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ENVIRONMENTAL NOISE ASSESSMENT

72 Errwood Road, Burnage
Manchester M19 2QH

Client:
Mr Dharmesh Naisuria

Report Date: 23rd September 2020

Ref: 20200923 8893 Burnage ProPG.docx

Site Visit by: M A Kenyon

Site Visit date: 18th & 21st September 2020

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1.0 INTRODUCTION

At the request of Messrs Howard & Seddon, acting on behalf of the client, Martec Environmental Consultants Ltd. undertook an assessment of the environmental noise impact of road traffic and commercial/leisure uses, on a residential development at 72 Errwood Road, Burnage, Manchester M19 2QH in connection with compliance with the planning consent conditions for the development.

This report considers the conditions attached to the consent, the requirements of current government guidance, measurements of noise made on this site, assesses the likely noise impact on the proposed dwellings, and makes recommendations for noise mitigation as necessary. Acoustic Terminology is set out at Appendix 1, the consultants' qualifications are at Appendix 2, and References at Appendix 3 with measurement results at Appendix 4.

2.0 PROJECT BACKGROUND

2.1 General

No.72 Errwood Road is a large detached dwelling at the corner of Errwood and Crompton Roads [See Figure 1 below]; Errwood carries a significant volume of road traffic whereas Crompton is a quiet residential street.

Planning consent has been granted to build three new properties in the grounds of the existing property [See Figure 1 for existing site plan and Figure 2 for proposed].

Condition 9 of Manchester City Council consent [124282/FO/2019] states:

“Before the development commences a scheme for acoustically insulating the proposed residential accommodation against noise from Errwood Road and other nearby noise sources shall be submitted to and approved in writing by the City Council as local planning authority. There may be other actual or potential sources of noise which require consideration on or near the site, including any local commercial/industrial premises. The approved noise insulation scheme shall be completed before any of the dwelling units are occupied.

Upon completion of the development and before first occupation of the residential units, a verification report will be required to validate that the work undertaken throughout the development conforms to the recommendations and requirements in the approved acoustic consultant's report. The report shall also undertake post completion testing to confirm that the internal noise criteria has been met. Any instances of non-conformity with the recommendations in the report shall be detailed along with any measures required to ensure compliance with the internal noise criteria.

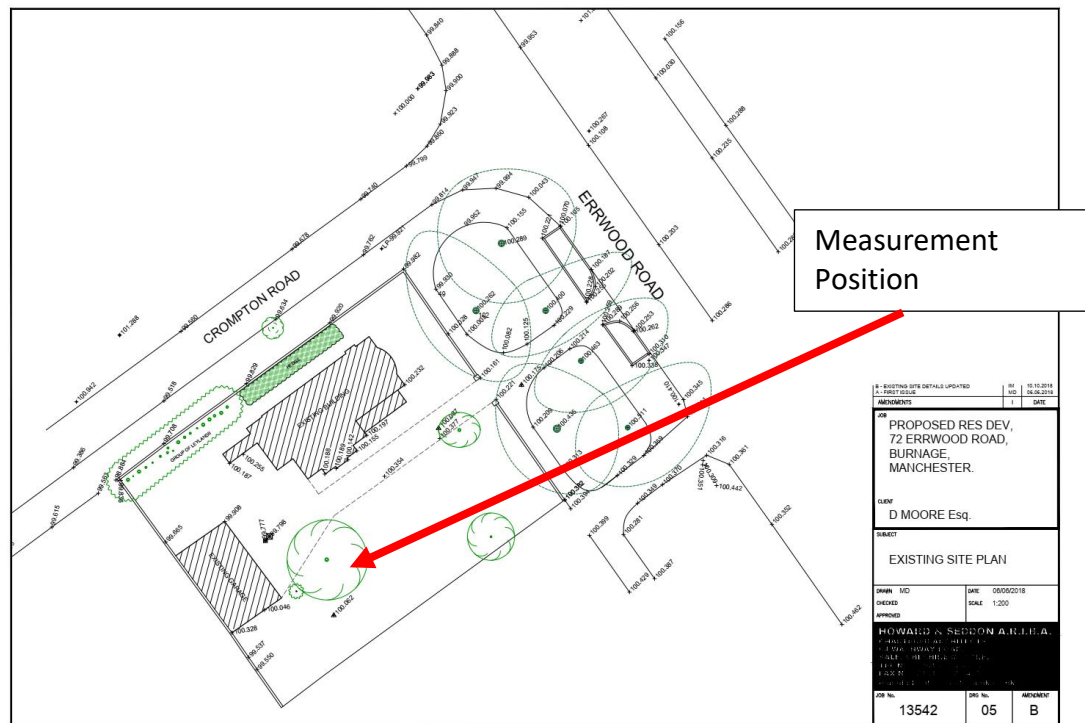
Reason: To secure a reduction in noise from traffic or other sources in order to protect future residents from noise disturbance, pursuant to policies SP1 and DM1 of the Core Strategy for the City of Manchester and saved policy DC26 of the Unitary Development Plan.”

Given that the noise condition applies only to “the proposed residential accommodation” it can be seen that it does not apply to the existing dwelling [No.72].

In addition, because the gardens of the proposed dwellings are existing residential gardens [of No.72] it has been assumed that external noise criteria should not be applied to the ‘new’ gardens; indeed the post completion validation testing refers solely to the internal noise criteria.

2.2 Coronavirus

The measurements in this study were made during the period of coronavirus restrictions. Latest government information only provides information on national traffic flows and does not break down the data any more than this; however, the government data indicates that road traffic flows are back to pre-covid levels. The effect on other noise sources is unclear.



3.0 ASSESSMENT CRITERIA

3.1 ProPG: Planning & Noise

Internal Noise Levels

The ProPG's target noise levels are broadly as set out in BS8233:2014 [see Table 1 below] with additional guidance on nighttime noise events based on World Health Organisation advice.

Activity	Location	07:00 to 23:00	23:00 to 07:00
Resting	Living Room	35 LAeq,16hr	--
Dining	Dining Room/Area	40 LAeq,16hr	--
Sleeping (daytime resting)	Bedroom	35 LAeq,16hr	30 LAeq,8hr 45 L _{Amax} ,F [1]

Table 1: ProPG - Target Internal Noise Levels

[1] Added from WHO and applies to 10th highest nighttime event.

The footnotes to this table make it clear that the guidance is based on the current WHO recommendations and that the above internal levels can be relaxed by 5dB to achieve "reasonable" internal conditions. The footnotes also make it clear that planning consent can be granted when external levels exceed the WHO guidance targets provided that appropriate internal noise levels are achieved.

The ProPG makes it clear that, where possible, the target internal noise levels in Table 2, should be achieved with windows open.

Following on from the above, the question then arises as to what attenuation should be assumed for an open window. Section 2.33 of the ProPG states

“It should be noted that the acoustic performance of the building envelope will be reduced in the event windows are opened for ventilation or cooling purposes, typically reducing the insulation to no more than 10 to 15 dB(A).”

In addition, it will be recalled that the ProPG states that if nighttime **external** noise events are 60 L_{Amax,F} or less, then there is negligible risk of noise and no adverse **effect**; given that the corresponding **internal** target noise level is 45 L_{Amax,F}, it can be seen that the ProPG is assuming that the difference between external and internal levels, i.e. the attenuation of a façade with an open window, is 15 dBA [60-45=15].

