Development Site

ALDI

Top Hand Car Wash

ChargePoint
Charging Station

Texaco Gorton
petrol station

Gorton Police Station

KFC

Roots

VAPE ALOT

Gorton Tyres

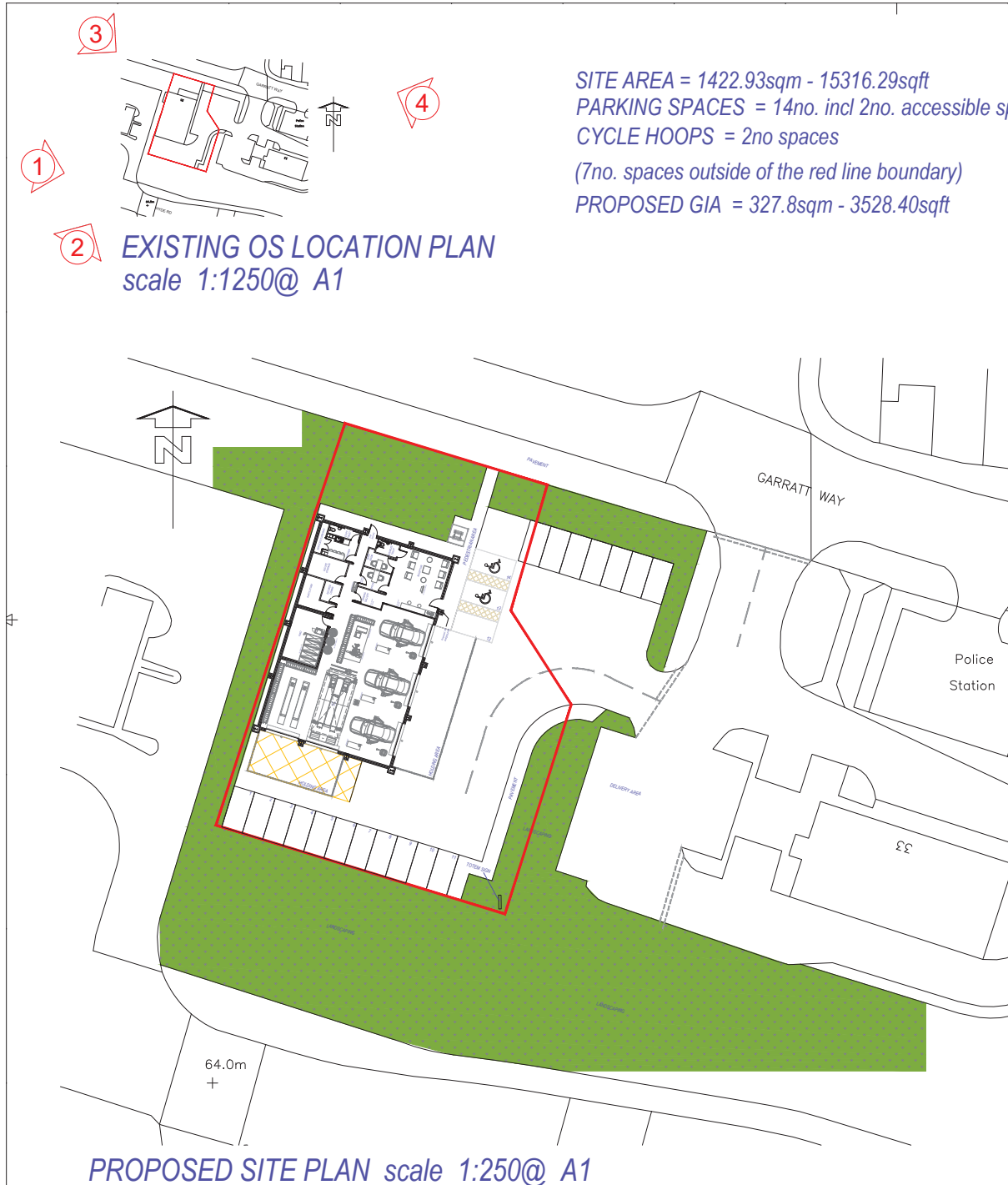
Gorton Payless

M & S Mobile Services

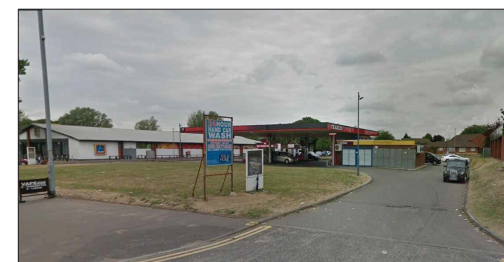
Easthub

APPENDIX B

Proposed Scheme Drawings



SITE PHOTO VIEW 1



SITE PHOTO VIEW 2



SITE PHOTO VIEW 3



SITE PHOTO VIEW 4

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B	12.12.19	Site Plan revised inline with SK02