In addition to the above, the Defra research report NANR116 tested a variety of open windows and concluded that the difference between external and internal road traffic noise levels, ranged from 12 dBA [wide open outward opening side-hung casement] to 18 dBA [top hung opening light of single casement window]. The distribution of performance from NANR116 is as shown in Chart 1.

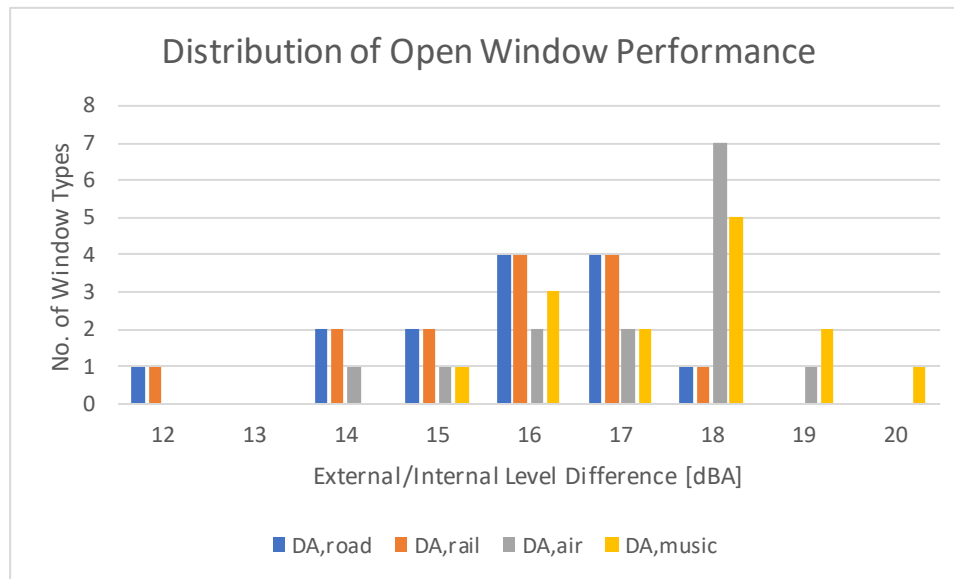


Chart 1: NANR116 test data

Given the above, for road traffic noise it is considered reasonable to assume a “global” figure of 15 dBA as the difference between external and internal levels for a façade with an open window.

NANR116 also reports details of research carried out by Ford and Kerry who found that secondary glazing with staggered openings permits through “fresh air” ventilation and *“It was concluded that, in general, open double windows are about 10 dBA better than open single windows.”* The ProPG refers to this window type as “plenum” windows. Therefore, it is considered reasonable to assume a “global” figure of 25 dBA as the difference between external and road traffic noise internal levels for a façade with an open “plenum” window.

Should it not be possible to meet the internal noise targets with openable windows, the ProPG sets out a variety of options that should be considered in an endeavour to avoid the need for windows to be closed, but if this is the only reasonable method by which the internal noise targets can be met, the ProPG requires that the approach should be justified and

“Where the local authority accepts that there is a justification that the internal target noise levels can only practically be achieved with windows closed, which may be the case in urban areas and at sites adjacent to transportation noise sources, special care may be taken to design the accommodation...”

If closed glazing is required to achieve suitable internal noise targets, some local authorities require the glazing to be sealed; however, the ProPG explicitly states at Sn.2.22:

“Using fixed unopenable glazing for sound insulation purposes is generally unsatisfactory and should be avoided;”

Consequently, the ProPG confirms that windows should not be sealed.

External Noise Levels

Section 3(ii) of the ProPG states:

“The acoustic environment of external amenity areas that are an intrinsic part of the overall design should always be assessed and noise levels should ideally not be above the range 50 – 55 dB $L_{Aeq,16hr}$.”

And at Section 2.49

“Developers are particularly encouraged to enter into pre-application discussions with the LPA where noise levels in proposed amenity spaces are likely to be above 55 dB $L_{Aeq,16hr}$ ”

Therefore, noise levels up to 55 dB $L_{Aeq,16hr}$ in external amenity areas are within the “ideal” range. It is only when levels in these areas exceed 55 $L_{Aeq,16hr}$ that the ProPG recommends other methods to avoid significant adverse impact discussions with the LPA.

The wording of the ProPG [and BS8233] make it clear that the guideline noise levels for gardens, patios, larger balconies etc., are not overriding planning considerations in any event.

4.0 MEASUREMENTS

The noise measurements were made with the microphone of the sound level meter [See Table 1 below] mounted on a pole approximately 1.4m above local ground height and fitted with a RION WS02 'all-weather' windmuff. The instrumentation calibrated correctly before and after measurements and had been laboratory calibrated in the preceding two years. The meter was located in free-field conditions in the location shown in Figure 1 above.

Model	Instrument	Serial No.	Lab Cal Certificate	Re-Calibration Due
C Svan 957	Sound Level Meter	23201	14012420-3	21/03/2021
Svan SV12L	Preamp	24265	14012420-3	21/03/2021
PCB 377B02	Microphone	LW136090	14012420-3	21/03/2021
RION NC74	Calibrator	34262041	14014839-4	20/02/2022

Table 1: Instrumentation used on site

During the survey, road traffic noise was dominant with occasional noise audible from the school grounds.

The meter re-set itself daily, between 13:15 and 13:30hrs, to permit simultaneous recordings of the noise to be made. It is not considered that these 'missing' periods would significantly alter the conclusions of the assessment.

The weather conditions during the survey were dry with generally lower wind speeds and are not considered likely to have significantly influenced the measurements.

5.0 RESULTS

5.1 Noise Results - Measurements

The full measurement results appear at Appendix 4 at the rear of the report. The results can be analysed to produce daytime and nighttime period results, shown in Table 2 below. The façade measurements have been converted to free-field results

Period		Measured Levels			Derived Traffic	
Day	Date	Day LAeq,16hr	Night LAeq,8hr	Day LA10,18hr	Day LAeq,16hr	Night LAeq,8hr
Fri	18-Sep	50.6	42.9	52.8	51.0	43.8
Sat	19-Sep	49.5	42.7	51.0	49.3	42.2
Sun	20-Sep	48.5	42.8	49.5	47.8	40.8
Mon	21-Sep	51.8	--	52.8	51.0	--

Table 2: Summary Results [dBA free field]

The LA10 measurements in the fifth column ['Day LA10,18hr'] have been converted to daytime [column 6] and nighttime [column 7] LAeq,T levels on the assumption that they were produced by road traffic noise [using Reference 4]. It can be seen that there is good correlation between the derived and actual LAeq,T levels for both daytime and nighttime, indicating that road traffic noise was indeed the dominant noise source at the measurement position. This confirms the observer's subjective opinion that road traffic noise was the dominant source.

The LAFmax,1s readings, for the first [loudest] night of monitoring, have been plotted in Appendix 4. The 10th highest reading was 58.6 LAFmax,F.

It should be noted that from listening to the recordings made by the meter, a bird was singing close to the microphone at 6:20am; these results have been removed from the analysis; hence the gap in the trace in Appendix 4.

Finally, Table 3 below is the logarithmic average of the spectra measured on site.

Octave Band Centre Freq. [Hz]				
125	250	500	1000	2000
51.4	44.6	43.2	44.6	40.3

Table 3: Log Average Spectrum

5.2 Noise Results - Predictions

From Table 2 above it is considered reasonable to assume levels of 51.8 and 42.9 LAeq,T for daytime and nighttime levels respectively; however, the monitoring position was some 43m from the roadside edge of Errwood Road, whereas the nearest 'new' façade would be some 22m away; consequently it is necessary to predict levels at the nearest facade which has been done, using the procedures of reference 3, in Table 4 below.

CRTN Calcs © Martec Version 1.6	Meas	Plot 4 GF	Plot 4 FF	Meas GF LAmax	Plot 4 FF LAmax
Road Segments	Errwood	Errwood	Errwood	Errwood	Errwood
Basic Noise Level of Road	63.7	63.7	63.7	75.9	75.9
Ht of C'way AoD	1	1	1	1	1
Angle of View	120	180	180	120	180
Ht of Ground at Receiver AoD	1	1	1	1	1
Ht of Receiver Abv local grnd	1.5	1.5	4	1.5	4
Dist of Receiver from C'way Edge	43	22	22	43	22
Proportion of Soft Ground	0.9	0.8	0.8	0.9	0.8
Height of Propagation Path	1	1	2.25	1	2.25
Total Barrier Attenuation	0.0	0.0	0.0	0.0	0.0
Soft Ground Attenuation	-4.7	-3.1	-1.4	-4.7	-1.4
Net Barrier Effect	0.0	0.0	0.0	0.0	0.0
Distance Attenuation	-5.4	-2.8	-2.8	-10.7	-5.6
Angle of View Correction	-1.8	0.0	0.0	-1.8	0.0
Reflection Correction	0.0	0.0	0.0	0.0	0.0
Total Attenuation	-11.9	-5.9	-4.2	-17.3	-7.0
Segment Level	51.8	57.8	59.5	58.6	68.9
Total Level	51.8	57.8	59.5	58.6	68.9

Table 4: Predicted Noise Levels [free-field]

From Table 4, the levels at the façade of the new property would be say 58 and 60 LAeq,16hr at ground and first floor levels respectively, and the LAmax level, where the bedrooms are proposed to be located, would be 68.9 LAmax,F.

6.0 ASSESSMENT

It is possible to conduct approximate predictions to determine if the criteria can be met with open glazing as shown in Table 5 below.

Condition	Day LAeq,16hr	Night LAeq,8hr	Night LAmax,F
External Level	58.6	49.7	68.9
Open Windows		-15	
Internal Level	43.6	34.7	53.9
Criteria	35	30	45
Exceedance	8.6	4.7	8.9
Criteria Met?	No	No	No

Table 5: Indicative External [free-field] & Internal Levels [dBA]

From Table 5 it can be seen that none of the criteria would be met with windows open; therefore, it will not be possible to rely on open glazing for general ventilation because this would lead to the noise criteria being breached. Consequently, it will be necessary to provide alternative [mechanical] ventilation. NB. Rapid/purge ventilation would be by means of opening the windows, temporarily, and therefore, the windows should not be fixed shut but need to be openable as required.

Using the proposed room and window dimensions shown in the approved Architect's drawings, the external levels above can be used to derive internal noise levels using the methodology described in BS EN 12354-3:2000 [Ref 5].

The following matters have been assumed:

- The reverberation time of a Bedroom is 0.3 seconds and for other habitable rooms 0.5 seconds.
- The rooms would be provided with a form of ventilation

system that does not require vents.

- The walls are [or have the same performance as] standard cavity masonry.
- The typical worst-case window area and room dimensions have been used, i.e. small room with large window.

BS EN 12354-Calcs		Use	Volume	18.5				
Version	4.3	length				Building Atten dBA (59.5 - 26.3)		
© 2018 Martec Environmental Consultants Ltd		width	RT	0.3				
& Acute Acoustics Ltd		height	Octave Band Centre Frequency [Hz]				dBA	
			125	250	500	1k	2k	
External Spectrum Leq (Free Field & Lin)			51.4	44.6	43.2	44.6	40.3	
Adjustment to Given Level if required							47.8	
External Spectrum Adjusted for Level							59.5	
			63.1	56.3	54.9	56.3	52.0	
							59.5	
Wall		Area m2	Element Sound Reduction Index [SRI]					Contrib
BS8233 Brick & Block External Wall		14.3	40	44	45	51	56	
Drs/Wndws								
4 (20) 6		4.2	24	28	31	43	39	
Roof Lights								
None		0.0	0	0	0	0	0	
Door								
None		0.0	0	0	0	0	0	
Roof								
None		0.0	0	0	0	0	0	
Vent Dn,e		# Vents						
None		0.0	0	0	0	0	0	
								dBA
		Internal SPL/dBLin	38.7	27.9	23.7	14.4	12.5	
								26

Similar predictions can be performed for the ground floor Lounge in Plot 4 [See Table 7 below]:

BS EN 12354-Calcs		Use	Volume	53.5				
Version	4.3	length						
© 2018 Martec Environmental Consultants Ltd		width						
& Acute Acoustics Ltd		height						
			RT	0.5				
			Octave Band Centre Frequency [Hz]					dBA
				125	250	500	1k	2k
External Spectrum Leq (Free Field & Lin)				51.4	44.6	43.2	44.6	40.3
Adjustment to Given Level if required								
External Spectrum Adjusted for Level				61.4	54.6	53.2	54.6	50.3
								47.8
								57.8
								57.8
Wall		Area m2	Element Sound Reduction Index [SRI]					Contrib
BS8233 Brick & Block External Wall		14.3	40	44	45	51	56	12.5
Drs/Wndws								
4 (20) 6		4.2	24	28	31	43	39	21.8
Roof Lights								
None		0.0	0	0	0	0	0	0.0
Door								
None		0.0	0	0	0	0	0	0.0
Roof								
None		0.0	0	0	0	0	0	0.0
Vent Dn,e		# Vents						
None		0.0	0	0	0	0	0	0.0
								dBA
			Internal SPL/dBLin	34.6	23.8	19.6	10.3	8.4
								22

Table 7: Internal Levels – Plot 4 Lounge – Road Traffic Noise - Day

Table 7 demonstrates that the predicted internal daytime traffic noise levels of 22 LAeq,16hr would conform with the ProPG recommendations of 35 LAeq,16hr for daytime resting.

7.0 DISCUSSION, CONCLUSIONS AND RECOMMENDATIONS

The measurements and the observer's subjective impressions indicate that road traffic noise is the dominant noise source affecting the site.

The predictions above indicate that for the most affected Plot [No.4] it

is possible to meet the requirements of appropriate guidance. The required minimum performance levels of the glazing to be provided to the front façade of all properties is as shown in Table 8 below. The rooms should not be fitted with vents.