A	08.11.19	Site photos annotation updated

REV	DATE	REMARKS
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Suite 2,
 Clocktower House,
 Station Rd,
 West Horndon,
 Essex,
 CM13 3XL
 tel: 01709 427899
 fax: 0709 223 4930
 e: office@qarchitects.ltd.uk
 web: www.qarchitects.ltd.uk



Client



Job Title
 35 Garrett way
 Manchester
 M18 8HD

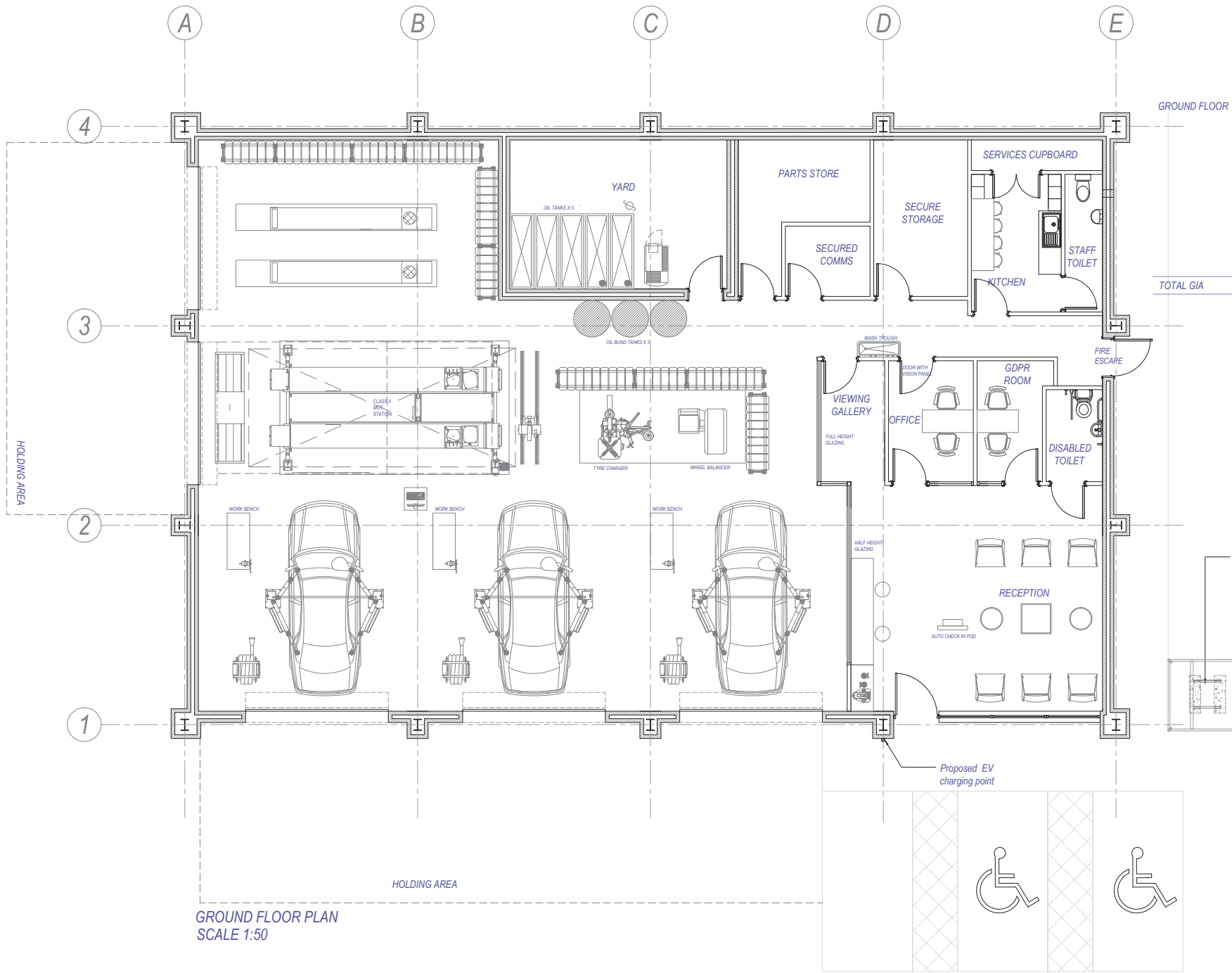
Drawing Title
 Proposed
 Quick Lane 4+1
 Site Plan