Element	Unit	Octave Band Centre Frequency [Hz]				
		125	250	500	1k	2k
Windows	SRI	24	28	31	43	39

Table 8: Required Element Performance [SRI dB]

All properties should be provided with powered ventilation systems. It is understood that both of the following systems conform to the ANC ‘Acoustics Ventilation and Overheating residential Design Guide – January 2020”:

- a. An EnviroVent Positive Input Ventilation (PIV) system. We understand that with the proposed ventilation system there is no requirement for ventilation grilles in the facades of living rooms, dining rooms or bedrooms.
- b. A Nuaire MEV Ecosmart Continuous Mechanical Extract Ventilation Unit system. We understand that with the proposed ventilation system, whilst the ductwork is ducted directly to grilles in the building façade, there is no requirement for ventilation grilles in the facades of living rooms, dining rooms or bedrooms.

Rapid or purge ventilation will be provided via openable windows at the occupants' discretion. As such, the internal daytime and night-time noise criteria may potentially be exceeded during rapid/purge ventilation conditions.

The above package of measures should ensure compliance with the first part of Condition No.9.

In relation to the post construction validation tests, it is considered that this should be by means of measuring the building's [Plot 4] façade sound insulation capabilities as per BS EN ISO 16283-3:2016, and thereby confirming that the building is capable of reducing the previously measured levels so as to meet the internal noise criteria. The tests would be conducted in one of the living rooms and in one of the bedrooms.

APPENDIX 1

EXPLANATION OF ACOUSTIC TERMS

The dB or the decibel, is the unit of noise. The number of decibels or the level, is measured using a sound level meter. It is common for the sound level meter to filter or 'weight' the incoming sound so as to mimic the frequency response of the human ear. Such measurements are designated **dB(A)**.

A doubling of the sound is perceived, by most people, when the level has increased by 10 dB(A). The least discernible difference is 2 dB(A). Thus, most people cannot distinguish between, say 30 and 31 dB(A).

The Background level of noise is most commonly represented by the level which is exceeded for 90% of the time i.e. the LA90.

If a noise varies over time then the **equivalent continuous level, or LAeq**, is the notional constant level of noise which would contain the same amount of acoustic energy as the time varying noise.

The following table gives an approximate indication of the comparative loudness of various noises expressed in terms of the A weighted scale:

Source of noise	dB(A)	Nature of Noise
Inside Quiet bedroom at night	25-30	Very Quiet
Quiet office	40-45	
Rural background noise	35-45	
Normal conversational level	55-65	
Busy restaurant	65-75	
Inside suburban electric train	70-80	
Hand clap @ 1m	75-85	
HGV accelerating @ 5m away	85-90	Very Loud

APPENDIX 2

QUALIFICATIONS AND EXPERIENCE OF M.A. KENYON

My full name is Melville Alexander Kenyon. I am the principal of the firm of Martec Environmental Consultants Ltd, a consultancy company that specialises in environmental noise assessment and control. I graduated in 1982 with a Bachelor's degree in Engineering and subsequently a Master's degree in Environmental Acoustics. I have been a corporate member of the professional body for noise and vibration specialists, the Institute of Acoustics, since 1988, and have sat on the British Standards Committee dealing with noise in buildings [BS.8233:1999].

I have lectured at Liverpool John Moores University on the Diploma of Acoustics course and at Manchester Metropolitan University on their Environmental Health degree course.

The firm of Martec Environmental Engineering was formed in the 1970's and joined The Association of Noise Consultants in 1996. The company is now known as Martec Environmental Consultants Ltd.

Since its formation, Martec has advised many groups of both residents and developers about the problems of noise and vibration in the environment.

APPENDIX 3

REFERENCES

- 1 ProPG 24: Planning and Noise. – IoA, CIEH, ANC - June 2017
- 2 BS.8233:2014 “Guidance on Sound Insulation and noise reduction for buildings.”
- 3 Calculation of Road Traffic Noise (CRTN) – Department of Transport and the Welsh Office, HMSO, 1988, ISBN 0-11-550847-3
- 4 Method for Converting the UK Road Traffic Noise Index $L_{A10,18h}$ to the EU Noise Indices for Road Noise Mapping – TRL/Cassella Stanger
http://www.defra.gov.uk/environment/quality/noise/research/crt_n/documents/noise-crtn-update2006.pdf
- 5 BS EN 12354-3:2000 *Building Acoustics-Estimation of Acoustic Performance in buildings from the performance of elements. Part 3 Airborne Sound Insulation against Outdoor Sound.*
- 6 The Department of Transport “*Calculation of Railway Noise 1995*” - HMSO
- 7 BS4142:2014 “Methods for rating and assessing industrial and commercial sound”
- 8 “Design Manual for Roads and Bridges HD 213/11 Volume 11, Section 3, Part 7, Revision 1” - The Highways Agency November 2011.

APPENDIX 4**Noise Measurements [dBA free-field]**

Date & time	Duration	LAmx,F	LAmin	LAeq	L01	L10	L50	L90
18/09/2020 12:45:30	00:15:00	63.8	40.8	50.1	58.2	53.4	48	43.6
18/09/2020 13:00:30	00:15:00	65.3	41.7	49.6	56.5	52.4	48	44.1
18/09/2020 13:15:30	00:15:00	65.6	42	50.2	58	53	48.2	44.6
18/09/2020 13:45:24	00:15:00	65.6	43	51.2	60.1	53.7	49.1	45.9
18/09/2020 14:00:24	00:15:00	63.5	42.2	50.4	57.1	53	49.1	45.1
18/09/2020 14:15:24	00:15:00	64.1	41.9	49.3	55.6	52.3	47.9	44.4
18/09/2020 14:30:24	00:15:00	64.1	42.4	49.5	55.2	52.1	48.6	45.3
18/09/2020 14:45:24	00:15:00	62.7	42.2	49.6	56.9	51.8	48.4	45.5
18/09/2020 15:00:24	00:15:00	73.8	44.3	56.5	70.1	56.6	50.4	47.1
18/09/2020 15:15:24	00:15:00	68.3	42.6	51.3	59.2	53.6	49.9	46.6
18/09/2020 15:30:24	00:15:00	66	43.8	52.2	58	54.6	51.4	47.7
18/09/2020 15:45:24	00:15:00	67.5	42.1	51.3	57.2	53.7	50.5	46.5
18/09/2020 16:00:24	00:15:00	71.2	41.6	52	61.1	54.4	50	45.4
18/09/2020 16:15:24	00:15:00	64.3	42.6	52.2	57.1	54.6	51.6	47.1
18/09/2020 16:30:24	00:15:00	69.1	43	53.5	58.9	56.7	51.9	46.3
18/09/2020 16:45:24	00:15:00	65.9	41.8	50.3	56.3	53.1	49.1	45
18/09/2020 17:00:24	00:15:00	68.3	43.6	51.4	57.6	53.9	50.4	46.8
18/09/2020 17:15:24	00:15:00	67.8	42.7	51.5	57.5	53.8	50.2	46.1
18/09/2020 17:30:24	00:15:00	60.6	41.8	50.1	56.2	52.9	49.1	45.3
18/09/2020 17:45:24	00:15:00	68.5	44.6	52	57.8	54.6	51.1	47.4
18/09/2020 18:00:24	00:15:00	60.3	43.7	51.1	56.8	53.9	50.1	46.2
18/09/2020 18:15:24	00:15:00	65.6	43	50.3	55.9	52.9	49.2	46.2
18/09/2020 18:30:24	00:15:00	67.2	41.9	49.4	55	52.2	48.3	44.7
18/09/2020 18:45:24	00:15:00	62.2	41.2	49.9	55.9	52.7	48.5	44.7
18/09/2020 19:00:24	00:15:00	65.1	42	50.6	56.5	53.4	49.5	45.8
18/09/2020 19:15:24	00:15:00	62.6	41.1	49	55.8	52	47.5	43.8
18/09/2020 19:30:24	00:15:00	64.6	40.9	50	57.7	52.8	47.9	44
18/09/2020 19:45:24	00:15:00	64.9	41	50.1	59.4	53.1	47.2	43.6
18/09/2020 20:00:24	00:15:00	63.4	40.7	49.6	56.3	52.5	48.2	44.5
18/09/2020 20:15:24	00:15:00	66.8	41.1	49.5	57.9	52.3	47.1	43.6
18/09/2020 20:30:24	00:15:00	60.1	40.6	49.2	56.6	52.4	47.3	43.8
18/09/2020 20:45:24	00:15:00	64.8	40.1	49.4	57.1	52.2	47.5	43.4
18/09/2020 21:00:24	00:15:00	62.1	40	48.2	55.8	51.4	45.9	42.4
18/09/2020 21:15:24	00:15:00	65.6	40.4	48.8	56.9	51.3	46.7	42.8
18/09/2020 21:30:24	00:15:00	67.6	39.6	48.9	58.2	51.6	46.2	42.6
18/09/2020 21:45:24	00:15:00	64.2	41	48.4	54.7	51.4	46.9	43.4
18/09/2020 22:00:24	00:15:00	59.8	40.2	47.7	54.4	51.3	45.6	42.5
18/09/2020 22:15:24	00:15:00	75.1	38.1	51.5	61.2	52.6	46.4	41.6
18/09/2020 22:30:24	00:15:00	60.4	38.3	46.8	56.2	50.4	43	40.1
18/09/2020 22:45:24	00:15:00	60.6	37.7	46.3	55	50.3	42.8	40
18/09/2020 23:00:24	00:15:00	61.3	37.4	45.5	54	49.3	41.9	39.4

18/09/2020 23:15:24	00:15:00	56.9	37.4	44.5	52.3	48	42	39.3
18/09/2020 23:30:24	00:15:00	56.6	36.3	45.1	53.7	48.7	42	38.6
18/09/2020 23:45:24	00:15:00	64.2	36.5	43.8	52.9	46.6	40.3	38
19/09/2020 00:00:24	00:15:00	58.1	35.4	42.9	52.6	45.7	39.5	37.2
19/09/2020 00:15:24	00:15:00	55.7	34.4	42.1	51.5	45.5	38.8	36.9
19/09/2020 00:30:24	00:15:00	55.3	35.2	43.8	52.9	48	39.3	37.2
19/09/2020 00:45:24	00:15:00	58.6	34.7	41.8	51.6	44.7	38.3	36.3
19/09/2020 01:00:24	00:15:00	57.5	34.1	42.6	53.5	45.4	38.5	36.4
19/09/2020 01:15:24	00:15:00	57.1	35	40.5	49.8	41.8	38.6	36.7
19/09/2020 01:30:24	00:15:00	61.3	34.3	42.9	52.6	44.5	39.1	37.1
19/09/2020 01:45:24	00:15:00	52.7	33.9	39.9	49.4	41.3	38.1	36.3
19/09/2020 02:00:24	00:15:00	53.4	35.4	40.6	48.8	42.8	38.9	37.1
19/09/2020 02:15:24	00:15:00	53.5	34.1	40.4	49	42.8	38.5	36.4
19/09/2020 02:30:24	00:15:00	56.3	34.2	40.8	52.7	40.9	37.8	35.9
19/09/2020 02:45:24	00:15:00	53.8	34.3	40.6	49.5	42.7	38.6	36.3
19/09/2020 03:00:24	00:15:00	56.4	33.8	41.3	48.9	44.2	39	36.6
19/09/2020 03:15:24	00:15:00	54.2	35.4	42.5	51.2	45.6	40.1	37.3
19/09/2020 03:30:24	00:15:00	50.1	34.5	39.7	46.3	41.4	39.1	36.9
19/09/2020 03:45:24	00:15:00	57.7	36.8	41.1	48.6	42.6	40	38.2
19/09/2020 04:00:24	00:15:00	52.3	37.8	42.5	49.2	44.3	41.6	39.8
19/09/2020 04:15:24	00:15:00	55.1	34.8	41.6	50.2	44.1	39.7	37.2
19/09/2020 04:30:24	00:15:00	56.3	34	40.4	50.2	41.4	38.4	36.3
19/09/2020 04:45:24	00:15:00	51.5	33.6	40.2	48.6	41.9	38.6	36.7
19/09/2020 05:00:24	00:15:00	50.9	34.2	39	47.3	40.7	37.8	36
19/09/2020 05:15:24	00:15:00	48.9	33.3	38.4	43.5	40.5	37.7	35.7
19/09/2020 05:30:24	00:15:00	56.4	34.8	43.7	53.7	46.2	40.7	37.7
19/09/2020 05:45:24	00:15:00	55.3	35.2	41.9	50.1	44.5	40	38
19/09/2020 06:00:24	00:15:00	53.9	36.2	43	51.3	45.7	41.2	38.2
19/09/2020 06:15:24	00:15:00	63.8	36	43.7	52.6	45.4	41	37.9
19/09/2020 06:30:24	00:15:00	67.9	36.3	50	62.8	51.4	42.9	39.3
19/09/2020 06:45:24	00:15:00	59.9	37.1	45.2	53.9	48.8	42	39.3
19/09/2020 07:00:24	00:15:00	59.4	36.4	44.7	54.8	47.7	41.2	39
19/09/2020 07:15:24	00:15:00	62.1	36.3	46.6	56.6	50.5	42	38.2
19/09/2020 07:30:24	00:15:00	69	37.2	47.2	56.4	50.1	42.7	39.4
19/09/2020 07:45:24	00:15:00	60.2	37.2	46.7	56.7	50.2	43.1	40.2
19/09/2020 08:00:24	00:15:00	62.5	38.2	47.6	57.4	50.8	43.6	40.1
19/09/2020 08:15:24	00:15:00	60.7	38.3	46.5	54.9	50.4	43.1	40.3
19/09/2020 08:30:24	00:15:00	59	37.5	46.2	54.5	50.2	42.5	39.5
19/09/2020 08:45:24	00:15:00	69.1	37.2	48.6	57.3	51	43.9	40.1
19/09/2020 09:00:24	00:15:00	68.2	39.1	49.9	59.3	52.4	46.8	42.1
19/09/2020 09:15:24	00:15:00	65.4	39.7	50.1	59	52.9	47.7	43.3
19/09/2020 09:30:24	00:15:00	64.5	39.3	48.5	56.9	51.6	46.2	42.1
19/09/2020 09:45:24	00:15:00	70.3	39.2	51.4	63.7	52.7	46.6	42.1
19/09/2020 10:00:24	00:15:00	64.2	40.7	50.8	59.7	53.5	48.3	44.5
19/09/2020 10:15:24	00:15:00	67.4	41.9	50.3	57.9	52.8	48.4	45.2
19/09/2020 10:30:24	00:15:00	70.5	41.9	50.7	58.8	53.1	48.6	45.1