Scale 1:250 / 1:1250 Sheet size A1

Date 04/19 Dm. by MM

Orig. No. 19-0062/SK03 Rev. B

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AREA LEGEND		
RECEPTION	40m²	
OFFICE	7.2m²	
GDPR ROOM	6.1m²	
KITCHEN	10m²	
SERVICES	1.9m²	
STAFF TOILET	2.1m²	
DISABLED TOILET	3.3m²	
WORKSHOP	227m²	
PARTS STORE	10m²	
VIEWING GALLERY	5.6m²	
SECURED STORE	10.4m²	
SECURE COMMS	4.2m²	
TOTAL GIA		327.8m²
YARD		22.9m²

GROUND FLOOR PLAN
SCALE 1:50

B	12.12.19	Sheltered Cycle hoop added & position of EV charging point revised
A	08.11.19	Floor Plans revised inline with SK01 Rev C

REV No.	DATE	REMARKS
2		
1		

Client

Job Title

35 Garratt Way
Manchester
M18 8HD

Drawing Title

Proposed
Quick Lane 4+1
Ground Floor Plan

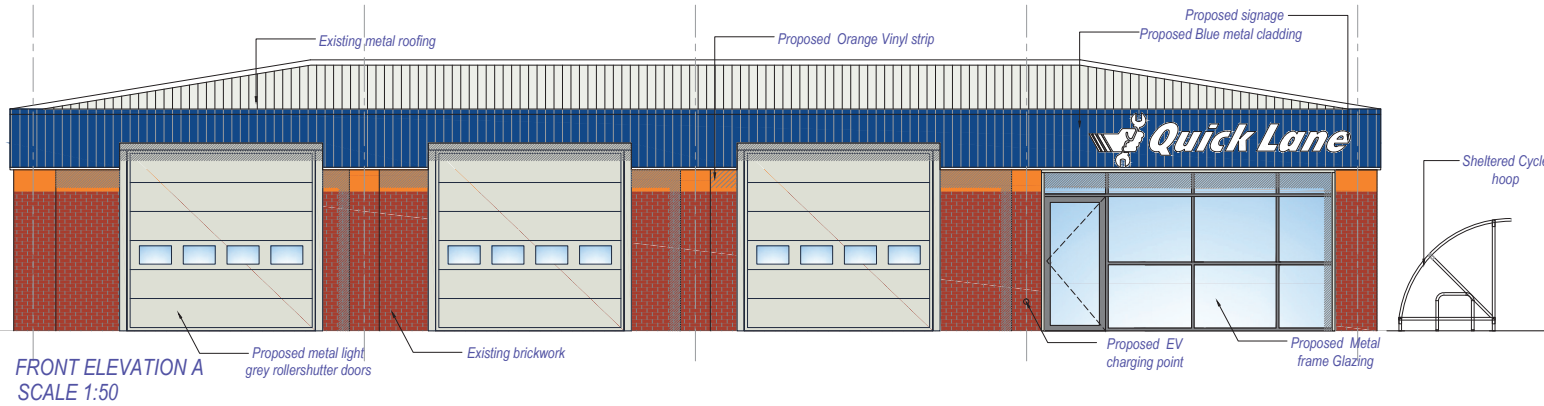
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Orig. No.	19-0062/SK02	Rev.	B