19/09/2020 10:45:24	00:15:00	66.9	42.4	51.4	62.4	53.4	48.9	45.2
19/09/2020 11:00:24	00:15:00	68.3	42	51.3	57.8	53.5	50.2	47.1
19/09/2020 11:15:24	00:15:00	69.8	43.5	51.2	58	53.4	50.1	46.8
19/09/2020 11:30:24	00:15:00	74.7	41.2	50.1	55.5	52.4	48.5	44.5
19/09/2020 11:45:24	00:15:00	62.1	42.3	49.5	56.1	52	48.3	44.9
19/09/2020 12:00:24	00:15:00	64.9	40.7	51.3	59.1	54.1	49.4	45.8
19/09/2020 12:15:24	00:15:00	74.5	43.7	51.4	58.5	52.8	48.6	45.5
19/09/2020 12:30:24	00:15:00	66.9	41.3	51.2	59.6	53.7	49.6	45.2
19/09/2020 12:45:24	00:15:00	65.3	41.1	49.6	56.4	52.3	47.8	44
19/09/2020 13:00:24	00:15:00	69.2	42.1	50.4	57	52.8	48.6	44.5
19/09/2020 13:15:24	00:15:00	67	41.8	50.4	57.6	52.9	48.8	45.2
19/09/2020 13:45:30	00:15:00	70.9	43.5	51.1	57.3	53	50	46.3
19/09/2020 14:00:30	00:15:00	65.8	43.6	50.8	57.5	53.3	49.5	46.3
19/09/2020 14:15:30	00:15:00	62.4	43.7	50.5	56.8	53.1	49.1	46.3
19/09/2020 14:30:30	00:15:00	62	43	50.3	56.6	52.7	49.3	46
19/09/2020 14:45:30	00:15:00	72.3	41.8	53.8	67	54.3	49.2	45.2
19/09/2020 15:00:30	00:15:00	62.8	43.5	50.1	56.2	52.7	49.1	46
19/09/2020 15:15:30	00:15:00	64.6	43.6	49.4	54.8	51.8	48.4	45.9
19/09/2020 15:30:30	00:15:00	64.8	42.6	50.1	56	53	48.9	45.6
19/09/2020 15:45:30	00:15:00	56.6	42	49	54.9	52.1	47.6	44.4
19/09/2020 16:00:30	00:15:00	71.9	42.9	51.3	60.7	53.3	48.9	45.7
19/09/2020 16:15:30	00:15:00	65	42.4	49.9	55.4	52.7	48.7	45.3
19/09/2020 16:30:30	00:15:00	66.8	43	50.9	59.1	53.2	49.1	45.8
19/09/2020 16:45:30	00:15:00	59.1	42.2	49.9	54.7	52.5	49.3	45.6
19/09/2020 17:00:30	00:15:00	61.6	42.9	50.2	56.4	53	48.8	45.7
19/09/2020 17:15:30	00:15:00	61.6	42.2	50	56.4	52.9	48.9	44.8
19/09/2020 17:30:30	00:15:00	61.5	44.4	51.2	56.4	53.8	50.3	47.4
19/09/2020 17:45:30	00:15:00	59	42.6	50.5	56.2	53.1	49.5	46.3
19/09/2020 18:00:30	00:15:00	61.5	43.1	50.7	56.8	53.4	49.7	46.2
19/09/2020 18:15:30	00:15:00	59.2	41.8	49	54.2	51.9	47.9	44.5
19/09/2020 18:30:30	00:15:00	60	41.4	49.1	56.4	52.2	47.3	43.4
19/09/2020 18:45:30	00:15:00	58.2	40.4	49	55.6	52.1	47.6	43.7
19/09/2020 19:00:30	00:15:00	57	40.1	48.1	54.2	51.2	46.8	42.8
19/09/2020 19:15:30	00:15:00	59.9	38.8	48	56.3	51.1	45.9	41.6
19/09/2020 19:30:30	00:15:00	67.4	39.2	50.4	60.5	53.1	46.8	42.2
19/09/2020 19:45:30	00:15:00	67.5	39.1	47.6	54.7	50.9	45.7	41.2
19/09/2020 20:00:30	00:15:00	64.5	38.5	47.9	56.2	50.9	45.3	40.4
19/09/2020 20:15:30	00:15:00	69.2	39.3	48.3	56.1	50.7	45.3	41.3
19/09/2020 20:30:30	00:15:00	57.7	37.6	46.2	54.7	49.7	43.5	40.1
19/09/2020 20:45:30	00:15:00	56.8	38	46.3	54.1	50.1	43.7	39.7
19/09/2020 21:00:30	00:15:00	59.1	37.5	46.5	53.7	50.3	44	40.1
19/09/2020 21:15:30	00:15:00	56.6	36.8	46.1	53.7	50.1	43.1	39.5
19/09/2020 21:30:30	00:15:00	68.4	37.5	49	60.6	51	43.2	39.8
19/09/2020 21:45:30	00:15:00	59.3	36.6	46.1	54.5	50	42.4	39.1
19/09/2020 22:00:30	00:15:00	57.9	37.8	45.9	53.5	49.6	43.3	39.7
19/09/2020 22:15:30	00:15:00	57.3	37.2	45.7	54	49.6	42.1	39.4