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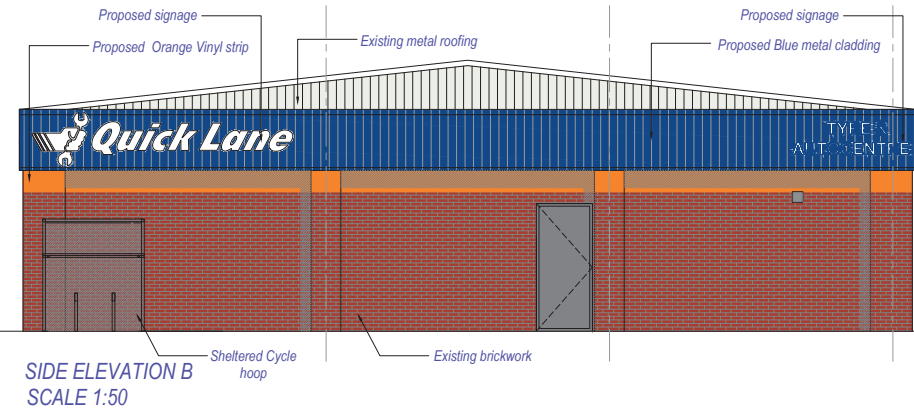
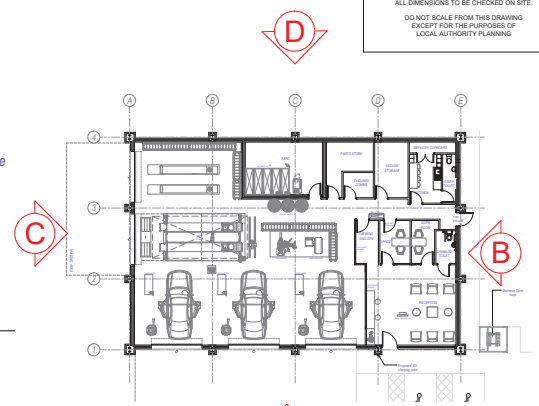
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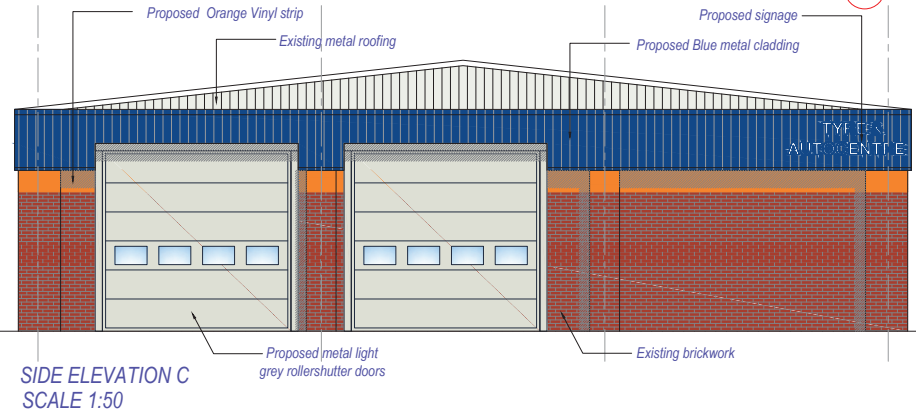
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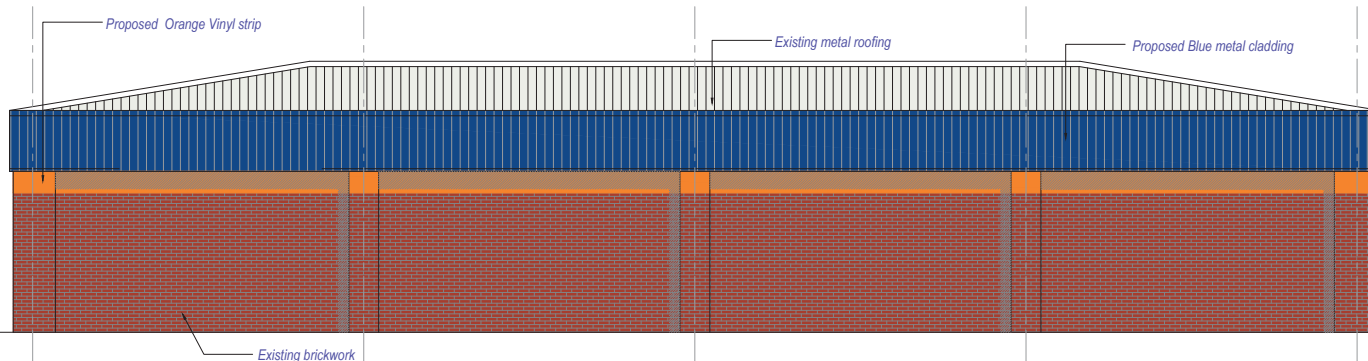
FRONT ELEVATION A
SCALE 1:50