19/09/2020 22:30:30	00:15:00	60.6	37.7	46.7	55	50.4	43.7	40.3
19/09/2020 22:45:30	00:15:00	58	36.6	45.5	53.9	49.3	42.5	39.7
19/09/2020 23:00:30	00:15:00	59	37.8	46.2	53.7	49.9	43.5	40
19/09/2020 23:15:30	00:15:00	62.8	36.8	46	55.7	49	42.3	39.1
19/09/2020 23:30:30	00:15:00	55.4	35.9	43.2	51.9	46.9	40	37.9
19/09/2020 23:45:30	00:15:00	56.6	35.8	44.5	53.2	48.8	40.8	38
20/09/2020 00:00:30	00:15:00	58.6	35.3	44.2	52.7	48.3	40.5	37.8
20/09/2020 00:15:30	00:15:00	59.4	35.6	44.2	53.3	48	40.2	37.7
20/09/2020 00:30:30	00:15:00	57.4	35.2	43.5	53.7	46.9	39.5	37.1
20/09/2020 00:45:30	00:15:00	73	35	47	54.8	47.3	40.1	37.6
20/09/2020 01:00:30	00:15:00	54.7	34.6	41.8	51.9	44.6	38.7	36.4
20/09/2020 01:15:30	00:15:00	56.7	34.7	42.4	52.5	45.4	38.6	36.5
20/09/2020 01:30:30	00:15:00	54.2	33.8	40.9	50.3	44.3	37.5	35.5
20/09/2020 01:45:30	00:15:00	50.3	33.8	39.1	47.4	40.9	37.7	36
20/09/2020 02:00:30	00:15:00	52.6	34	39	48.2	40.5	37.4	35.6
20/09/2020 02:15:30	00:15:00	64	33.1	42.2	54.3	41.6	36.9	35.2
20/09/2020 02:30:30	00:15:00	52.2	32.6	38.3	48.6	38.9	36.2	34.5
20/09/2020 02:45:30	00:15:00	54.9	32.7	39.4	50.6	39.7	36.8	35.1
20/09/2020 03:00:30	00:15:00	63.7	33.6	41.2	49.2	40	37.4	35.3
20/09/2020 03:15:30	00:15:00	62.6	32.9	41.7	52.8	41.6	36.8	34.8
20/09/2020 03:30:30	00:15:00	51.7	32.7	38.5	48	40.4	36.4	34.6
20/09/2020 03:45:30	00:15:00	50.6	31.9	37.2	47.3	38.1	35.5	33.6
20/09/2020 04:00:30	00:15:00	53	31.5	36.9	47.4	37.6	35.2	33.4
20/09/2020 04:15:30	00:15:00	56.8	31.1	37.5	49.1	37.4	34.7	32.9
20/09/2020 04:30:30	00:15:00	51.7	30.2	36.1	45.5	37.3	34.5	32.2
20/09/2020 04:45:30	00:15:00	52.4	30.7	37	47.7	37.9	34.2	32.4
20/09/2020 05:00:30	00:15:00	48	30.8	35.3	44.2	36.4	34.2	32.4
20/09/2020 05:15:30	00:15:00	57	30.7	38.7	50.5	38.2	35.1	33.1
20/09/2020 05:30:30	00:15:00	52.1	31.2	37.7	47.9	39.1	35.7	33.6
20/09/2020 05:45:30	00:15:00	49.9	31.5	36.3	42.5	37.5	35.5	34
20/09/2020 06:00:30	00:15:00	55.9	31.9	39.2	49.1	40.5	36.5	34
20/09/2020 06:15:30	00:15:00	60.2	33.3	44.1	53.5	47.4	40.6	37.4
20/09/2020 06:30:30	00:15:00	74.6	34	49.3	62.6	45.7	38.7	36.2
20/09/2020 06:45:30	00:15:00	65	33.1	48	60.2	50.4	41	36.2
20/09/2020 07:00:30	00:15:00	67.9	34.3	45.1	55.3	48.6	39.3	36.2
20/09/2020 07:15:30	00:15:00	61.9	34.3	45.5	57.7	48.2	39.2	37
20/09/2020 07:30:30	00:15:00	62.6	34.4	45.5	57.5	48.2	39.9	37.1
20/09/2020 07:45:30	00:15:00	73	35.2	50.1	63.7	50	41.8	38.2
20/09/2020 08:00:30	00:15:00	75	36.1	49.6	61.8	51	40.1	37.7
20/09/2020 08:15:30	00:15:00	57.5	35.5	43.8	53.3	47.2	40.3	37.7
20/09/2020 08:30:30	00:15:00	62	35.7	45.5	55.2	48.9	41.2	38.1
20/09/2020 08:45:30	00:15:00	62.3	36.3	45.9	55.3	49.4	41.8	39.2
20/09/2020 09:00:30	00:15:00	60.7	36.3	45.2	53.8	48.9	41.6	38.3
20/09/2020 09:15:30	00:15:00	64.6	37.2	47.2	57.7	50.2	43	39.3
20/09/2020 09:30:30	00:15:00	67.7	38.9	49.3	59.4	51.9	45.7	41.6
20/09/2020 09:45:30	00:15:00	66.6	37.3	49	58.9	52.3	44.9	40.1

20/09/2020 10:00:30	00:15:00	64.5	39.9	47.5	55.6	50.5	45.2	42
20/09/2020 10:15:30	00:15:00	63.7	40.3	47.5	55.6	50.8	44.6	41.5
20/09/2020 10:30:30	00:15:00	58.2	38.4	47	54.3	50.4	44.9	41
20/09/2020 10:45:30	00:15:00	68.2	38.3	48.6	58.3	51	44.7	40.5
20/09/2020 11:00:30	00:15:00	80.1	41	50.8	58.2	52.1	47.3	43.4
20/09/2020 11:15:30	00:15:00	68.8	37.3	49.4	57	52.2	47.5	42.4
20/09/2020 11:30:30	00:15:00	62.3	38.2	47.7	55.4	50.9	45.5	41.2
20/09/2020 11:45:30	00:15:00	62.2	37.9	47.5	55.1	50.8	45.4	41
20/09/2020 12:00:30	00:15:00	60.5	37.3	48.3	55.8	51.6	46.6	41.3
20/09/2020 12:15:30	00:15:00	67	39.4	50.5	59.8	53.1	48	43.5
20/09/2020 12:30:30	00:15:00	65.4	40.2	50.4	58.8	53.2	48.5	43.5
20/09/2020 12:45:30	00:15:00	64.5	38.9	47.9	54.7	50.9	46.1	41.8
20/09/2020 13:00:30	00:15:00	59.9	38.9	48.4	55.7	51.9	46.3	41.5
20/09/2020 13:15:30	00:15:00	61.8	38	47.6	54.7	50.9	45.9	40.4
20/09/2020 13:45:32	00:15:00	60.9	38.7	46.9	53.6	50.1	45.3	41.3
20/09/2020 14:00:32	00:15:00	62.5	38.2	49.2	58.2	52.1	47.1	41.9
20/09/2020 14:15:32	00:15:00	63.3	39.4	48.7	55	51.6	47.3	43.5
20/09/2020 14:30:32	00:15:00	62.7	39.7	48.6	55.9	51.9	46.8	42.1
20/09/2020 14:45:32	00:15:00	69.7	37.9	49.6	61.8	50.8	45.6	41.3
20/09/2020 15:00:32	00:15:00	67.5	39.1	48.2	57.9	50.7	45.3	41.1
20/09/2020 15:15:32	00:15:00	66.2	39.3	48.2	55.6	51.2	46.3	42.2
20/09/2020 15:30:32	00:15:00	67.3	39.4	49.5	58.9	51.7	46.6	42.2
20/09/2020 15:45:32	00:15:00	66.3	37.8	48.4	56	51.3	46.1	41.2
20/09/2020 16:00:32	00:15:00	76.6	38.8	57.3	69.4	57.7	47.6	41.7
20/09/2020 16:15:32	00:15:00	64.3	39.3	48	55.2	50.9	46.2	41.8
20/09/2020 16:30:32	00:15:00	67.1	38.1	49.9	60.4	52.5	46.4	41.5
20/09/2020 16:45:32	00:15:00	71.1	38.1	48.3	56	51.1	45.6	41.3
20/09/2020 17:00:32	00:15:00	75.2	38.3	49.2	54.9	51.6	46.7	41.7
20/09/2020 17:15:32	00:15:00	63.7	37.6	48.1	57.2	51.3	45.1	41
20/09/2020 17:30:32	00:15:00	59.2	38.5	47.1	54.4	50.6	45	40.9
20/09/2020 17:45:32	00:15:00	63.3	38.2	47.5	54.4	50.9	45.5	41.2
20/09/2020 18:00:32	00:15:00	64.1	38.7	50.5	59.6	53.5	48	42.5
20/09/2020 18:15:32	00:15:00	66	38.5	49.5	58.1	52.5	47.2	42.4
20/09/2020 18:30:32	00:15:00	62.4	39.9	48.3	54.5	51.2	47	42.7
20/09/2020 18:45:32	00:15:00	58.7	38.1	47.7	55	51.1	45.6	40.4
20/09/2020 19:00:32	00:15:00	59.2	37.9	47.2	54.6	51	44.6	40.3
20/09/2020 19:15:32	00:15:00	59.3	38.2	47.1	54.7	50.5	44.7	40.7
20/09/2020 19:30:32	00:15:00	69.7	38.2	49	59.1	50.4	44.6	40.6
20/09/2020 19:45:32	00:15:00	67.7	36.6	48.1	57.4	51.2	44.4	39.7
20/09/2020 20:00:32	00:15:00	62.4	37.7	47	55.5	50.6	44	39.9
20/09/2020 20:15:32	00:15:00	61.5	36.7	47.4	58.3	50.5	42.3	39.2
20/09/2020 20:30:32	00:15:00	58.5	38	46.6	54.9	50.6	43.3	40.1
20/09/2020 20:45:32	00:15:00	56.5	38.3	45.6	53	49.4	42.6	40.2
20/09/2020 21:00:32	00:15:00	55.8	38.8	45.7	53	49.3	43.2	40.3
20/09/2020 21:15:32	00:15:00	59.2	37	45.7	54.6	49.3	42.3	39.3
20/09/2020 21:30:32	00:15:00	61.5	37.7	45.6	52.9	49	43.3	39.9

20/09/2020 21:45:32	00:15:00	62	37.3	46.2	56.2	49.6	42.6	39.3
20/09/2020 22:00:32	00:15:00	65.1	36.2	46.5	57.8	49.5	41.8	38.5
20/09/2020 22:15:32	00:15:00	64.9	36.1	46	55.8	49.6	41	38.6
20/09/2020 22:30:32	00:15:00	62.3	36.8	45.1	53.7	48.9	41	38.4
20/09/2020 22:45:32	00:15:00	55.3	34.9	42.9	51.5	45.9	40.6	38.4
20/09/2020 23:00:32	00:15:00	59.6	36.2	44.6	53.7	48.7	40.5	38.2
20/09/2020 23:15:32	00:15:00	54.4	36.5	42.2	50.9	45.3	39.8	38.3
20/09/2020 23:30:32	00:15:00	56.5	37.4	44.4	52.5	47.7	42.2	39.5
20/09/2020 23:45:32	00:15:00	57.2	36.8	43.8	53.4	47	41	38.9
21/09/2020 00:00:32	00:15:00	57.4	35.8	42.5	52.4	45.2	39.6	37.9
21/09/2020 00:15:32	00:15:00	56.6	36	41.9	51.7	43.3	39.6	37.8
21/09/2020 00:30:32	00:15:00	56.5	36.1	41.6	50.9	42.9	39.6	37.6
21/09/2020 00:45:32	00:15:00	57.7	35	42	51.6	43.9	39.1	37.1
21/09/2020 01:00:32	00:15:00	56.1	34.2	41.4	51.2	43.1	38.7	36.4
21/09/2020 01:15:32	00:15:00	56.5	34.2	39.6	48.7	40.6	37.9	36
21/09/2020 01:30:32	00:15:00	57.1	31.2	39	49.4	39.2	35.7	33.4
21/09/2020 01:45:32	00:15:00	54.6	31.8	36.6	46.4	36.7	34.5	33.1
21/09/2020 02:00:32	00:15:00	54	33.2	38.1	47.8	38.7	36.7	35.3
21/09/2020 02:15:32	00:15:00	49.5	34.2	38.5	46.8	39.6	37.2	35.7
21/09/2020 02:30:32	00:15:00	58.4	34	40.4	53	39.8	37.1	35.5
21/09/2020 02:45:32	00:15:00	49.7	34	37.5	42.9	39.3	36.7	35.2
21/09/2020 03:00:32	00:15:00	49.7	33.9	37.5	44.5	39	36.6	35.1
21/09/2020 03:15:32	00:15:00	51.3	32.4	37.2	45.7	38.7	35.8	34.1
21/09/2020 03:30:32	00:15:00	51.1	32.4	36.5	44.1	37.5	35.3	34
21/09/2020 03:45:32	00:15:00	54.9	33.3	38.5	48	39.9	36.4	34.7
21/09/2020 04:00:32	00:15:00	52.6	32.7	37.6	47.7	38.8	35.9	34.1
21/09/2020 04:15:32	00:15:00	53.1	31.3	35.9	44.1	36.4	34.5	33.1
21/09/2020 04:30:32	00:15:00	55.3	34	38.5	48.5	38.9	36.7	35.4
21/09/2020 04:45:32	00:15:00	49.6	34.1	38.4	45.2	39.6	37.7	36.2
21/09/2020 05:00:32	00:15:00	53.4	34.9	38.1	43.2	38.9	37.4	36.2
21/09/2020 05:15:32	00:15:00	54	35.3	39.6	50.4	40.3	38.1	36.6
21/09/2020 05:30:32	00:15:00	55.5	35.5	42.7	52	45.8	39.6	37.8
21/09/2020 05:45:32	00:15:00	56	37.5	42.8	51.2	44.7	41.2	39.2
21/09/2020 06:00:32	00:15:00	55	38.8	43.3	50.9	45.9	41.7	40.1
21/09/2020 06:15:32	00:15:00	60.2	38.7	46.4	56.8	49.2	42.5	40.2
21/09/2020 06:30:32	00:15:00	70.9	40.4	49.8	62	50	44.5	42.2
21/09/2020 06:45:32	00:15:00	69.4	42.2	49.1	58.2	51.5	45.9	43.5
21/09/2020 07:00:32	00:15:00	64.7	41.8	48.6	57	51.8	45.7	43.7
21/09/2020 07:15:32	00:15:00	62.7	41.8	49.2	57.1	52.2	47	43.6
21/09/2020 07:30:32	00:15:00	63.9	42.6	50.2	57.3	52.9	48.7	45.5
21/09/2020 07:45:32	00:15:00	76.1	42.6	53.8	63.9	53.8	49.9	45.4
21/09/2020 08:00:32	00:15:00	72.9	44	52.5	62.5	54	49.9	46.2
21/09/2020 08:15:32	00:15:00	68.6	42.6	50.6	57.3	52.6	49.1	45.4
21/09/2020 08:30:32	00:15:00	70.4	44.6	51.9	58.9	53.8	50.5	47.7
21/09/2020 08:45:32	00:15:00	71.6	45.2	53.8	62	55.7	51.8	49
21/09/2020 09:00:32	00:15:00	67.8	43	51.5	57.7	53.9	50.5	46.7

21/09/2020 09:15:32	00:15:00	74.2	41.1	51.4	59.6	53.5	48.9	44
21/09/2020 09:30:32	00:15:00	68.4	38.6	50	58.5	53.2	47.7	42
21/09/2020 09:45:32	00:15:00	77.4	38.1	51.9	63	54.1	46.9	40.6