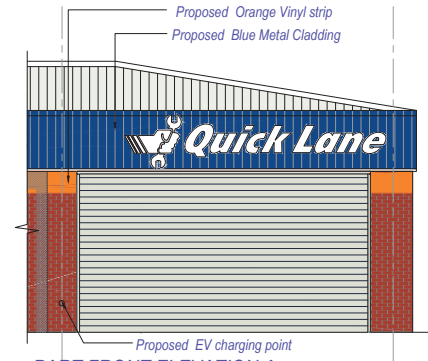
SIDE ELEVATION B
SCALE 1:50



SIDE ELEVATION C
SCALE 1:50



REAR ELEVATION D
SCALE 1:50



PART FRONT ELEVATION A WITH SHUTTERS CLOSED
SCALE 1:50

REV	DATE	REMARKS
E	13.12.19	Orange Vinyl strip annotated.
D	11.12.19	EV Charging point position revised. Existing & Proposed materials & Sheltered cycle hoop added as per Planning Consultants comments.
C	06.11.19	Layout revised as per MM comments. Shopfront to Elevation C & Fire exit to Yard removed. Staff Toilet relocated & Fire Exit Door added to Elevation B
B	01.11.19	Elevation B, C & Roller Shutters revised as per email dated 25/10/19
A	13.08.19	Roller shutter door revised

architects

Suite 2,
Clocktower House,
Station Rd,
West Horndon,
Essex,
CM13 3XL
tel: 01708 407889
fax: 01709 223 4930
e: office@architects.ltd.uk
web: www.architects.ltd.uk



Client

Job Title

35 Garratt Way
Manchester
M18 8HD

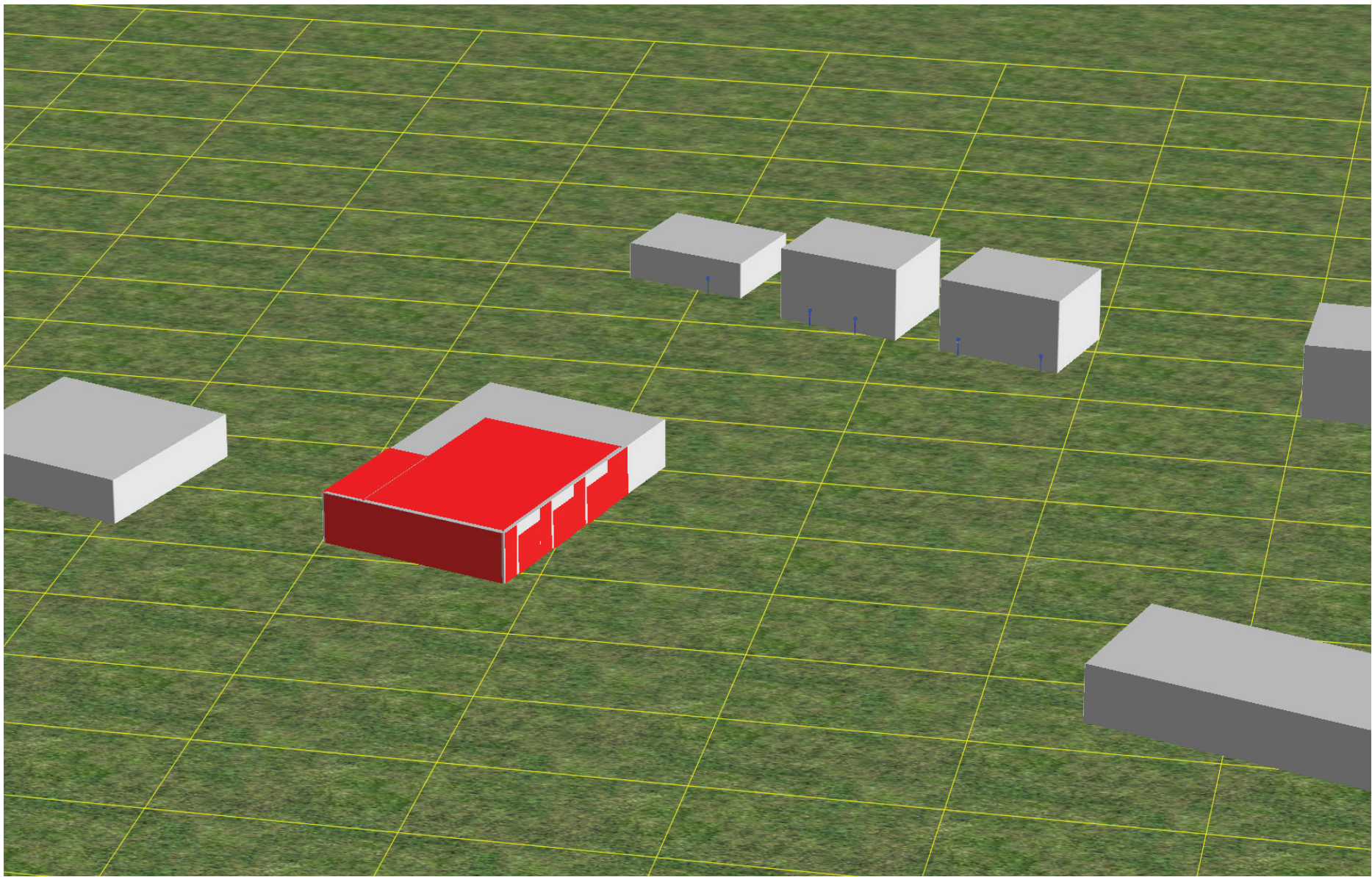
Drawing Title

Proposed
Quick Lane 4+1
Elevations

Scale	1:100	Sheet size	A1
Date	04/19	Dim. by	MM
Orig. No.	19.0062/SK01	Rev.	E

APPENDIX C

Noise Prediction Model



Quick Lane, Gorton
Predicted Noise Levels - Roller Shutter Doors Closed

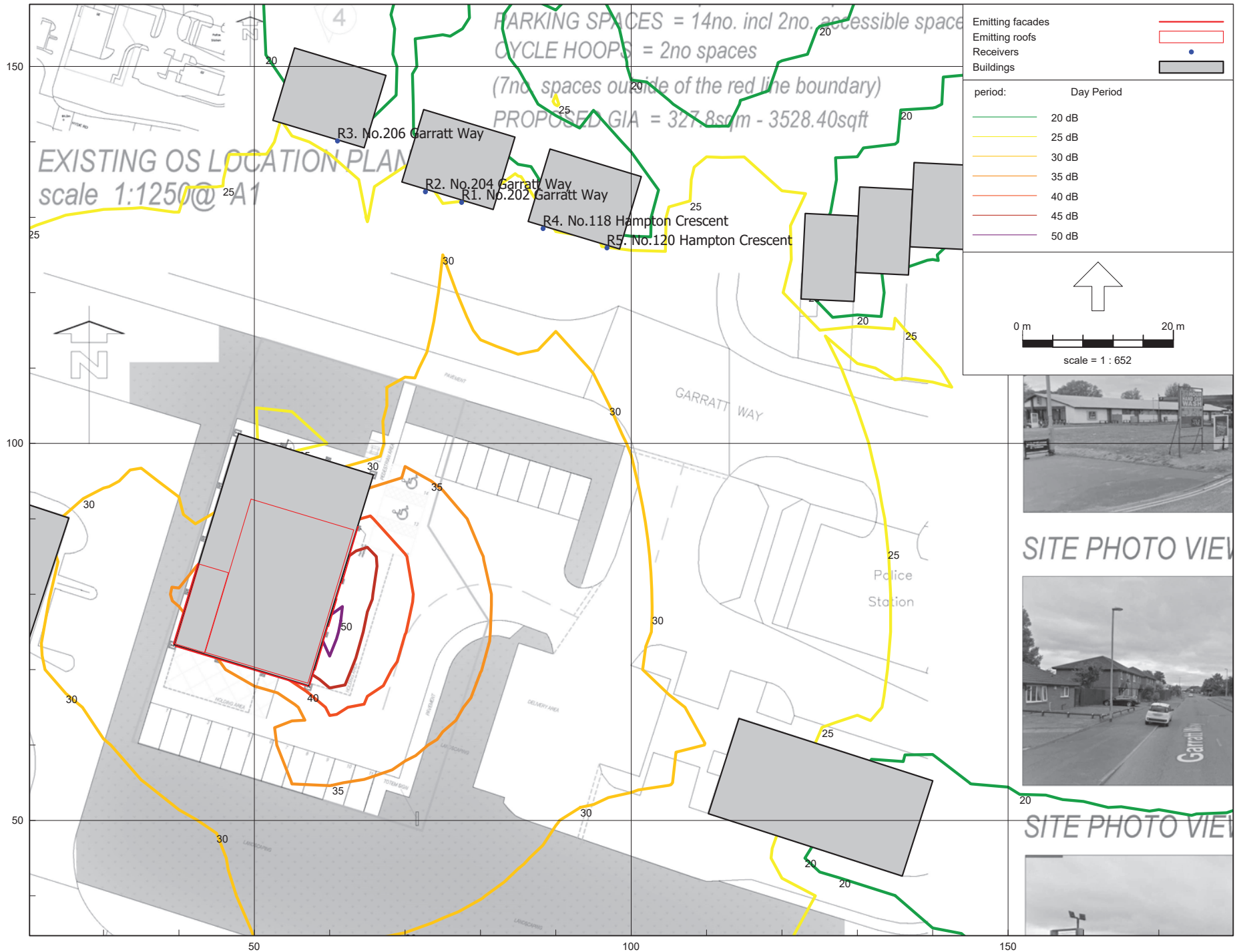
Report: Table of Results
Model: Closed Doors
LAeq per octave: total results for receivers
Group: (main group)
Group Reduction: No

Name		Height	Day									
Receiver	Description		Total	63	125	250	500	1000	2000	4000	8000	
_A	R1. No.202 Garratt Way	1.50	27	12	11	17	21	23	21	13	--	
_A	R2. No.204 Garratt Way	1.50	24	10	8	15	18	20	17	8	--	
_A	R3. No.206 Garratt Way	1.50	24	9	7	15	18	20	16	8	--	
_A	R4. No.118 Hampton Crescent	1.50	27	12	10	16	21	23	21	13	--	
_A	R5. No.120 Hampton Crescent	1.50	27	11	10	16	20	22	21	13	--	

All shown dB values are A-weighted

Predictor V2019.3

04/03/2020 19:35:21



Quick Lane, Gorton

Predicted Noise Levels - Roller Shutter Doors Open

Report: Table of Results
Model: Open Doors
LAeq per octave: total results for receivers
Group: (main group)
Group Reduction: No

Name		Height	Day								
Receiver	Description		Total	63	125	250	500	1000	2000	4000	8000
_A	R1. No.202 Garratt Way	1.50	46	22	26	31	37	41	43	36	23
_A	R2. No.204 Garratt Way	1.50	27	14	13	19	21	22	20	13	--
_A	R3. No.206 Garratt Way	1.50	26	12	12	17	20	21	20	12	--
_A	R4. No.118 Hampton Crescent	1.50	46	21	25	31	37	41	43	36	23
_A	R4. No.120 Hampton Crescent	1.50	46	21	25	30	37	41	42	36	22

All shown dB values are A-weighted

Predictor V2019.3

04/03/2020 19:42:31



Head Office

Spectrum Acoustic Consultants Ltd
27-29 High Street
Biggleswade
Bedfordshire
SG18 0JE
UNITED KINGDOM

 +44 (0)1767 318871

 enquiries@spectrumacoustic.com

 www.spectrumacoustic.com